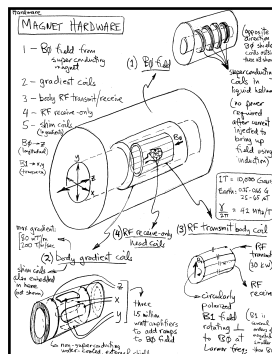


Foundations of Neuroimaging

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13 Nov 2022

(124 pages)



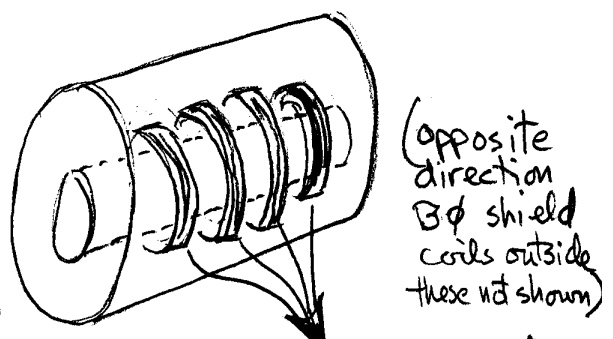
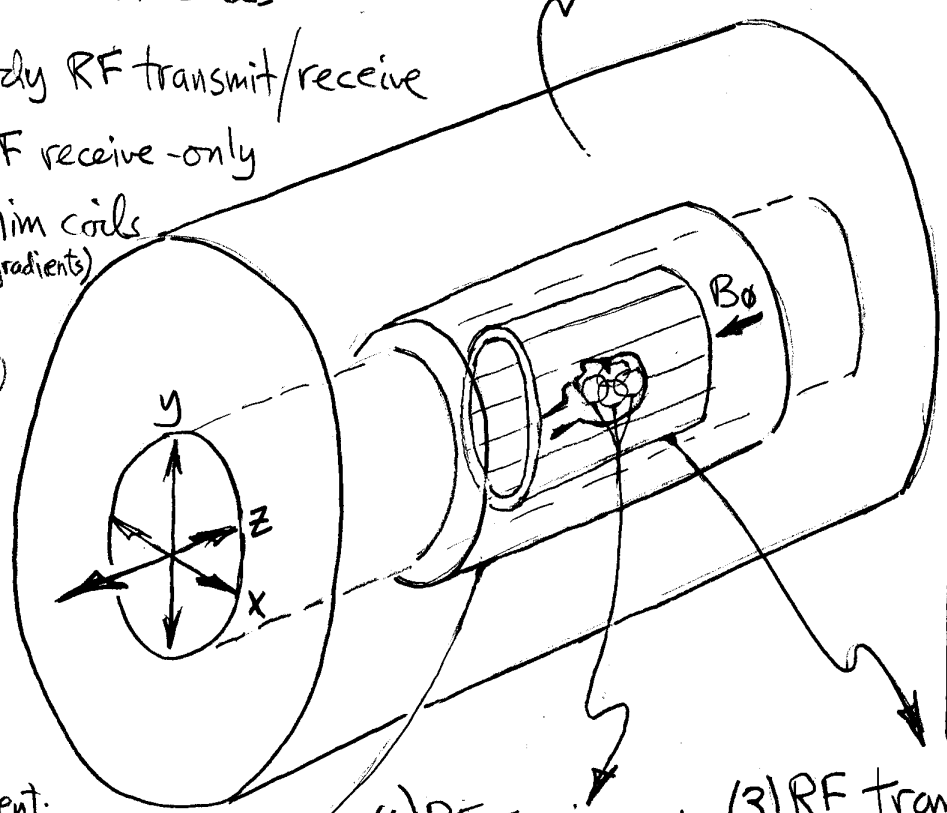
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Hardware

MAGNET HARDWARE

- 1 - B_0 field from superconducting magnet
- 2 - gradient coils
- 3 - body RF transmit/receive
- 4 - RF receive-only
- 5 - shim coils (in gradients)

$B_0 \rightarrow z$
(longitudinal)
 $B_1 \rightarrow x, y$
(transverse)



(opposite direction B_0 shield coils outside these not shown)

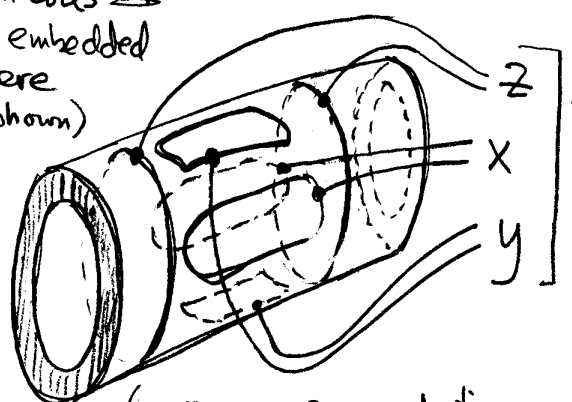
superconducting coils in liquid helium
(no power required after current injected to bring up field using induction)

$I_T = 10,000$ Gauss
Earth: $0.25 - 0.65$ G
 $25 - 65$ μ T
 $\frac{\gamma}{2\pi} = 42$ MHz/T

max gradient:
[80 mT/m
200 T/m/sec

(2) body gradient coils

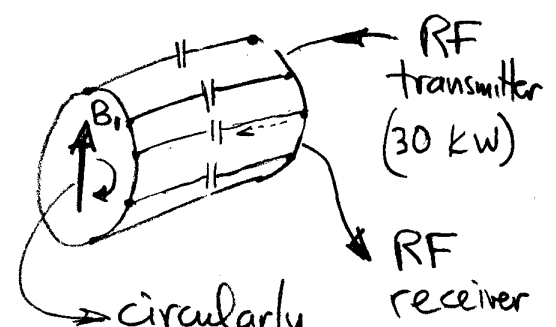
shim coils also embedded in here (not shown)



non-superconducting water-cooled, external shield

(4) RF receive-only head coils

(3) RF transmit body coil



circularly polarized B_1 field (rotating \perp to B_0 at Larmor freq: B_1 is several orders of magnitude smaller than B_0)

SPIN & PRECESSION

N.B.: compared to top & gravity
magnetic relaxation is:

- frictionless spin, doesn't slow
- signed gravity
 - ↳ can change precession dir
 - ↳ can stick under floor
- neighbor bumping causes decay (T2)

- nuclei act like a spinning sphere of matter with an embedded equatorial charge (nuclei w/ odd atomic weight or odd proton numbers)
- moving charge creates magnetic field



classical picture

- current loop from spinning charge (right-hand rule)
- N.B.: classically this would cause EM radiation, spindown

- Stern-Gerlach experiment

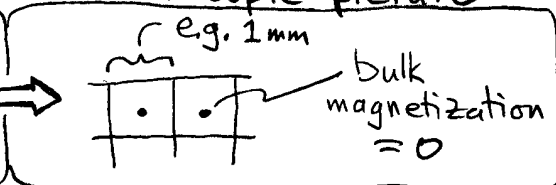
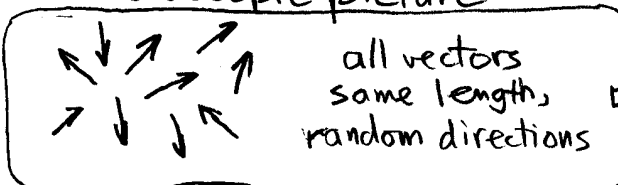


pass silver atoms thru strong mag. field → split into just 2 beams

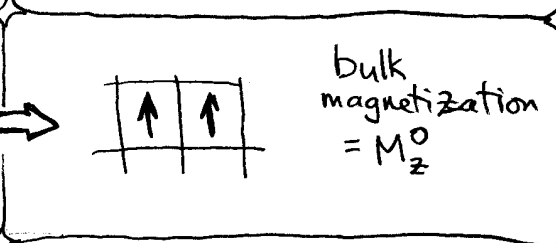
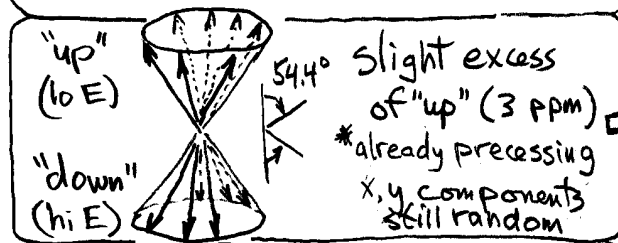
Microscopic picture

Macroscopic picture

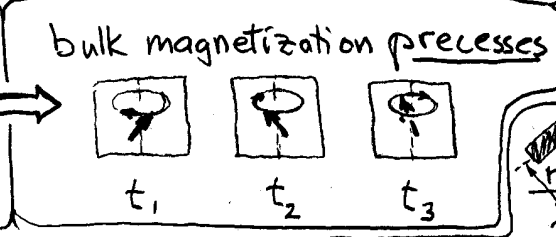
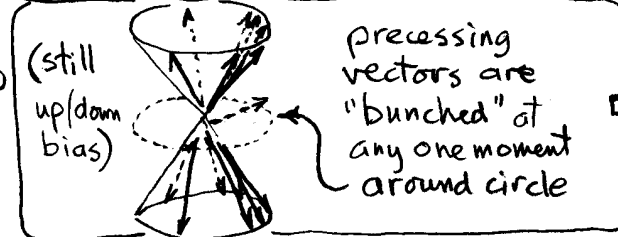
no strong magnetic field
 $B_0 = 0$



Strong magnetic field, $B_0 = \uparrow$



Strong B_0 plus oscillating B_1



Precession

- distinguish precession (slow) from spin (fast)
- treat classically, like spinning top

"Y" $\leftarrow \frac{\gamma}{2\pi} = \frac{r \cdot m \cdot g}{I \cdot \omega_{spin}}$
 $\omega_{top} = \frac{L}{I} = \frac{Ang. mom.}{inertia}$

$2\pi f_0 = \omega_0 = \gamma B_0$
 Larmor freq (e.g. 63 MHz) Same in radians/sec gyro-magnetic ratio static field (e.g. 1.5T)



left-hand rule:
thumb = B_0
fingers = precess.

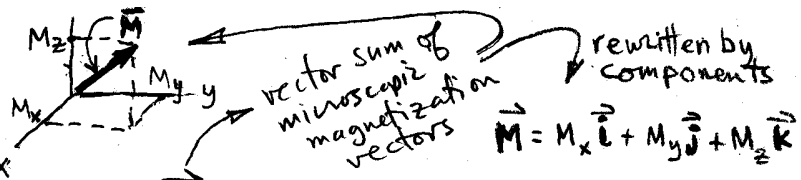
like top: precession faster w/ more gravity

- bulk equilibrium magnetization (parallel to B_0)

$M_z^0 = |\vec{M}| = \frac{\gamma^2 \hbar^2 B_0 N_s}{4 K T_s}$
 where $I = \pm 1/2$

- γ = gyromagnetic ratio
- \hbar = Planck's const.
- $B_0 \rightarrow$ i.e., M_z^0 proportional to B_0 strength
- $N_s \rightarrow$ i.e., M_z^0 proportional to number spins
- K = Boltzmann const.
- T_s = abs. temperature sample

BLOCH EQUATION



- time-dependent behavior of \vec{M} in the presence of an applied magnetic field (excitation \neq relaxation)

equilibrium \vec{M} value in only the B_0 field

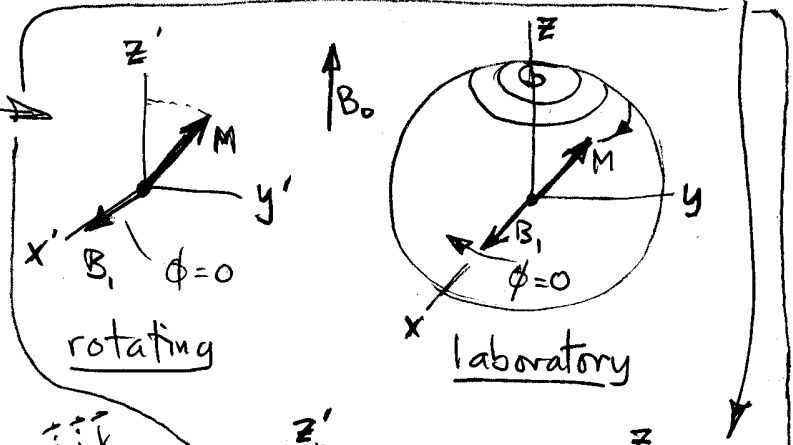
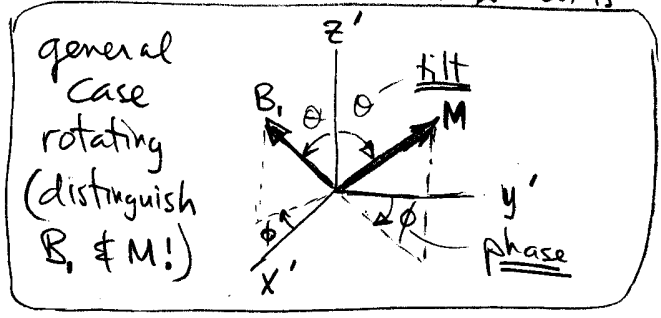
precession: $B = B_0$
excitation: $B = B_0 + B_1$

(Laboratory frame) $\frac{d\vec{M}}{dt} = \underbrace{\vec{M} \times \vec{B}}_{\text{existing mag vector sum} \times \text{applied field (typically rotating)}} - \underbrace{\frac{M_x \vec{i} + M_y \vec{j}}{T_2}}_{\text{"transverse" "spin-spin"}} - \underbrace{\frac{(M_z - M_z^0) \vec{k}}{T_1}}_{\text{"longitudinal" "spin-lattice"}}$

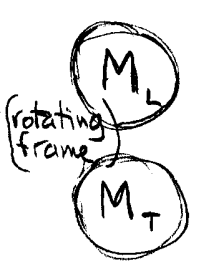
unit vector \vec{z} -dir.

these can be ignored during short excitation, so magnetic vector stays same length as it spirals down (vs. relaxation, where it shrinks, then grows)

- in the Larmor-rotating coordinate system, a tilt w/o a phase shift for a standard B_1 excitation is rotation around x -axis



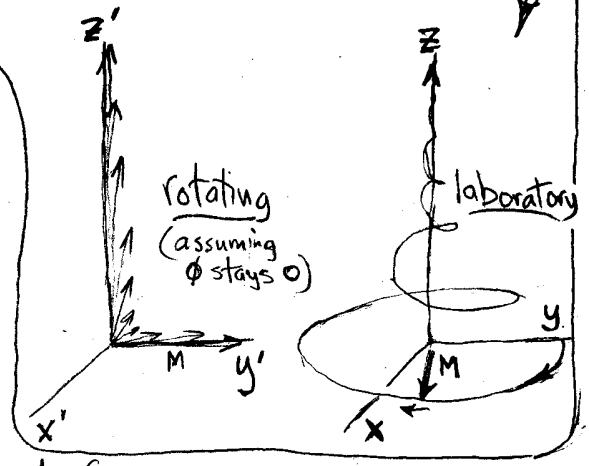
- longitudinal and transverse relaxations



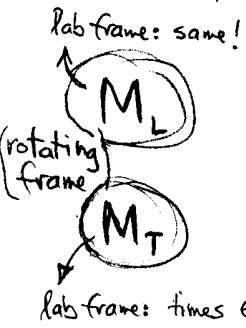
$$\frac{dM_z(t)}{dt} = -\frac{M_z(t) - M_z^0}{T_1}$$

$$\frac{dM_{x'y'}(t)}{dt} = -\frac{M_{x'y'}(t)}{T_2}$$

from Bloch equation after dropping applied field term



- solution to equations above: \vec{M} : time-dependent free precession eq's



Lab frame: same!

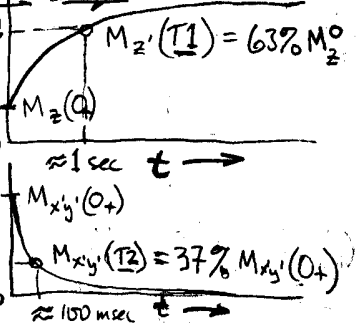
$$M_{z'}(t) = M_z^0 (1 - e^{-t/T_1}) + M_{z'}(0_+) e^{-t/T_1}$$

[equiv] $= M_z^0 + [M_{z'}(0_+) - M_z^0] e^{-t/T_1}$

$$M_{x'y'}(t) = M_{x'y'}(0_+) e^{-t/T_2}$$

initial condition

ML, MT at time immed. after pulse



Bloch-1c

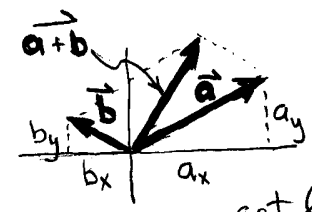
VECTOR ADD, MULTIPLY

- adding vectors is easy

$$\vec{c} = \vec{a} + \vec{b} = [a_x + b_x, a_y + b_y]$$

- just add components (vector)
- applies to complex numbers

- generalizes to any D



get length

$$\|\vec{c}\| = \sqrt{(a_x + b_x)^2 + (a_y + b_y)^2}$$

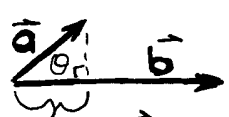
- multiple ways to multiply vectors: here are 3

dot product

(= inner product)
(= "scaled projection onto")

$$c = \vec{a} \cdot \vec{b} = [b_x \ b_y \ b_z] \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix} = a_x b_x + a_y b_y + a_z b_z$$

(scalar)



$p = \|\vec{a}\| \cos \theta$
 $c = p \|\vec{b}\|$ \rightarrow $c = p$ if $\|\vec{b}\| = 1$

- generalizes to any D

N.B. equals: $\sqrt{\vec{a} \cdot \vec{a}}$
 $\sqrt{a_x^2 + a_y^2 + a_z^2}$

length of \vec{a}

$$c = \|\vec{a}\| \|\vec{b}\| \cos \theta$$

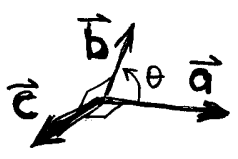
\rightarrow zero if \vec{a}, \vec{b} orthogonal

Cross product

(= outer product)
(can be generalized: see "geometric algebra")

$$\vec{c} = \vec{a} \times \vec{b} = \begin{bmatrix} 0 & b_z & -b_y \\ -b_z & 0 & b_x \\ b_y & -b_x & 0 \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix} = [a_y b_z - a_z b_y, a_z b_x - a_x b_z, a_x b_y - a_y b_x]$$

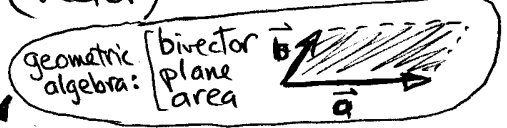
(vector)



skew-symmetric: $A^T = -A$

right hand rule: curl fingers from \vec{a} to \vec{b} : thumb is \vec{c}

- unique orthogonal specific to 3D



$$\|\vec{c}\| = \|\vec{a}\| \|\vec{b}\| \sin \theta$$

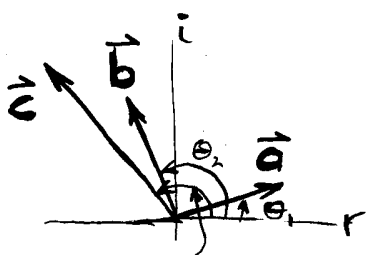
\rightarrow max if orthogonal

Complex multiply

(see also quaternions, geometric algebra generalization)

$$\vec{c} = \vec{a} \cdot \vec{b} = \begin{bmatrix} b_x & -b_y \\ b_y & b_x \end{bmatrix} \begin{bmatrix} a_x \\ a_y \end{bmatrix} = [a_x b_x - a_y b_y, a_x b_y + a_y b_x]$$

(vector)



sum of angles: $\theta_1 + \theta_2$

- angles add
- magnitudes multiply

- specific to 2D

$$\|\vec{c}\| = \|\vec{a}\| \|\vec{b}\|$$

\rightarrow like real nums

cf. not affected by angle between

Bloch 1a

EFFECTS OF \vec{M} , \vec{B} , and θ ON PRECESSION FREQ.

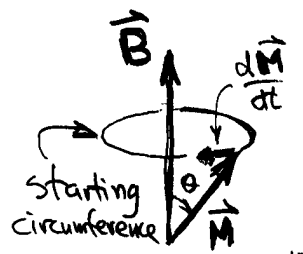
Bloch 1st term

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B}$$



cross prod. properties review

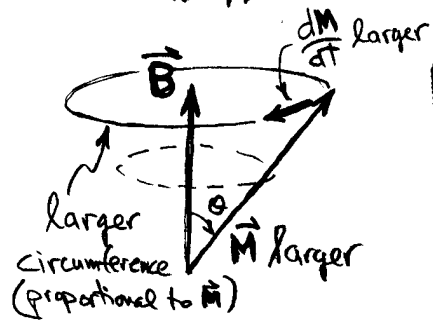
$$\left\| \frac{d\vec{M}}{dt} \right\| = \|\vec{M}\| \cdot \|\gamma \vec{B}\| \cdot \sin \theta$$



starting condition

now see effects of changing $\|\vec{M}\|, \|\vec{B}\|, \theta$

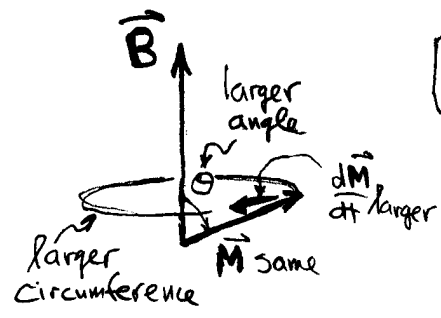
N.B. length vectors define this



change \vec{M} length

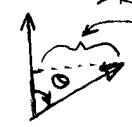
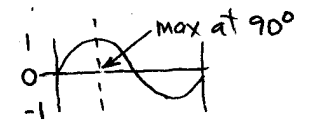
$\frac{d\vec{M}}{dt}$ proportionally larger, so cancels effect of larger \vec{M}

b/c \vec{M} on both sides eq.
 \uparrow
 same precession freq. as starting cond.



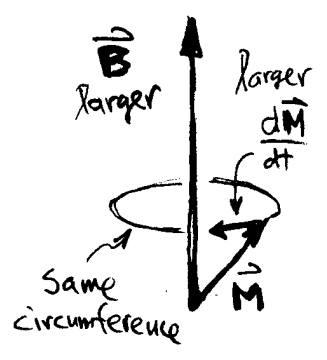
change θ between \vec{M} and \vec{B}

$\frac{d\vec{M}}{dt}$ goes up (then down) as $\sin \theta$
 but circumference also goes up as $\sin \theta$, cancelling again



opposite = $\sin \theta$ = radius
 so circumference proportional to $\sin \theta$

same precession freq.



change \vec{B} length

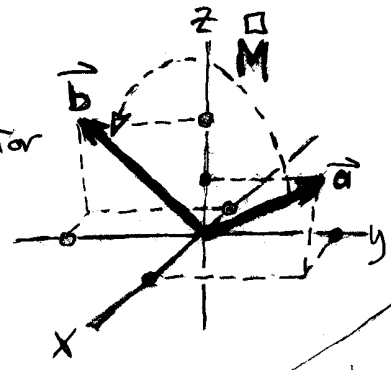
$\frac{d\vec{M}}{dt}$ goes up, proportional to \vec{B}
 but circumference is same at starting cond.

increased precession freq. ($\omega = \gamma B$)

Blach-1e SIMPLE MATRIX OPERATIONS

Basic idea

- a matrix $\left[\begin{matrix} \text{rotates} \\ \text{scales} \end{matrix} \right]$ a vector

$$\vec{b} = M \vec{a}$$


to get a pure rotation (no scaling) these 3 col. vectors must be orthogonal

3D example

$$\begin{bmatrix} b_x \\ b_y \\ b_z \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} & M_{13} \\ M_{21} & M_{22} & M_{23} \\ M_{31} & M_{32} & M_{33} \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix}$$

Add translate (after rotate/scale)

- commonly used "hack" for aligning vols

- a 4D matrix $\left[\begin{matrix} \text{rotates/scales} \\ \text{then} \\ \text{translates} \end{matrix} \right]$ a 3D vector (4th D=1)

- N.B.: Have to keep track of order!!

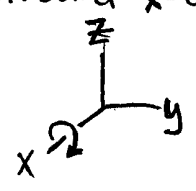
$$\begin{aligned} b_x &= M_{11}a_x + M_{12}a_y + M_{13}a_z \\ b_y &= M_{21}a_x + M_{22}a_y + M_{23}a_z \\ b_z &= M_{31}a_x + M_{32}a_y + M_{33}a_z \end{aligned}$$

→ rotate/scale then trans \neq trans, then rot/scale
 → change rot component: untranslate, rot, retranslate

$$\begin{bmatrix} b_x \\ b_y \\ b_z \\ 1 \end{bmatrix} = \begin{bmatrix} \begin{matrix} 3 \times 3 \\ \text{rot/scale} \end{matrix} & \begin{matrix} dx \\ dy \\ dz \end{matrix} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \\ 1 \end{bmatrix}$$

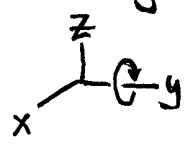
3 special cases (3D): rotate around each major axis without changing length (scale = 1.0)

- rotate around x-axis: $R_x(\alpha) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha & \sin \alpha \\ 0 & -\sin \alpha & \cos \alpha \end{bmatrix}$



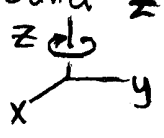
e.g., 90° flip

- rotate around y-axis: $R_y(\alpha) = \begin{bmatrix} \cos \alpha & 0 & -\sin \alpha \\ 0 & 1 & 0 \\ \sin \alpha & 0 & \cos \alpha \end{bmatrix}$



e.g., 180° flip to avoid add 180° phase after 90° flip on x'

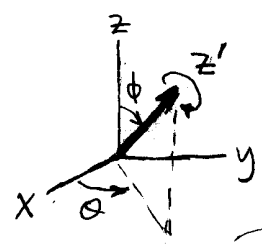
- rotate around z-axis: $R_z(\alpha) = \begin{bmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$



e.g., precession with $B\phi$ along z'

General case

- rotate around general z'-axis:



$$R_{z'}(\alpha) = R_z(-\theta) R_y(-\phi) R_z(\alpha) R_y(\phi) R_z(\theta)$$

(quaternions are more efficient)

[unrot. axis to z
z-rot.
re-rot.]

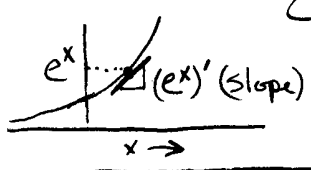
SOLUTIONS TO SIMPLE DIFFERENTIAL EQ.

diff. eq.: $dM_{x'y'}(t) = -\frac{M_{x'y'}(t)}{T_2}$

solution: $M_{x'y'}(t) = M_{x'y'}(0_+) \cdot e^{-t/T_2}$

\uparrow ?? How this works, and where $M_{x'y'}(0_+)$ comes from...

- Goal:
- 1) find eq. whose derivative satisfies diff. eq.
 - 2) also find sol'n (one of many) that passes thru init condition



\leftarrow since our diff. eq. is: derivative of funct. = const. same funct
 \leftarrow try exponential, since derivative $(e^x) = e^x$ 😊

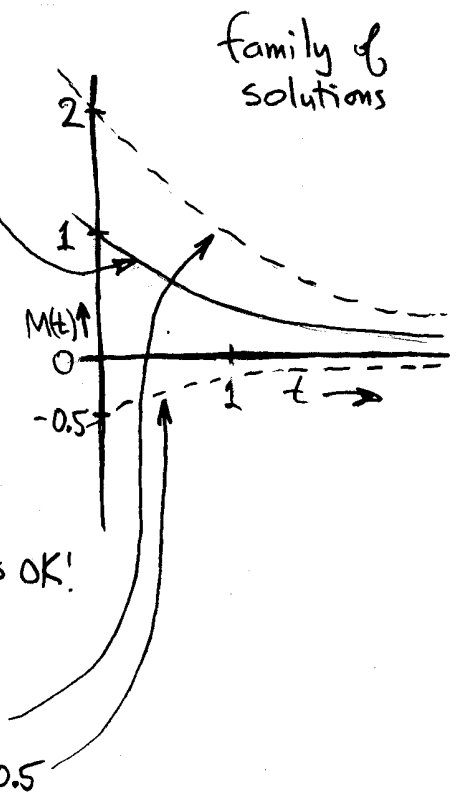
diff eq. $M'(t) = \frac{-1}{T_2} \cdot M(t)$

one sol'n $M(t) = e^{-t/T_2} = e^{\frac{-1}{T_2} \cdot t}$

take deriv. to check $M'(t) = \frac{-1}{T_2} \cdot e^{-t/T_2}$

Annotations: "deriv." points to $M'(t)$; "chain rule deriv of exponent" points to the exponent in the solution; "M(t)" points to the exponential term in the derivative.

N.B. this function is the "unknown" like the x in $x+1=3$



diff eq. $M'(t) = \frac{-1}{T_2} \cdot M(t)$

another sol'n $M(t) = \text{const} \cdot e^{-t/T_2}$

take deriv. to check $M'(t) = \frac{-1}{T_2} \cdot \text{const} \cdot e^{-t/T_2}$

Annotations: "chain rule" points to the exponent; "So: any const is OK!" points to the constant term; "for ex.: const = 2, const = -0.5" provides examples.

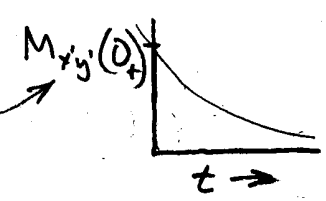
const is "initial condition"

information added to sol'n (not from diff eq.)

const = $M_{x'y'}(0_+)$

$M(t) = M_{x'y'}(0_+) \cdot e^{-t/T_2}$

magnetization immed. after RF (B1) ends



Bloch-1c2

VERIFY SOLUTION TO T1 REGROWTH

- slightly more complex T1 soln compared to T2 soln

T2 soln verify (from prev.)

T1 solution verify

$$\frac{dM}{dt} = \frac{M_{xy}}{T_2}$$

original
diff eq.

$$\frac{dM}{dt} = \frac{-(M_z - M_z^0)}{T_1}$$

$$M'(t) = \frac{-1}{T_2} \cdot M(t)$$

make unknown
funct $M(t)$
more visible

$$M'(t) = \frac{-1}{T_1} (M(t) - M_z^0)$$

init cond.

$$M(t) = M_{xy}(0_+) e^{-t/T_2}$$

proposed
solution

$$M(t) = M_z^0 (1 - e^{-t/T_1}) + M_z(0_+) e^{-t/T_1}$$

$$= M_z^0 - M_z^0 e^{-t/T_1} + M_z(0_+) e^{-t/T_1}$$

const

chain rule
as before

chain rule

$$M'(t) = \frac{-1}{T_2} M_{xy}(0_+) e^{-t/T_2}$$

test
by take
deriv.

$$M'(t) = 0 + \frac{1}{T_1} M_z^0 e^{-t/T_1} - \frac{1}{T_1} M_z(0_+) e^{-t/T_1}$$

$$= \frac{-1}{T_1} (-M_z^0 e^{-t/T_1} + M_z(0_+) e^{-t/T_1})$$

- derivative in original T1 eq. says $M(t)$ minus M_z^0

$$M'(t) = \frac{-1}{T_1} (M(t) - M_z^0)$$

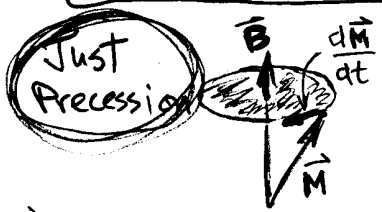
$$\text{solution} \rightarrow M_z^0 - M_z^0 e^{-t/T_1} + M_z(0_+) e^{-t/T_1}$$

- which equals our re-calculated derivative:

$$M'(t) = \frac{-1}{T_1} (-M_z^0 e^{-t/T_1} + M_z(0_+) e^{-t/T_1})$$

Block-1d

BLOCH EQ. - MATRIX VERSION

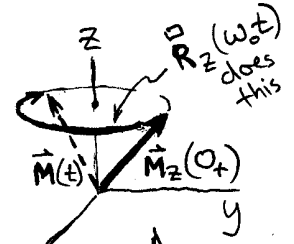


Differential Eq.:

$$\frac{d\vec{M}}{dt} = \begin{bmatrix} \frac{dM_x}{dt} \\ \frac{dM_y}{dt} \\ \frac{dM_z}{dt} \end{bmatrix} = \begin{bmatrix} 0 & \gamma B \phi & 0 \\ -\gamma B \phi & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix}$$

$$\vec{a} \times \vec{b} = \begin{bmatrix} 0 & b_z & -b_y \\ -b_z & 0 & b_x \\ b_y & -b_x & 0 \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix}$$

assume only z component of B present



Solution:

$$\vec{M}(t) = \begin{bmatrix} M_x(t) \\ M_y(t) \\ M_z(t) \end{bmatrix} = \begin{bmatrix} \cos \omega t & \sin \omega t & 0 \\ -\sin \omega t & \cos \omega t & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} M_x(0_+) \\ M_y(0_+) \\ M_z(0_+) \end{bmatrix} = R_z(\omega t) \vec{M}(0_+)$$

initial condition

Include Relaxation

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B} \phi - \frac{M_x \vec{i} + M_y \vec{j}}{T_2} - \frac{(M_z - M_z^0) \vec{k}}{T_1}$$

Differential Eq.:

$$\frac{d\vec{M}}{dt} = \begin{bmatrix} -1/T_2 & \gamma B \phi & 0 \\ -\gamma B \phi & -1/T_2 & 0 \\ 0 & 0 & -1/T_1 \end{bmatrix} \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ M_z^0/T_1 \end{bmatrix}$$

Solution:

$$\vec{M}(t) = \begin{bmatrix} e^{-t/T_2} & 0 & 0 \\ 0 & e^{-t/T_2} & 0 \\ 0 & 0 & e^{-t/T_1} \end{bmatrix} \begin{bmatrix} \cos \omega t & \sin \omega t & 0 \\ -\sin \omega t & \cos \omega t & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} M_x(0_+) \\ M_y(0_+) \\ M_z(0_+) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ M_z(0_+) (1 - e^{-t/T_1}) \end{bmatrix}$$

initial condition

Bloch-1f EXCITATION IN THE ROTATING FRAME

Remember:

$$\vec{a} \times \vec{b} = \begin{bmatrix} 0 & b_z - b_y & a_x \\ -b_z & 0 & b_x \\ b_y - b_x & 0 & 0 \end{bmatrix} \begin{bmatrix} a_x \\ a_y \\ a_z \end{bmatrix}$$

- original Bloch eq. in laboratory frame

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B}$$

$\begin{cases} B\phi \\ B1 \\ \text{gradients} \end{cases}$

- add on-resonance B1 to TSP

$$\vec{B} = B1(t) (\cos \omega_0 t \hat{i} - \sin \omega_0 t \hat{j}) + B\phi \hat{k}$$

lab frame $\begin{cases} \text{on-resonance} \\ \text{no gradient} \end{cases}$
 *basic excite
 ↳ matrix version

$$\frac{d\vec{M}}{dt} = \begin{bmatrix} \frac{dM_x'}{dt} \\ \frac{dM_y'}{dt} \\ \frac{dM_z'}{dt} \end{bmatrix} = \begin{bmatrix} 0 & \gamma B\phi & \omega_1(t) \cos \omega_0 t \\ -\omega_0 & 0 & \omega_1(t) \sin \omega_0 t \\ \omega_1(t) \sin \omega_0 t & -\omega_1(t) \cos \omega_0 t & 0 \end{bmatrix} \begin{bmatrix} M_x \\ M_y \\ M_z \end{bmatrix}$$

$\begin{matrix} \text{matrix multiply} \\ \text{matrix multiply} \\ \text{matrix multiply} \end{matrix}$

$\begin{matrix} \text{B1 y comp.} \\ \text{B1 x comp.} \end{matrix}$

- substitution to convert to the rotating frame

$$\begin{cases} \vec{M} \\ \vec{B} \end{cases} = \begin{cases} R_z(\omega_0 t) \\ R_z(\omega_0 t) \end{cases} \cdot \begin{cases} \vec{M}_{rot} \\ \vec{B}_{rot} \end{cases}$$

"subtract off" rotating frame both \vec{M} and \vec{B}

- after substitution any off-resonance appears as residual $B\phi$ (B_z) (see off-res notes page)

$$\frac{d\vec{M}_{rot}}{dt} = \vec{M}_{rot} \times \gamma \vec{B}_{eff}$$

$\begin{cases} \text{off-res (appears as } B\phi) \\ B1 \\ \text{gradients} \end{cases}$

rotating frame $\begin{cases} \text{on-resonance} \\ \text{no gradient} \end{cases}$
 *basic excite, B1x-only
 ↳ removes ω_0 , cos/sin

$$\frac{d\vec{M}_{rot}}{dt} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \omega_1(t) \\ 0 & -\omega_1(t) & 0 \end{bmatrix} \begin{bmatrix} M_{x'} \\ M_{y'} \\ M_{z'} \end{bmatrix}$$

$\begin{matrix} \text{ignore } x, z, \pi \\ \text{B1y=0} \end{matrix}$

rotating frame - off-resonance
 *general, B1x-only incl gradients

$$\frac{d\vec{M}_{rot}}{dt} = \begin{bmatrix} 0 & \omega_0 - \omega + \omega(z) & 0 \\ -(\omega_0 - \omega + \omega(z)) & 0 & \omega_1(t) \\ 0 & -\omega_1(t) & 0 \end{bmatrix} \begin{bmatrix} M_{x'} \\ M_{y'} \\ M_{z'} \end{bmatrix}$$

$\begin{matrix} \text{off-res.} \\ \text{gradient} \end{matrix}$

gradient: $\omega(z) = \gamma G_z z$

off-res: appears as residual B_z , lifting $B1$ vect. out of x-y plane

this means \vec{M} vect. update will contain component that rotates \vec{M} around z-axis (in rotating coords \equiv phase)

rotating frame $\begin{cases} \text{on-resonance} \\ \text{incl gradient} \end{cases}$
 *small tip approx. $\begin{cases} \text{small tip} \\ M_z \approx M_z^0 \\ \frac{dM_z}{dt} \approx 0 \end{cases}$

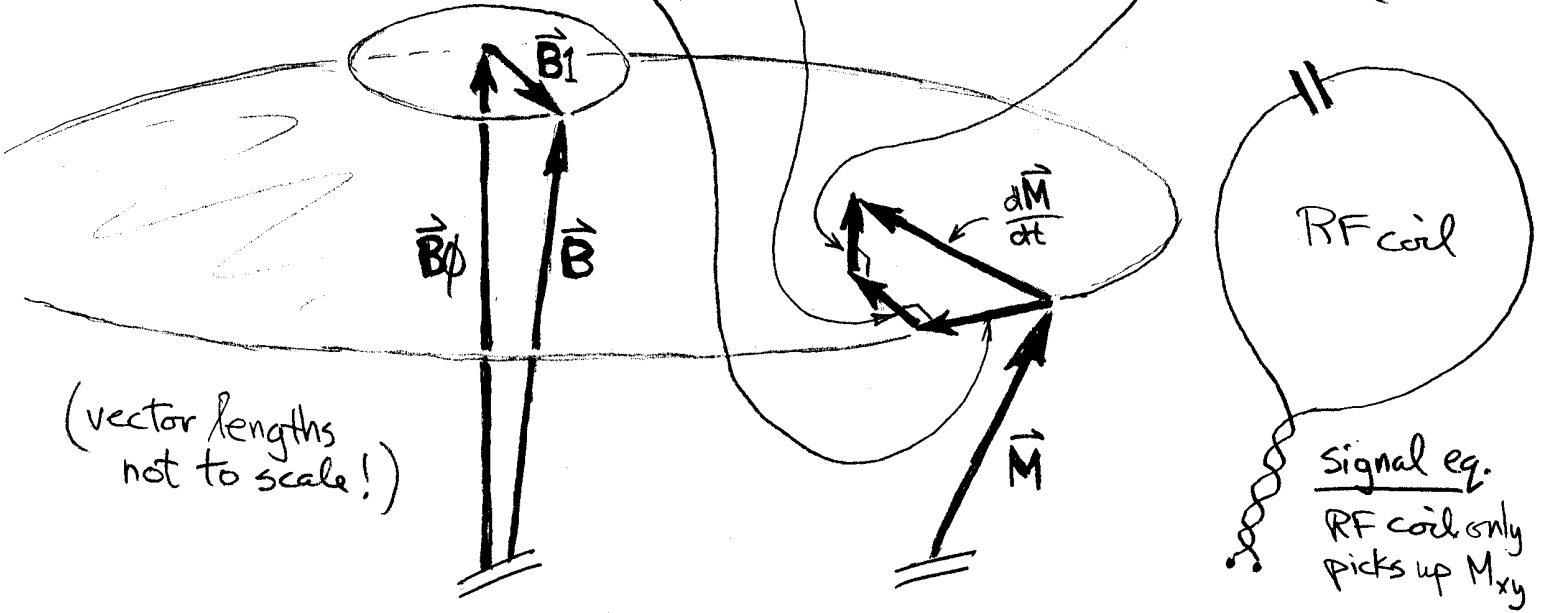
$$\frac{d\vec{M}_{rot}}{dt} = \begin{bmatrix} 0 & \omega(z) & 0 \\ -\omega(z) & 0 & \omega_1(t) \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} M_{x'} \\ M_{y'} \\ M_z^0 \end{bmatrix}$$

$\begin{matrix} \text{zeros this line in matrix} \\ \text{small tip} \Rightarrow \text{easier to solve!} \\ \text{small tip} \end{matrix}$

Bloch-1g
BLOCH EQ. SUMMARY

$$\frac{d\vec{M}}{dt} = \vec{M} \times \gamma \vec{B} - \frac{M_x \hat{i} + M_y \hat{j}}{T_2} - \frac{(M_z - M_z^0) \hat{k}}{T_1}$$

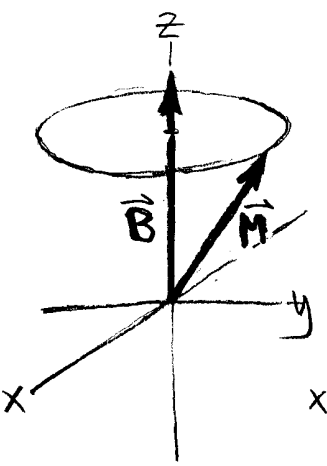
(Lab frame)



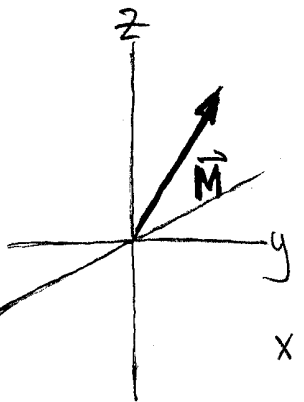
- full lab frame picture is complex:
 - 3 component of $\frac{d\vec{M}}{dt}$ update vector
 - Larmor freq. component 7-9 orders magnitude larger than T_2, T_1 decay
 - \vec{B}_1 is also rapidly wiggling
- conceptual simplification in 4 stages:

- 1) lab frame
- 2) rotating frame
- 3) add \vec{B}_1
- 4) off-resonance

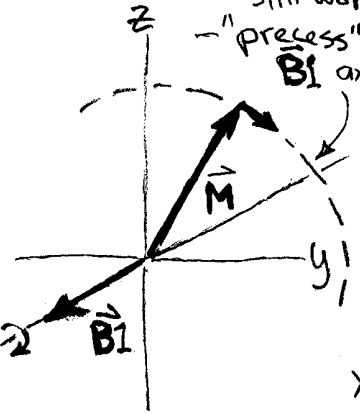
- just precession



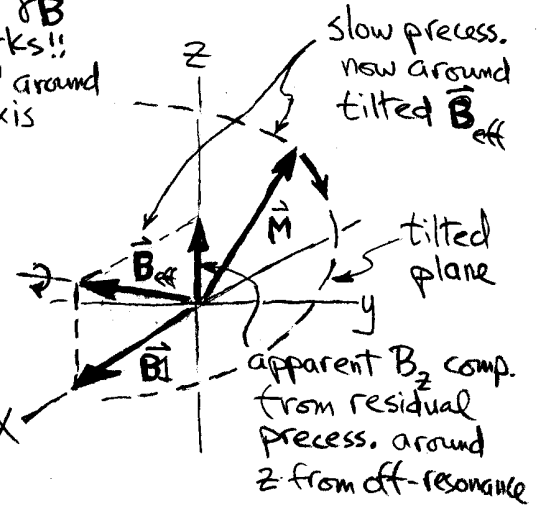
- \vec{M} stopped
 - that is, $B_0 = 0$



- \vec{B}_1 also stopped!
 - but $\vec{M} \times \gamma \vec{B}$ still works!!
 - "precess" around \vec{B}_1 axis



4) off-resonance



Bloch-2

RF FIELD POLARIZATION

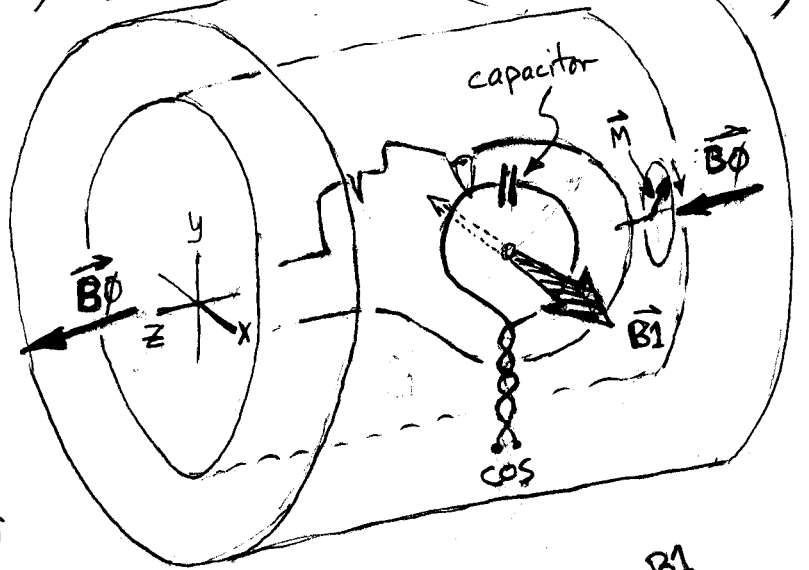
B1 generated/recorded by RF coil

- polarization (change of direction) of magnetic field (vs. electric field)

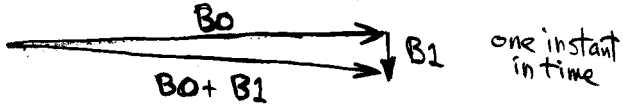
- linearly polarized field

$$\vec{B}_1(t) = \underbrace{B_1}_{\text{magn. strength}} \cdot \underbrace{\cos \omega t}_{\text{rad/sec} \rightarrow \text{sec}} \vec{x}$$

magn. strength $\cdot \{-1, 1\} \cdot 1$



- N.B.: \vec{B}_1 adds to much larger \vec{B}_0

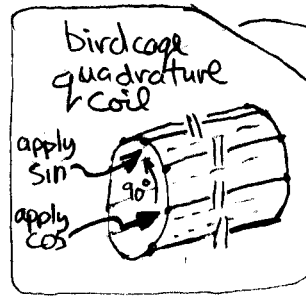
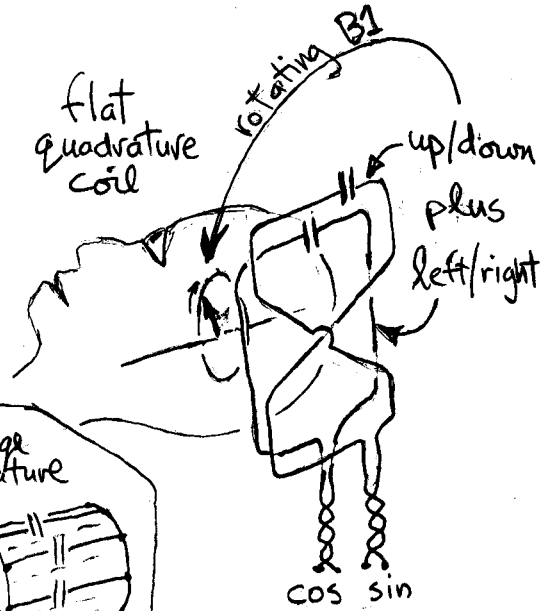
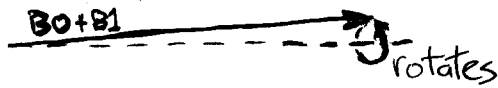
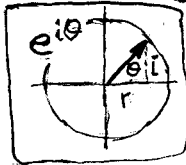


- circularly polarized field (quadrature)

$$\vec{B}_1^{circ}(t) = B_1 (\cos \omega t \vec{x} - \sin \omega t \vec{y})$$

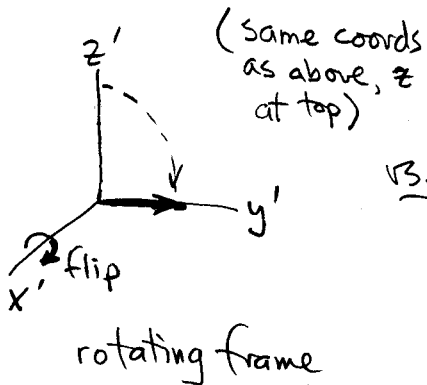
$$= B_1 \cdot e^{-i\omega t}$$

angle

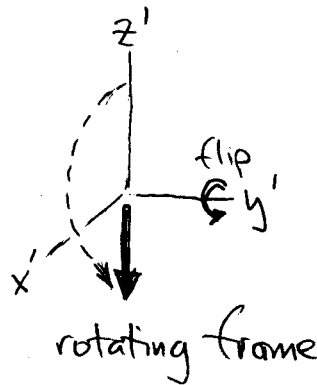


- in the rotating coordinate syst, flipping around x-axis vs. y-axis is just difference in phase of RF stim

typical 90° flip (around x-axis)



vs.



typical 180° flip (around opposite y-axis)

180° flip req's ~6X power of 90°

Bloch-3
SIGNAL EQUATION

one "voxel" for a particular (instant) in time vs. Bloch MxB which is change of M w/t

i.e., projection of mag. vector at each point onto coil magnetic field direction at each point, summed across object

$$\Phi(t) = \int_{obj} \vec{B}(\vec{r}) \cdot \vec{M}(\vec{r}, t) d\vec{r}$$

magnetic "flux" thru coil → scalar (integral mag. field perpendicular to area)

magn. field detected (= generated) by coil geometry at each point in object

local magnetization of object (time-dependent)

position: $\vec{r} \rightarrow x, y, z$

(const. retained in deriv)

- time deriv. inside
- use Bloch precess. soln
- [deriv. cos → -sin
deriv. sin → cos
[or using $e^{i\theta}$]
 $\frac{d}{dt}(e^{i\omega t}) = i\omega e^{i\omega t}$
mult by $i \rightarrow$ add 90°

$$V(t) = - \frac{\partial \Phi(t)}{\partial t} = - \frac{\partial}{\partial t} \int_{obj} \vec{B}(\vec{r}) \cdot \vec{M}(\vec{r}, t) d\vec{r}$$

Faraday law of Induction

- evaluate using free precession eqs. (solution to Bloch) ignoring relaxation
- rewrite w/ complex notation w/ time-dependence from lab frame Bloch

- ignore change in z-comp. \vec{M} because so slow → i.e., we only see M_{xy} , not M_z
- substitute $\vec{M}(t)$ with lab frame $\vec{M}_{xy}(t) = \underbrace{M_{xy}(0)}_{\text{complex}} e^{i\gamma z} e^{-i\omega_0 t}$
- simplify:
 - 1) ignore decay (assume this $t=0$) → so equals 1 (scalar)
 - 2) assume phase-sensitive detection [Sw (difference from ω_0) → rotating frame! makes data complex]

omit receive and init excite flip phase offsets

$$\vec{S}(t) = \int_{obj} \vec{B}_{xy}(\vec{r}) M_{xy}(\vec{r}, 0) e^{-i\delta\omega(\vec{r})t} d\vec{r}$$

complex: $2 \sqrt{V(t)}$

Laboratory frame Bloch solutions:
 $M_z \rightarrow$ same
 $M_T = M_{xy}(0) e^{i\gamma z} e^{-i\omega_0 t}$

demodulate

spatially-dependent resonant freq in rotating frame — i.e. after subtraction of $\omega_0 = \gamma B_0$

even from one coil!

assume homogeneous (ignore)

lab frame transverse magnetization at time $t=0$

ω_0 subtracted off by PSD

sum across object

M_{xy} is now scalar, direction is here

$\omega_0 = \text{freq} = \text{radians/sec}$
 $\omega = \omega_0 + \delta\omega$
 $\omega t = \text{angle}$
 $(\omega_0 + \delta\omega)t = \text{angle}$
 $\omega_0 t + \phi = \text{angle}$
gradients $B_1, \Delta B_0$

$$\vec{S}(t) = \int_{obj} M_{xy}(\vec{r}, 0) e^{-i\delta\omega(\vec{r})t} d\vec{r}$$

standard signal expression

i.e., at a single time point, RF signal is vector sum across object of local transverse magnetization vectors

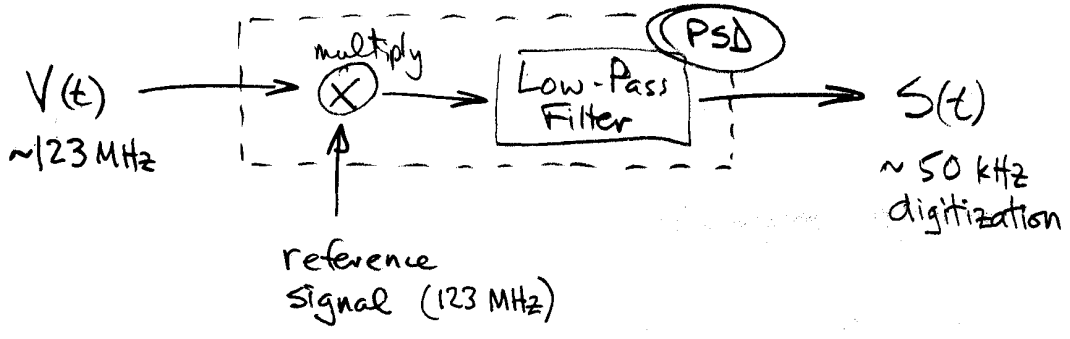
phase angle in rotating frame

$\omega t = \frac{\text{radians}}{\text{sec}} \times \text{sec} = \text{radians} (\phi = \int \omega dt)$
getting difference converts lab → rotating

Block-4

PHASE-SENSITIVE DETECTION

how we get rotating frame



- method for moving very high frequency Larmor oscillations down to tractable frequency range

demodulated signal \propto RF coil signal \cdot reference (transmitter)

$$\propto \sin[(\omega_0 + \delta\omega)t] \cdot \sin[\omega_0 t]$$

$\propto \frac{1}{2} [\cos \delta\omega t - \cos (2\omega_0 + \delta\omega)t]$

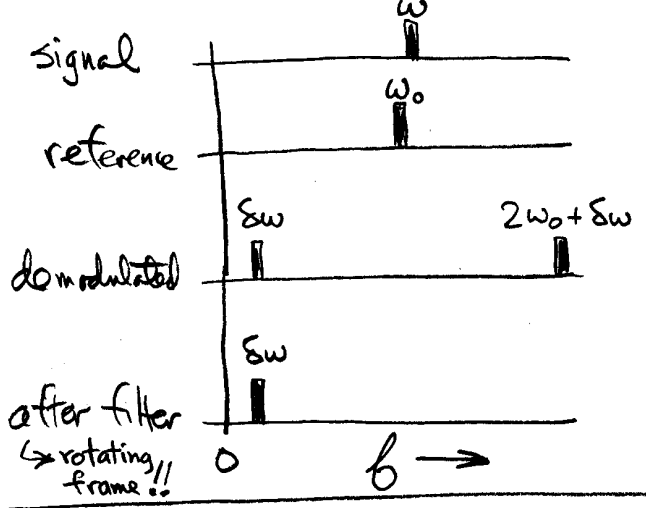
trig identity: $\sin a \sin b = \frac{1}{2} [\cos(a-b) - \cos(a+b)]$
 $\sin a \cos b = \frac{1}{2} [\sin(a-b) + \sin(a+b)]$

this signal is digitized

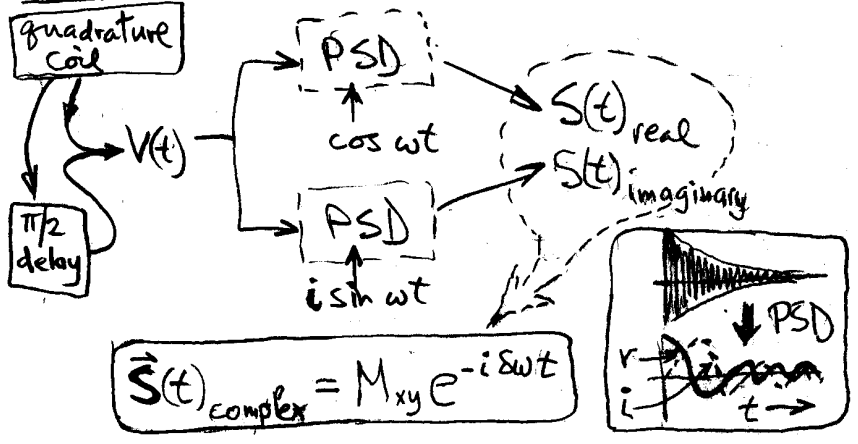
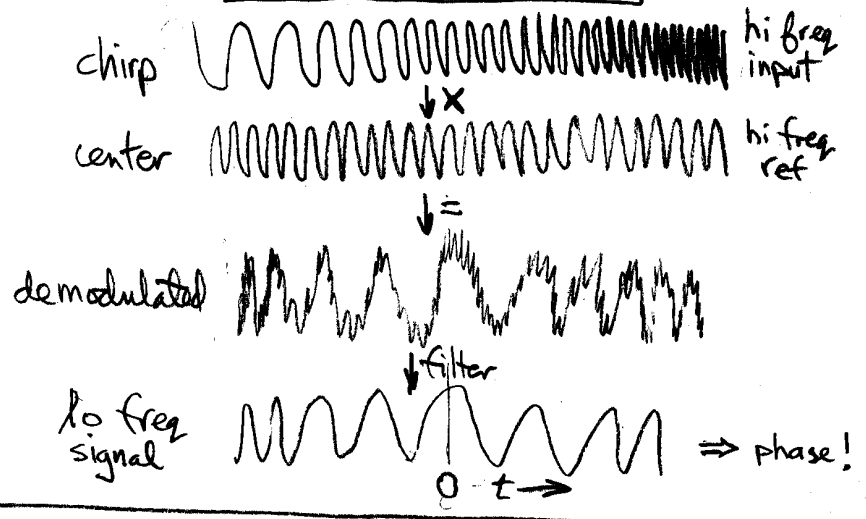
freq diff between RF input & ref

filter this one out w/ low pass filter

one freq - freq domain



chirp - time domain



- two signals are made from a single receiving RF coil
- a quadrature coil can be treated the same way (OK to combine after adding $\pi/2$ phase, then PSD)
- quadrature coil has better S/N since noise in each part is uncorrelated ($\sqrt{2}$ better)

echoes-1
FID - FREE INDUCTION DECAY, T_2^*

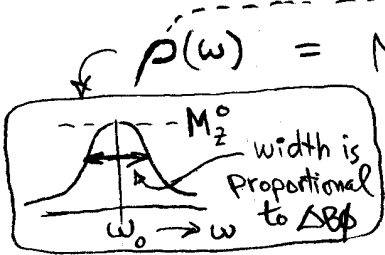
T_2 - unrecoverable (= rapid)
 T_2^* - add recoverable (= rapid + static)

- Signal (FID) resulting from RF pulse w/ angle α

$$\vec{S}(t) = \int_{-\infty}^{\infty} \underbrace{\sin \alpha}_{\text{amount of tip}} \underbrace{\rho(\omega)}_{\text{spectral density funct.}} \cdot \underbrace{e^{-t/T_2(\omega)}}_{\text{time-dep decay}} \cdot \underbrace{e^{-i\omega t}}_{\text{rapid oscillations}} \cdot \underbrace{d\omega}_{\text{incr freq.}}$$

ignore space in obj

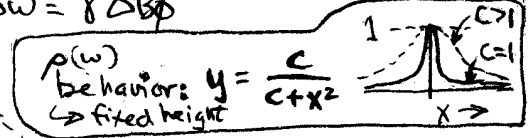
- An example spectral density ("Lorentzian inhomogeneity")



$\omega = \gamma B \phi$ (Bloch)
 $\Delta \omega = \gamma \Delta B \phi$

[subst $\rho(\omega)$, rearrange to extract ω_0 , take integral]

all atoms assumed to interact in same way in freq. range under curve



$$\vec{S}(t) = \underbrace{\pi}_{\text{complex signal}} \cdot \underbrace{M_z^0}_{\text{from integral of } \frac{1}{c^2 + \omega^2}} \cdot \underbrace{\gamma \Delta B \phi}_{\Delta \omega \text{ (big } \Delta \rightarrow \text{big sig.) (b/c fixed height) flip}} \cdot \underbrace{\sin \alpha}_{\text{flip}} \cdot \underbrace{e^{-t/\gamma \Delta B \phi}}_{\text{extra decay from static (big } \Delta \rightarrow \text{big decay)}} \cdot \underbrace{e^{-t/T_2}}_{\text{regular } T_2 \text{ decay}} \cdot \underbrace{e^{-i\omega_0 t}}_{\text{oscillations (complex) (one freq!)}}$$

[combine T_2 + static terms]

$$\vec{S}(t) = \pi \cdot M_z^0 \cdot \gamma \Delta B \phi \cdot \sin \alpha \cdot e^{-t/T_2^*} \cdot e^{-i\omega_0 t}$$

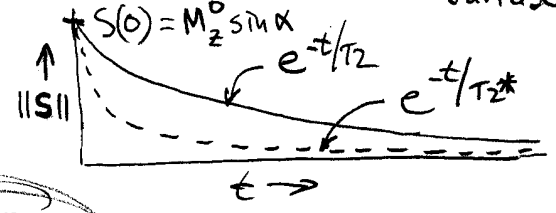
N.B. center freq., not original integration variable

$$\frac{1}{T_2^*} = \frac{1}{T_2} + \frac{1}{T_2'}$$

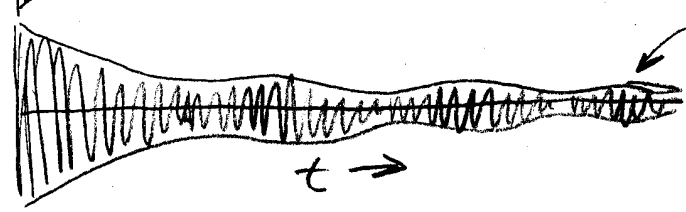
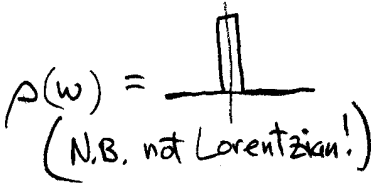
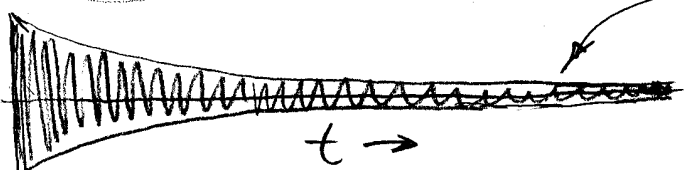
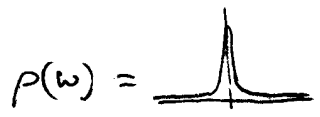
T_2' e.g. extra decay from BOLD

overall decay rate including inhomogeneous $B \phi$

unrecoverable "intrinsic" spin-spin → recoverable "static" → echo can cancel/fix!



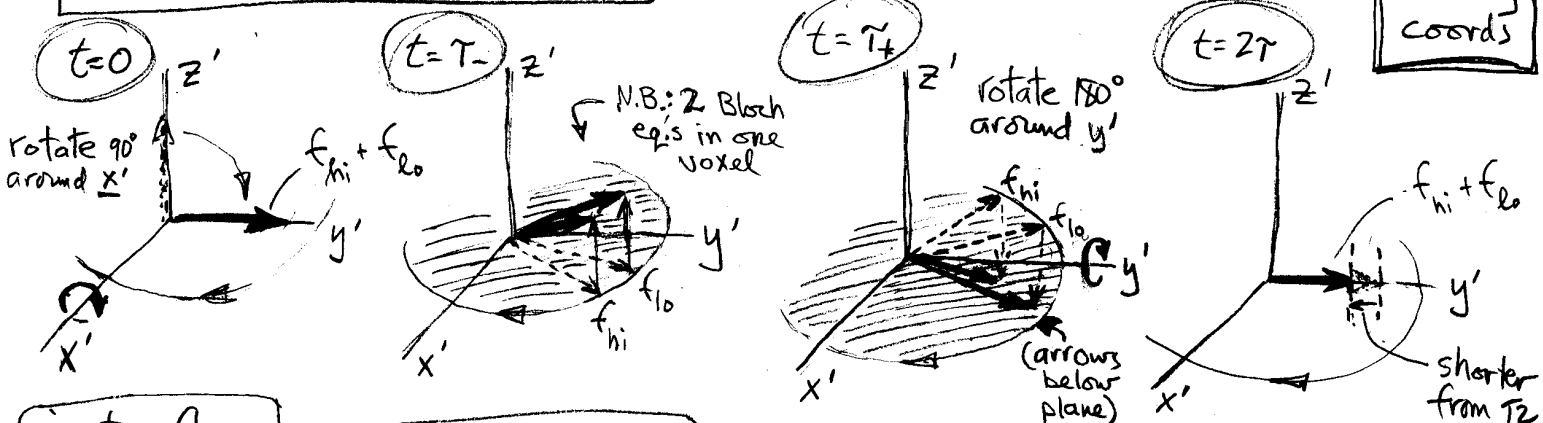
suggestive, since 100 million cycles per second
 N.B. complex → (r, i)



ECHOES — spin echo

$90^\circ - \tau - 180^\circ, T_2/T_2^* \neq \text{echo}$

rotating coords



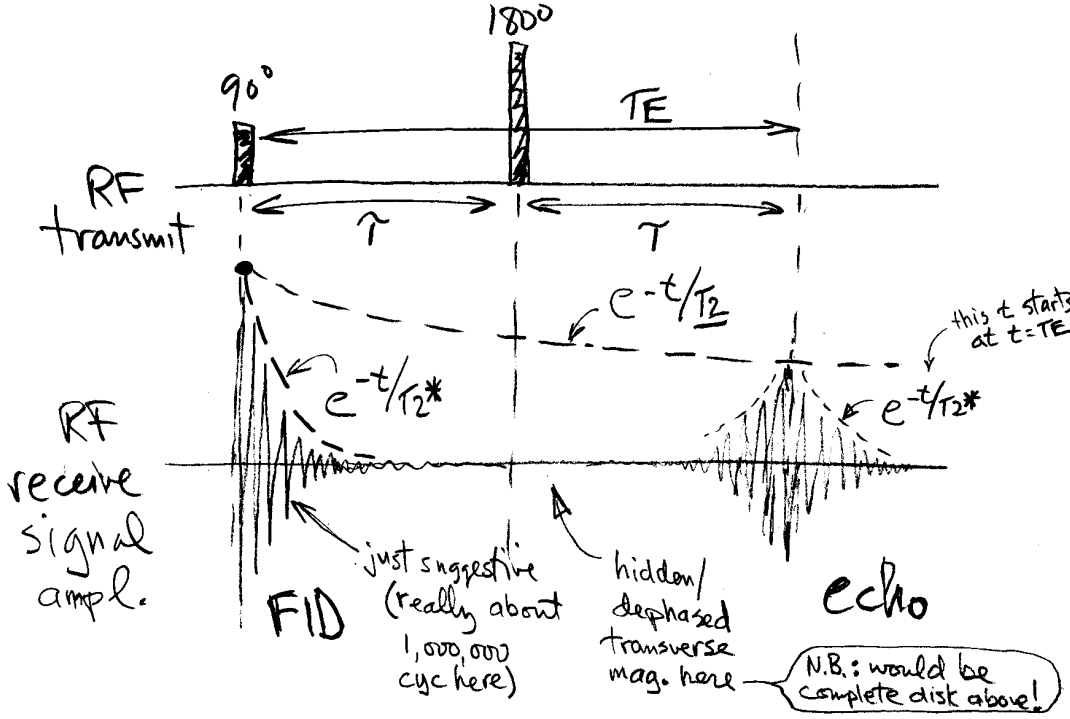
just after $90^\circ x'$ pulse $f_{lo} + f_{hi}$ have same phase

relaxation + phase dispersion of $f_{lo} + f_{hi}$ (both from $B > B_0$)

just after $180^\circ y'$ pulse (y' pulse like x' pulse but RF has $+90^\circ$ phase)

echo caused by re-phasing of $f_{lo} + f_{hi}$ (w/decay due to T_2)

- remember [brief RF just tips vectors while retaining length relaxation includes tips and shrinks (M_T) and grows (M_z , echo)]
- $180^\circ x'$ pulse works, too, but echo will have $+\pi$ phase (left side in figs above)
- echo generated even if second pulse not 180° (see next)



- FID decay (and echo growth/decay) described by T_2^* , from inhomogeneity
- reduction in height of echo compared to initial described by T_2 , echo fixes the "star"

echoes-3

ECHOES — spin echo

$\alpha_1 - \tau - \alpha_2 - \tau$ (both pulses along y' for simplicity)

effect of α_y pulse → see $\hat{R}_y(\alpha)$

general transforms (operators)

indicates rotating coord system

effect of τ delay → see $\hat{R}_z(\alpha)$

slow precession in rotating coords

decay

$$\begin{aligned} M_{x'} &\rightarrow M_{x'} \cos \alpha - M_{z'} \sin \alpha \\ M_{y'} &\rightarrow M_{y'} \\ M_{z'} &\rightarrow M_{x'} \sin \alpha + M_{z'} \cos \alpha \end{aligned}$$

↳ (etc for α_x, α_z)

$$\begin{aligned} M_{x'} &\rightarrow (M_{x'} \cos \omega \tau + M_{y'} \sin \omega \tau) e^{-\tau/T_2} \\ M_{y'} &\rightarrow (-M_{x'} \sin \omega \tau + M_{y'} \cos \omega \tau) e^{-\tau/T_2} \\ M_{z'} &\rightarrow M_z^0 (1 - e^{-\tau/T_1}) + M_z^0 e^{-\tau/T_1} \end{aligned}$$

immediately after α_1 pulse

$$\begin{aligned} M_{x'}(\omega, 0_+) &= -M_z^0(\omega) \sin \alpha_1 \\ M_{y'}(\omega, 0_+) &= 0 \\ M_{z'}(\omega, 0_+) &= M_z^0(\omega) \cos \alpha_1 \end{aligned}$$

for one isochromat of freq. ω

after τ delay

$$\begin{aligned} M_{x'}(\omega, \tau) &= -M_z^0(\omega) \sin \alpha_1 \cos \omega \tau e^{-\tau/T_2} \\ M_{y'}(\omega, \tau) &= M_z^0(\omega) \sin \alpha_1 \sin \omega \tau e^{-\tau/T_2} \\ M_{z'}(\omega, \tau) &= M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \end{aligned}$$

immediately after α_2 pulse (no effect on $M_{y'}$; rewrite y' ; combine x and y eqs)

$$\begin{aligned} M_{x'y'}(\omega, \tau_+) &= M_z^0(\omega) \sin \alpha_1 \left(\sin^2 \frac{\alpha_2}{2} e^{-i\omega \tau} - \cos^2 \frac{\alpha_2}{2} e^{i\omega \tau} \right) e^{-\tau/T_2} \\ &\quad - M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \sin \alpha_2 \end{aligned}$$

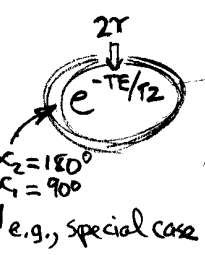
* time dependent free precession around z' (rewrite $M_{x'y'}(\omega, \tau_+)$)

$$\begin{aligned} M_{x'y'}(\omega, t) &= M_{x'y'}(\omega, \tau_+) e^{-(t-\tau)/T_2} e^{-i\omega(t-\tau)} \\ &= M_z^0(\omega) \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-t/T_2} e^{-i\omega(t-2\tau)} \\ &\quad - M_z^0(\omega) \sin \alpha_1 \cos^2 \frac{\alpha_2}{2} e^{-t/T_2} e^{-i\omega t} \\ &\quad - M_z^0(\omega) [1 - (1 - \cos \alpha_1) e^{-\tau/T_1}] \sin \alpha_2 e^{-(t-\tau)/T_2} e^{-i\omega(t-\tau)} \end{aligned}$$

terms
 ①
 ②
 ③

- for a large num of freq's:

[terms ② & ③ are dephasing → FID of echo
 term ① rephasing → rephase at $t = 2\tau$]



echo signal from ①

$$S(t) = \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-t/T_2(\omega)} e^{-i\omega(t-TE)} d\omega$$

↓ $t=TE$

peak ampl

$$A_E = \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-TE/T_2(\omega)} d\omega = M_z^0 \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-TE/T_2}$$

- * $90_y - \tau - 90_y$ $S_1(t) = \frac{1}{2} \int_{-\infty}^{\infty} \rho(\omega) e^{-t/T_2} e^{-i\omega(t-TE)} d\omega$
- $90_y - \tau - 180_y$ $S_2(t) =$ no 1/2 factor
- $90_x - \tau - 180_y$ $S_2(t) =$ multiply by i → add $\pi/2$ phase → etc for $A_E \dots$ like ↑

(echo amplitude, ignoring freq dependence of T_2)

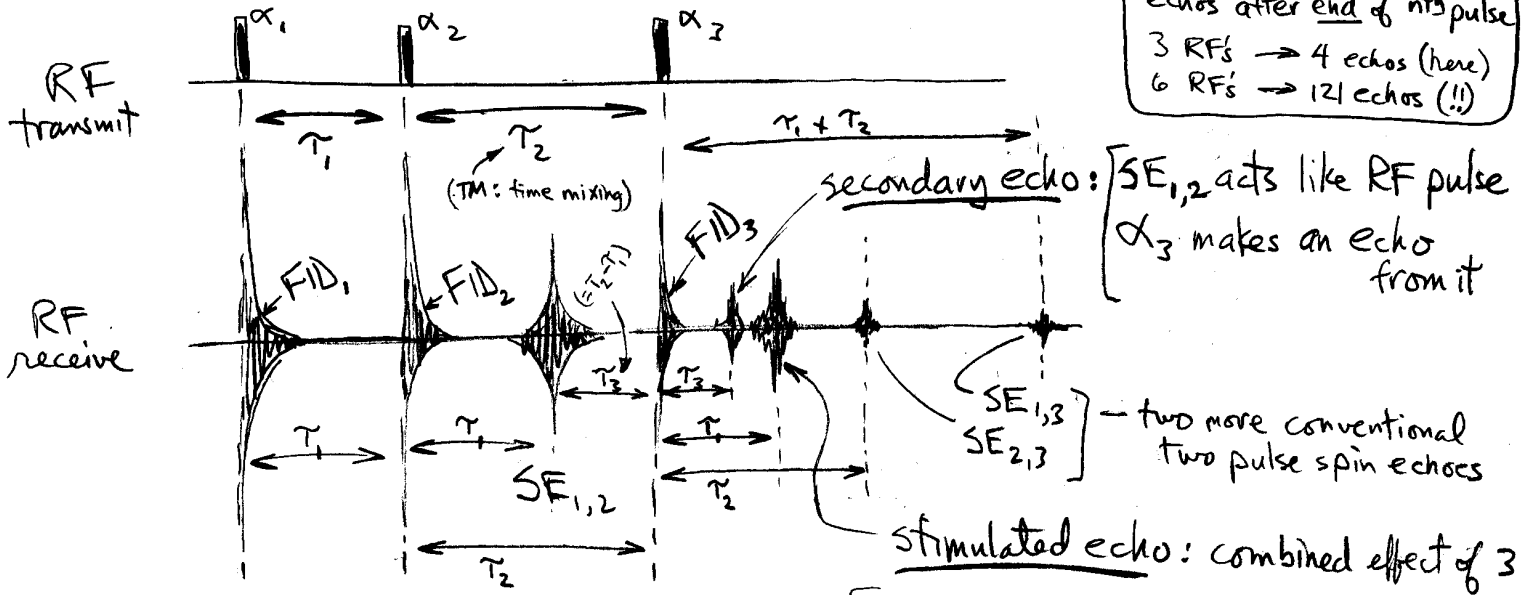
echos-4

ECHO TRAINS - spin-echo trains

- it's (too) easy to make echos...

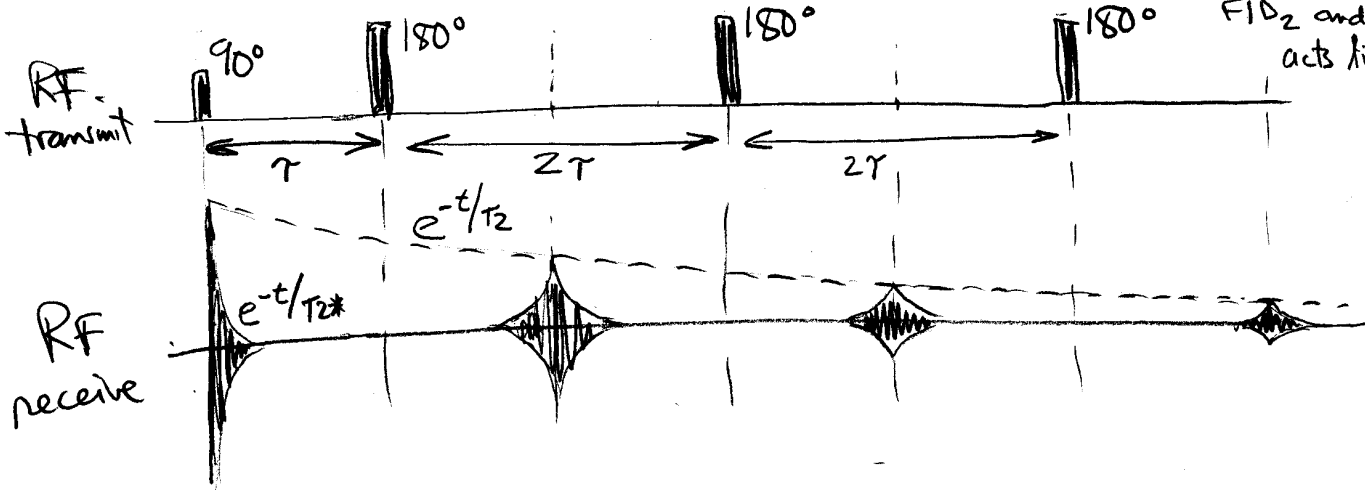
$$E_n = \frac{3^{(n-1)} - 1}{2}$$

echos after end of nth pulse
 3 RFs → 4 echos (here)
 6 RFs → 121 echos (!!)



- a useful multi-echo sequence (CPMG) is a 90° followed by 180° at 2τ spacing

α_1 : $M_L \rightarrow M_T$
 α_2 : leftover M_T flipped to M_L ("saved")
 α_3 : flip saved $M_L \rightarrow M_T$ which can then begin to cancel delays (after being held "in limbo" between FID₂ and FID₃); acts like 2-pulse echo



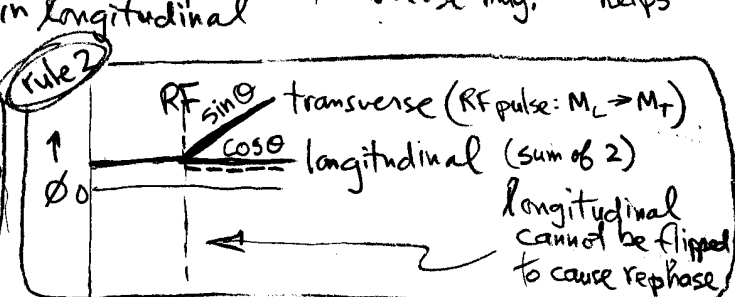
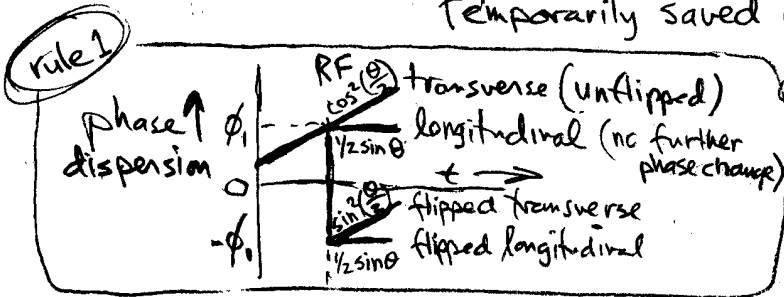
- typically, 90° and 180° applied in different axes (x', then y', y', y'...)
 which reduces phase errors due to imperfect 180° pulses (since slightly-off rotation around y' affects phase less)

EXTENDED PHASE GRAPHS

- using full Bloch eq. solutions is tedious 😊 (need 1000 copies)
- pictorial method for visualizing effects of a series of α pulses
- starting point: initial RF creates new transverse ↳ vs. easier to visualize 90/180°

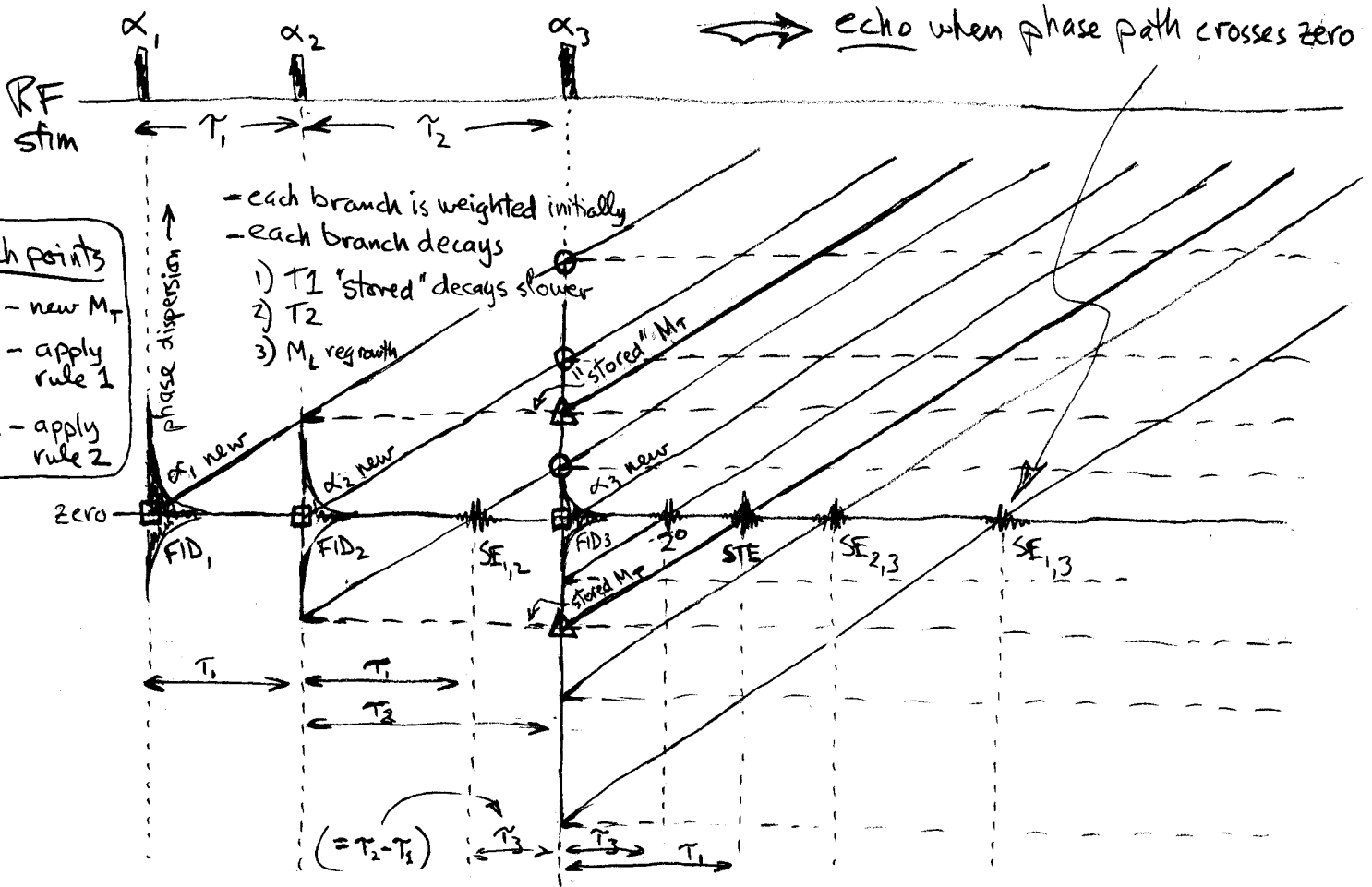
effects on existing α pulse rotates a portion of existing transverse mag. into a position that results in rephasing and another portion into M_L
 ↳ QM view helps

third pulse can uncover and rephase transverse mag. temporarily saved in longitudinal



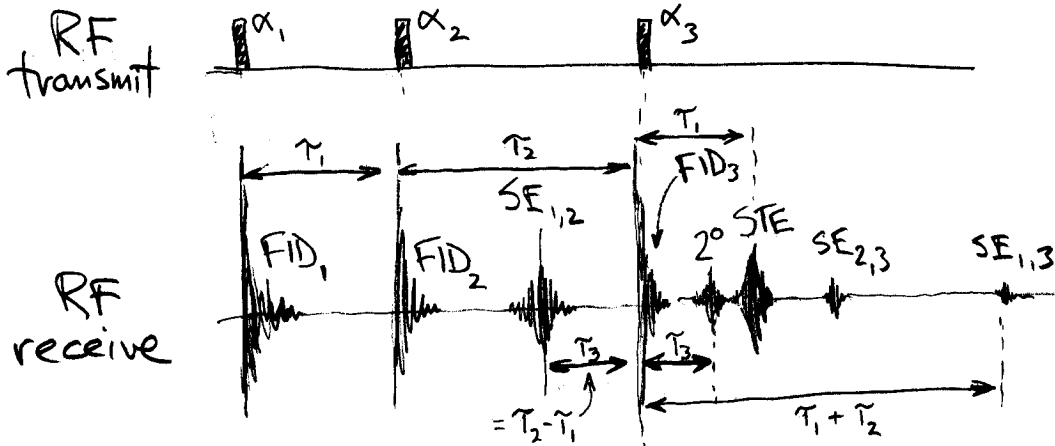
↳ branching rule for effect of α RF pulse on transverse mag

↳ branching rule for effect of α RF pulse on longitudinal mag



3-PULSE ECHO AMPLITUDES

- assume $M_z^0 = 1$



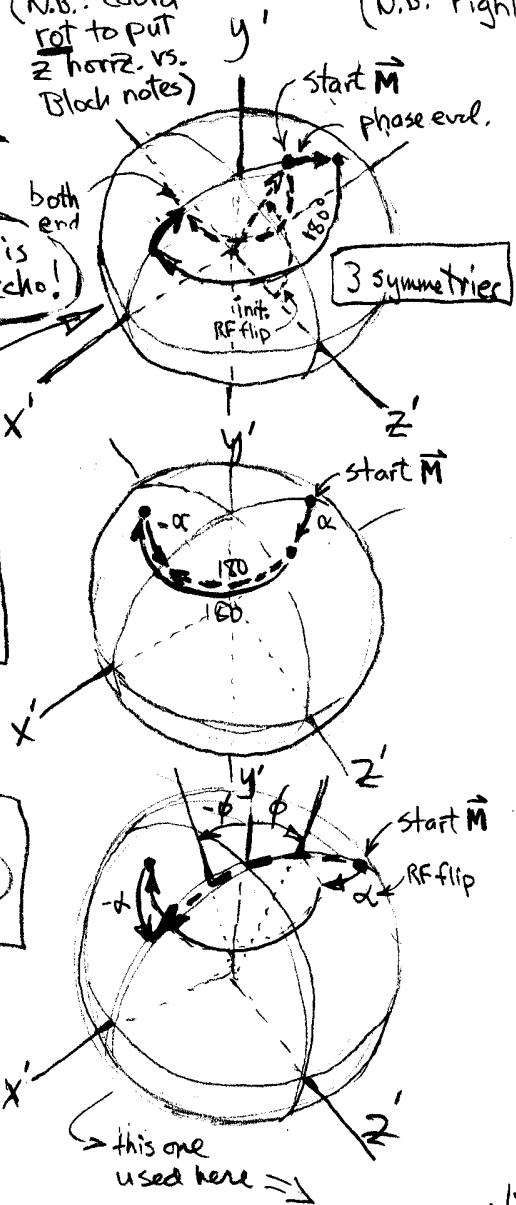
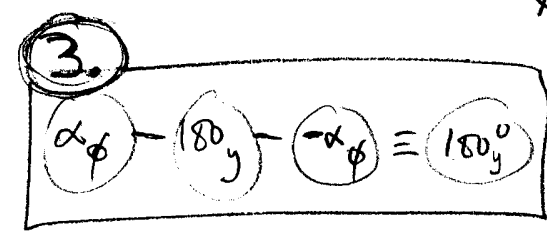
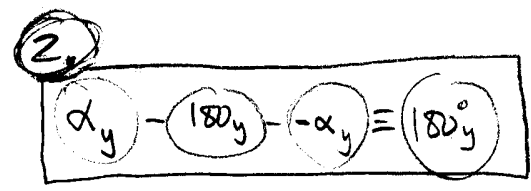
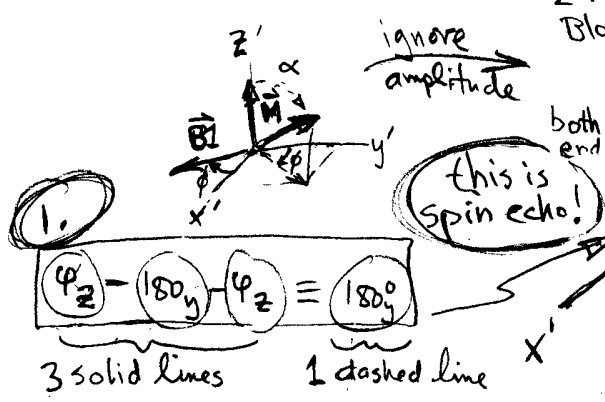
| echo | time | amplitude |
|----------------------------|--|---|
| $SE_{1,2}$ | $(t = 2\tau_1)$ | $\sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-2\tau_1/T_2}$ ↳ special cases |
| | | <div style="border: 1px solid black; display: inline-block; padding: 2px;">$\alpha_1 = 90^\circ, \alpha_2 = 180^\circ$</div> $e^{-2\tau_1/T_2}$ <div style="border: 1px solid black; display: inline-block; padding: 2px;">$2\alpha_1 = \alpha_2$</div> $\sin^3 \alpha_1 \cdot e^{-2\tau_1/T_2}$ |
| 2° ("secondary") | $(t = 2\tau_2)$ $(t = 2\tau_1 + 2\tau_3)$ | $-\sin \alpha_1 \sin^2 \frac{\alpha_2}{2} \sin^2 \frac{\alpha_3}{2} e^{-2\tau_2/T_2}$ |
| STE ("stimulated") | $(t = 2\tau_1 + \tau_2)$ | $\frac{1}{2} \sin \alpha_1 \sin \alpha_2 \sin \alpha_3 e^{-\tau_2/T_1} e^{2\tau_1/T_2}$ (N.B.: T1) |
| $SE_{2,3}$ | $(t = \tau_1 + 2\tau_2)$ | $[1 - (1 - \cos \alpha_1) e^{-\tau_1/T_1}] \sin \alpha_2 \sin^2 \frac{\alpha_3}{2} e^{-(\tau_1 + 2\tau_2)/T_2}$ (N.B.: T1) |
| $SE_{1,3}$ | $(t = 2(\tau_1 + \tau_2))$ | $\sin \alpha_1 \cos^2 \frac{\alpha_2}{2} \sin^2 \frac{\alpha_3}{2} e^{-2(\tau_1 + \tau_2)/T_2}$ |

- T1-dependence in STE (but also SE_{2,3}) from temporary "storage" of M_T in M_L, then recovery by third pulse

HYPER ECHOES

(N.B.: coord rot to put z horiz. vs. Bloch notes)

(N.B. right-handed coord syst vs. left-handed in Bloch eq. notes)

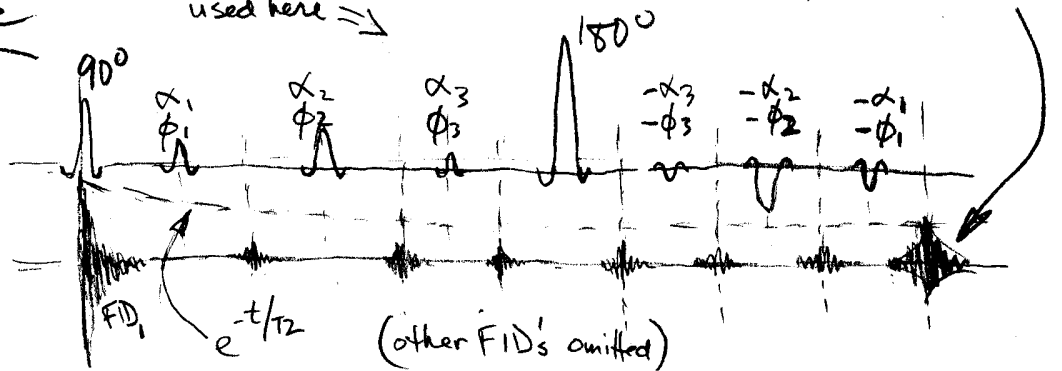


- Hennig & Scheffler (2001)
- normalize \vec{M} amplitude $\rightarrow 1$
- sphere surface defines 2D space for \vec{M} moved by:
 - 1) vect. rotation of \vec{M} around tilted axis in transverse x-y plane by RF with flip, α , and phase, $\phi = P(\alpha, \phi)$
 - 2) rotation around z by phase evolution due to freq offset, ω (B0 offset) and time, $t = \phi(\omega, t)$
- three symmetries:
 - Solid lines: phase evol or RF flip $\rightarrow 180^\circ \rightarrow$ phase evol or RF
 - Dashed lines: just 180° equiv.

- by combining long sequences observing these symmetries, can generate as strong echo even w/ many inserted α -pulses in between

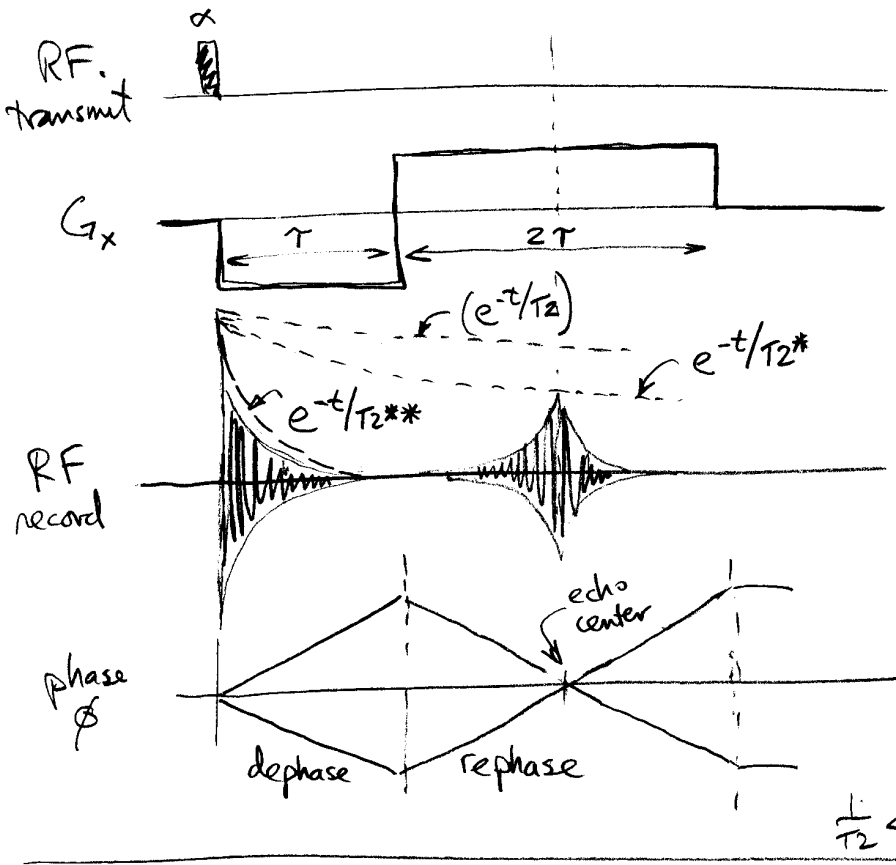
Practical use

- multi-echo example
- can also use to prepare, then separate read-out



- practical prob: 180° pulses deposit a lot of RF (6x 90°) \rightarrow prob at high fields
- by arranging to get big echo in middle of k-space can get by with much less RF power

GRADIENT ECHOES - T_2^* , GE chains



- initial negative gradient dephases spins

- after $t=T$ of positive gradient, spins rephase

- does not correct for T_2^* inhomogeneities so echo amplitude is

$$A_E = e^{-t/T_2^*}$$

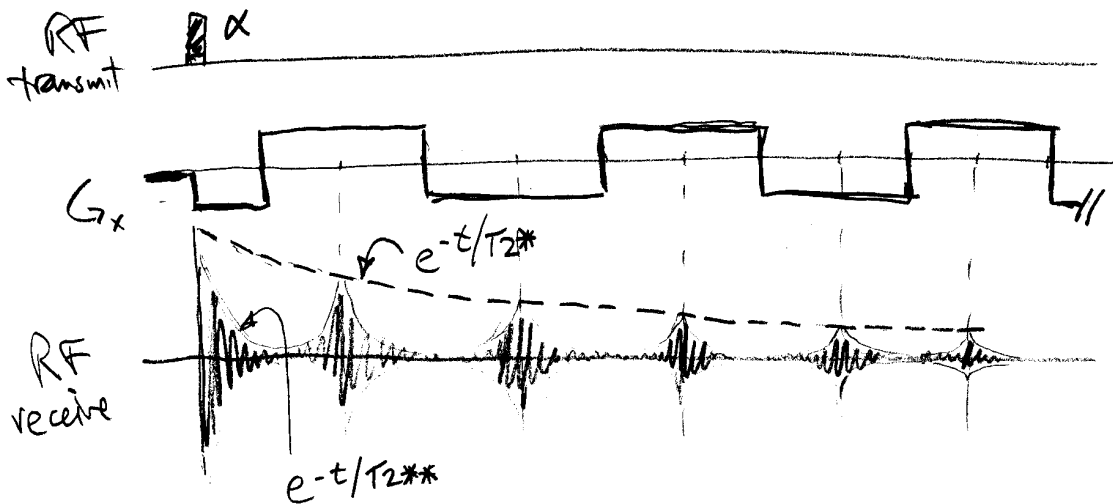
- the initial "FID" is not "free" since it is being actively de-phased by gradient, so FID decay

$$\frac{1}{T_2} < \frac{1}{T_2^*} < \frac{1}{T_2^{**}} \leftarrow A_E = e^{-t/T_2^{**}}$$

- key difference between spin-echo (SE) and gradient echo (GE) is that B_0 inhomogeneities not corrected

↳ hence, echoes are T_2^* -weighted, not T_2 -weighted \Rightarrow more susceptible to inhomogeneities

- echo trains possible w/ gradient echo (CPMG-like)



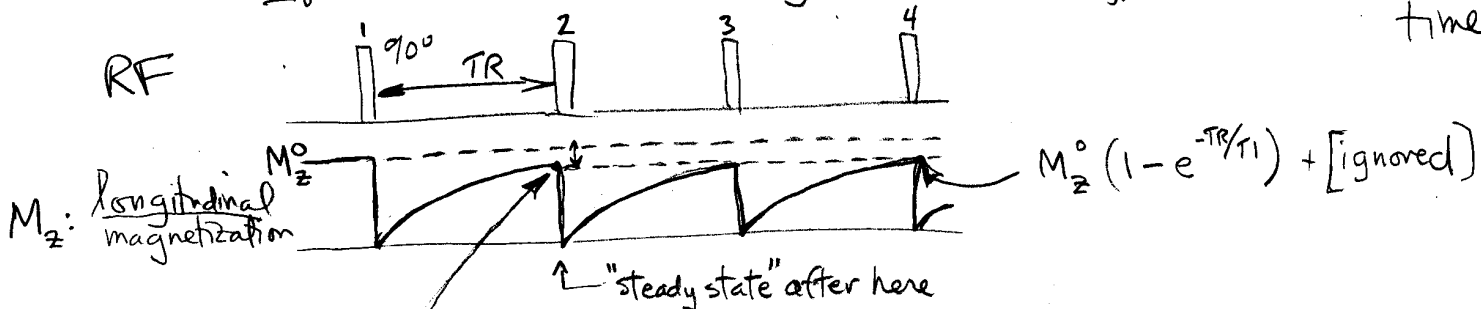
- the faster the gradients are switched, the more echoes you get

- EPI hardware \Rightarrow 64 echoes

IMAGE CONTRAST

T1 saturation-recovery (no echo, just FID)

- contrast (PD, T_1, T_2, T_2^*) depends on magnetization not getting back to equilibrium, and then differences in how far away each tissue type is at measurement time



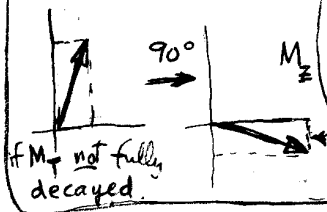
- simple saturation/recovery w/ no echo
- initial conditions: M_z before first pulse = M_z^0
 $M_z = 0$ immed. after first pulse (i.e., 90° pulse)

- from Bloch eq, M_z just before second pulse:

$$M_z^{(n)}(0_-) = \underbrace{M_z^{(0)}}_{M_z \text{ before current pulse}} \underbrace{\left(1 - e^{-\frac{TR}{T_1}}\right)}_{M_z \text{ "regrowth-from-zero" term}} + \underbrace{M_z^{(n-1)}(0_+) e^{-\frac{TR}{T_1}}}_{M_z \text{ "left-immed.-after-pulse" term (N.B. decaying)}}$$

- given $\begin{cases} (1) 90^\circ \text{ pulse} \\ (2) \text{ no } M_{xy} \text{ left} \end{cases} \rightarrow \text{pure tip: } M_{xy} = M_z$

assume this is 0 because we assume that M_{xy} (transverse) completely decayed so that a 90° pulse doesn't generate any initial longitudinal



* $M_z^{(n)}(0_-) = M_{x'y'}(0_+) = M_z^0 \left(1 - e^{-\frac{TR}{T_1}}\right)$

longitudinal mag just before pulse transverse we can record after pulse transverse mag depends on T1!

- that is, the not-completely-regrown longitudinal magnetization, which depends on T_1 , but which we cannot record, is completely converted to recordable transverse magnetization

assume immediate recording of signal

$$I(r) = \underbrace{C}_{\text{recon const.}} \underbrace{\rho(r)}_{\text{spectral dens}} \left(1 - e^{-\frac{TR}{T_1}(r)}\right)$$

spectral dens $\rho(r) \approx$ p. density: underlies equilb. M_z^0

Contrast-1b

IMAGE CONTRAST

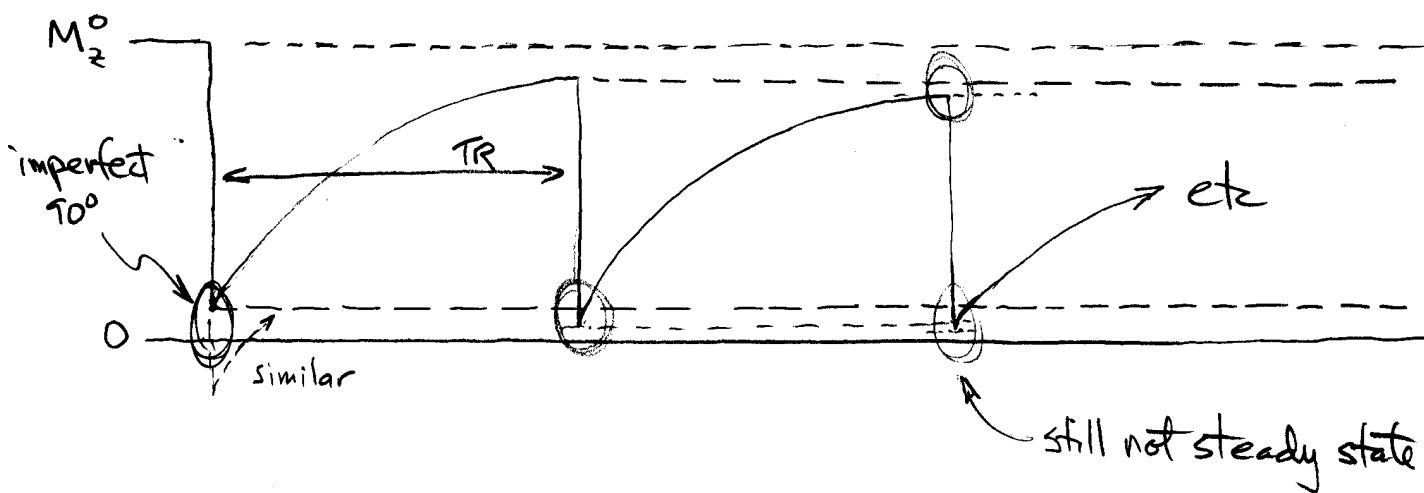
Why imperfect 90° takes multiple flips til steady state

- initial fMRI images are usually discarded (why?)

↳ because they are brighter than all the rest

↳ because multiple flip required before steady state

N.B.: B1 imperfections guarantee this situation will occur (e.g. at 3T, flip angle varies almost 25% across brain)



- at 3T, steady state for typical 1-2 sec TR images reached after ~8 images

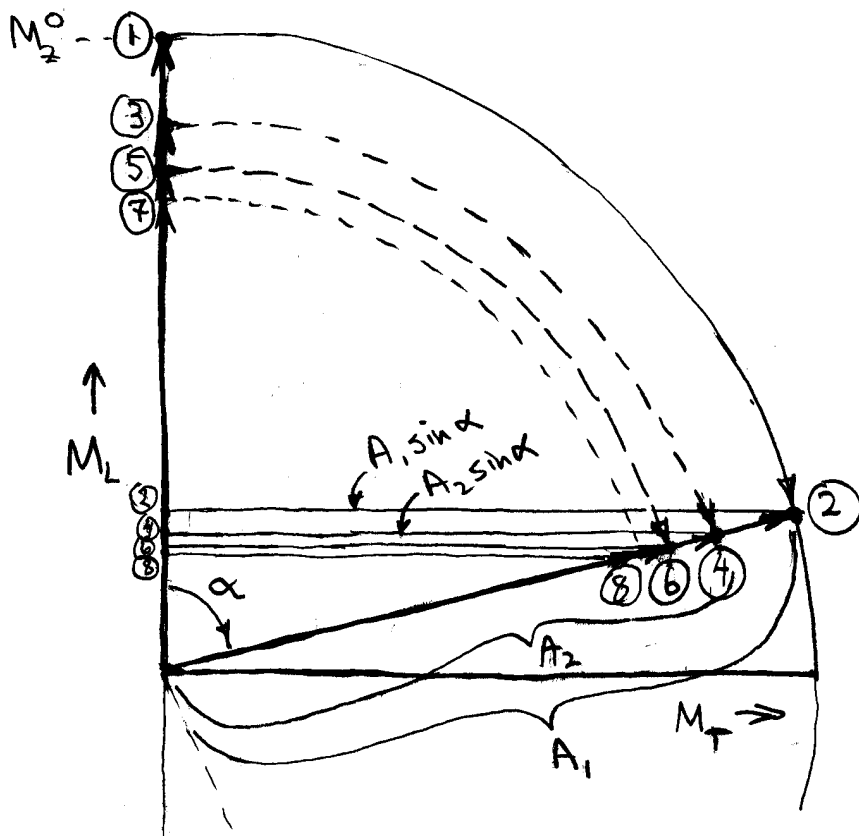
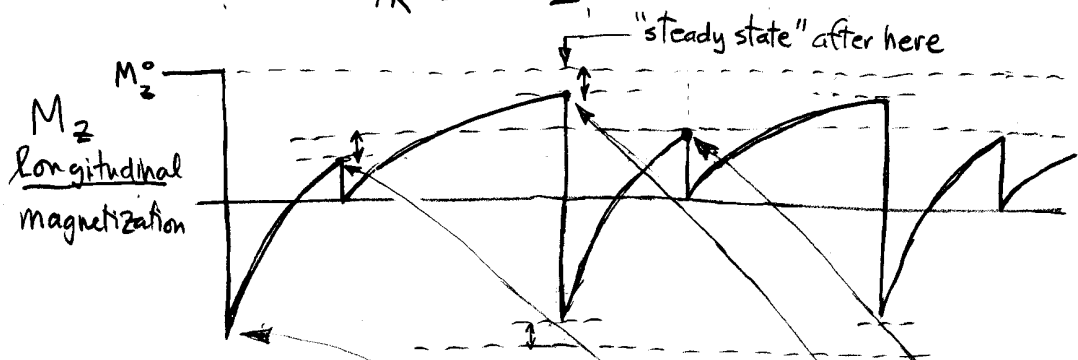
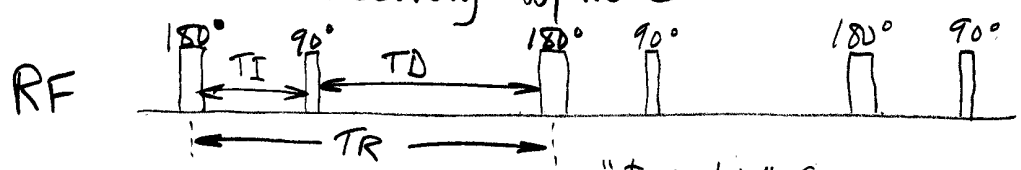


IMAGE CONTRAST IR (still just saturation-recovery - no echo)

- inversion recovery w/ no echo



- 180 deg pulse reverses longitudinal magnetization

$$M_z^{(0)} = -M_z^0$$

- recovery to end of first TI from long. part of Bloch eq.

$$M_z' = M_z^0 (1 - 2e^{-t/T_1}) \rightarrow \text{flipped into transverse by second pulse (1st 90)}$$

from 180°, since $-M_z$ in second Bloch term

- longitudinal then regrows from zero \rightarrow ignore!

$$M_z' = M_z^0 (1 - e^{-(TR-TI)/T_1})$$

from first Bloch term only

- after second 180°, just change sign again

$$M_z' = -M_z^0 (1 - e^{-(TR-TI)/T_1})$$

2nd Bloch term

- apply relaxation eq. again

$$M_z' = M_z^0 (1 - e^{-TI/T_1}) - M_z^0 (1 - e^{-(TR-TI)/T_1}) e^{-TI/T_1}$$

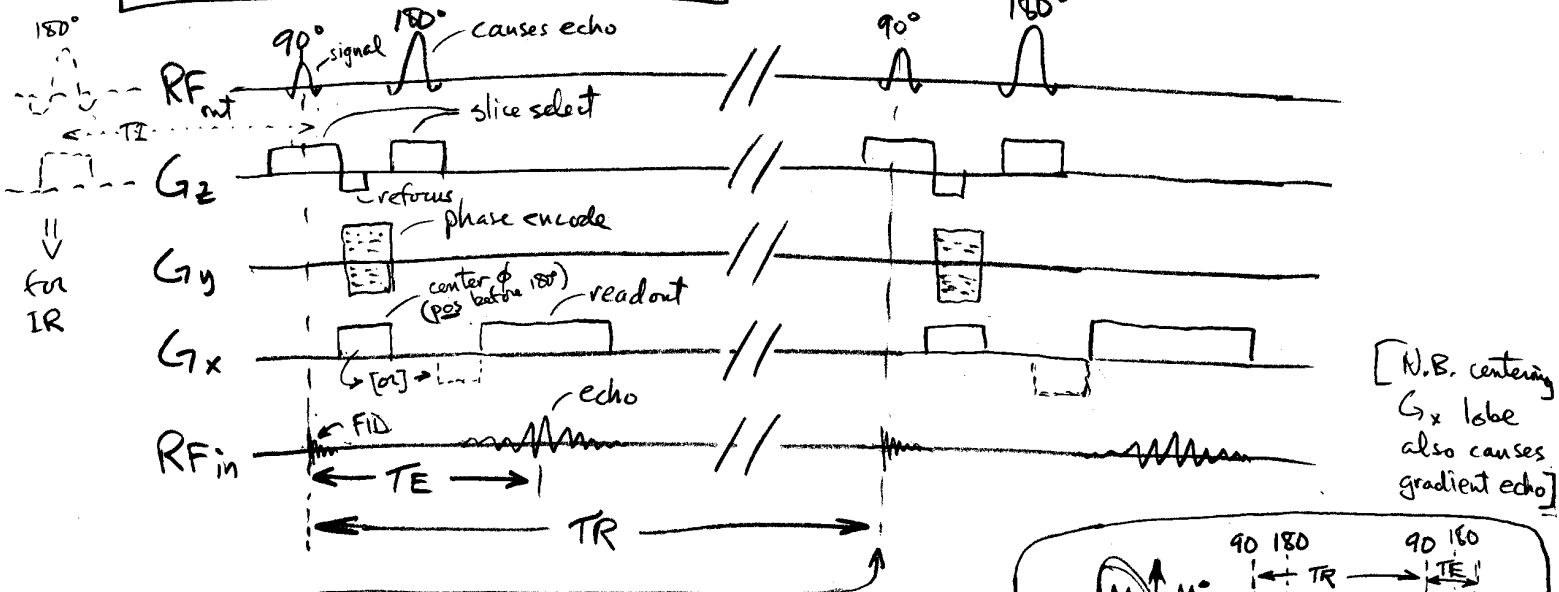
$$* M_z' = M_z^0 (1 - 2e^{-TI/T_1} + e^{-TR/T_1})$$

\rightarrow this is magnetization flipped to transverse, therefore made recordable

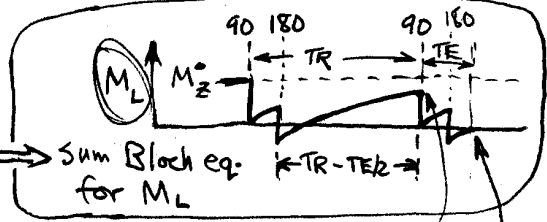
Contrast - 3

IMAGE CONTRAST

SE, IR-SE



- steady state mag (2nd TR) just before 90° ⇒



$$M_z'(0_-) = M_z^0 (1 - 2e^{-(TR-TE/2)/T_1} + e^{-TR/T_1})$$

- the echo signal (M_T) unlike in simple saturation-recovery FID has an additional delay before it is recorded, so we have to take account of transverse mag relaxation

$$A_E = M_z^0 (1 - 2e^{-(TR-TE/2)/T_1} + e^{-TR/T_1}) e^{-TE/T_2}$$

from spin echo equation hell

- if we assume TE much less than TR, then we can simplify:

$$A_E = M_z^0 (1 - e^{-TR/T_1}) e^{-TE/T_2}$$

* amplitude echo proton density TR controls T₁ contrast TE controls T₂ contrast

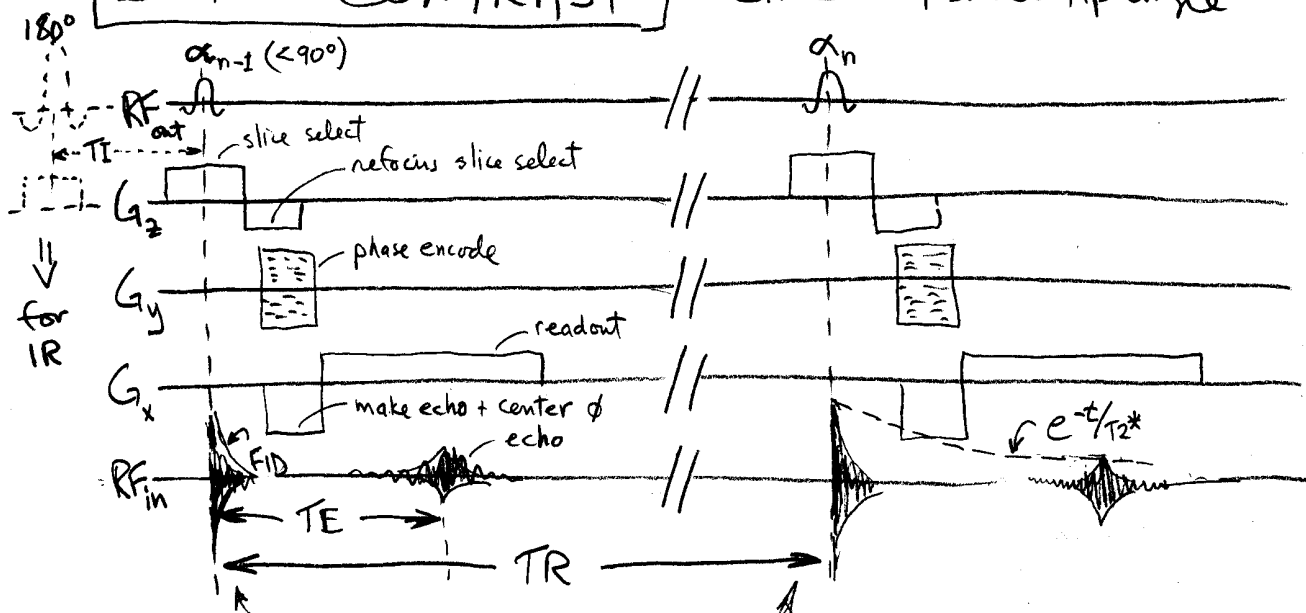
↳ TR - TE ≈ TR

- similar equation for SE-IR

$$A_E = M_z^0 (1 - 2e^{-TI/T_1} + e^{-TR/T_1}) e^{-TE/T_2}$$

Contrast-4

IMAGE CONTRAST GRE w/ small tip angle



- use basic longitudinal relaxation from Bloch eq, again
 \hookrightarrow \neq assume $M_{x'y'}^{(n)}(0_-) = 0 \rightarrow$ transverse dephased before next pulse

$$M_{z'}^{(n)}(0_-) = M_z^0 (1 - e^{-TR/T_1}) + M_{z'}^{(n-1)}(0_+) e^{-TR/T_1} \quad \text{long TR or spoiler}$$

- assume we have a small tip angle:

$$M_z \cos \alpha \Rightarrow M_{z'}^{(n)}(0_+) = M_z^{(n)}(0_-) \cos \alpha$$

$$M_{z'}^{(n)}(0_-) = M_z^0 (1 - e^{-TR/T_1}) + M_{z'}^{(n-1)}(0_-) \cos \alpha e^{-TR/T_1}$$

- assume we are in dynamic equilibrium: (current = previous)

$$M_{z'}^{(n)}(0_-) = M_{z'}^{(n-1)}(0_-) = M_{z'}^{ss}(0_-)$$

steady state:
 - subst. into prev. eq
 - solve for it

prepulse steady state longitudinal

$$M_{z'}^{ss}(0_-) = \frac{M_z^0 (1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}}$$

$$\begin{aligned} M_{ss} &= M_0 + M_{ss} \cos \alpha \\ M_{ss} - M_{ss} \cos \alpha &= M_0 \\ M_{ss} (1 - \cos \alpha) &= M_0 \\ M_{ss} &= M_0 / (1 - \cos \alpha) \end{aligned}$$

post-pulse transverse magnetization

$$M_{x'y'}^{ss}(t) = \frac{M_z^0 (1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}} \cdot \sin \alpha e^{-t/T_2^*}$$



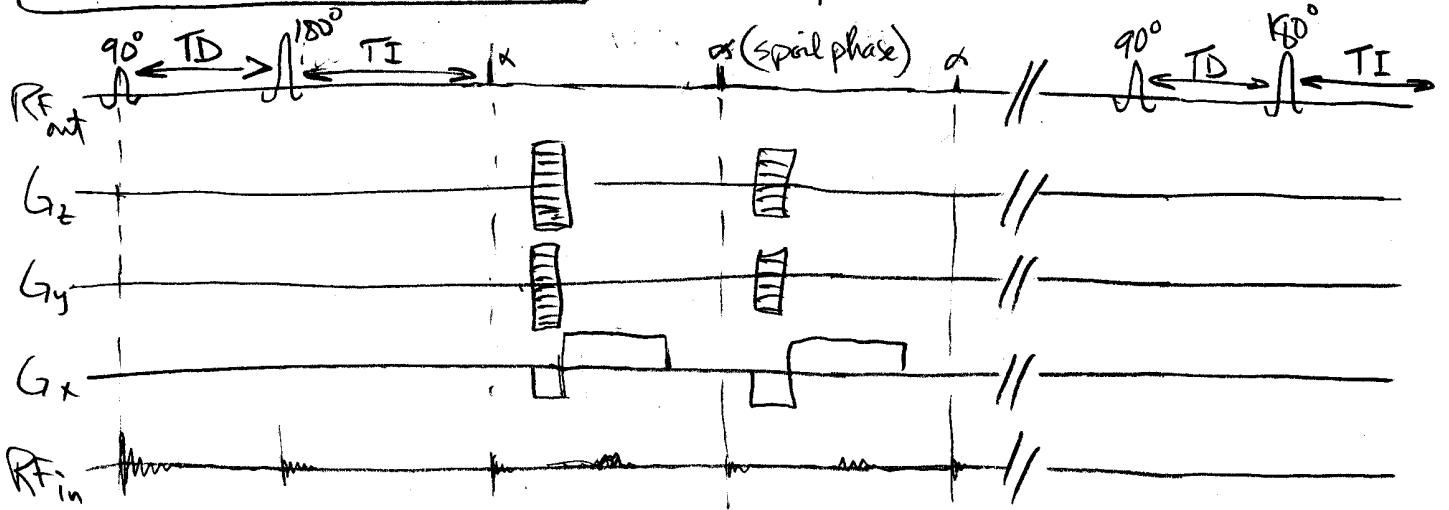
gradient echo amplitude

$$A_E = \frac{M_z^0 (1 - e^{-TR/T_1})}{1 - \cos \alpha e^{-TR/T_1}} \sin \alpha e^{-TE/T_2^*} \quad \text{from gradient echo}$$

T_1 contrast mainly depends on flip angle, not TR $\rightarrow \cos 90^\circ = 1 \rightarrow$ eliminates T_1 weight since denom = numer

Contrast - 4b

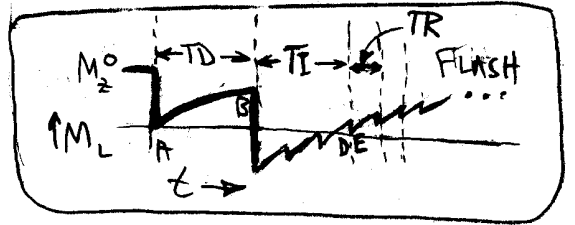
IMAGE CONTRAST MDEFT / 3D FLASH



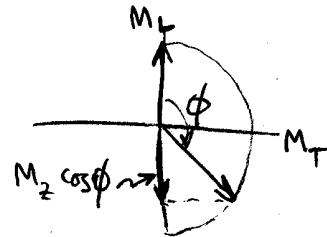
- saturate, wait for contrast₁, invert, wait for contrast₂, FLASH (center out)

A) M_z' (just after 90°) = 0 (perfect 90°)

B) M_z' (after TD) = $M_z^0 (1 - e^{-TD/T_2})$ (Bloch term #1)



C) M_z' (just after invert) = $\cos \phi M_z^0 (1 - e^{-TD/T_2})$



D) M_z' (after TI) = $M_z^0 (1 - e^{-TI/T_2}) + [\cos \phi M_z^0 (1 - e^{-TD/T_2})] e^{-TI/T_2}$

= $M_z^0 [1 - [1 - \cos \phi (1 - e^{-TD/T_2})] e^{-TI/T_2}]$ after preparation

Special case $TI \equiv TD$: $M_z^0 [1 - e^{-TI/T_2}]^2$

↳ using hard 180° 'inversion' can cancel hard alpha B1 inhomogeneities (Thomas et al. '05)

- after the first α pulse:

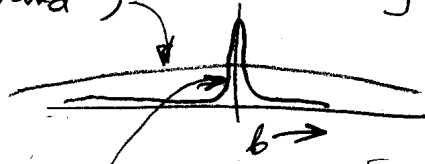
E) M_z' (just after first α) = $M_z^0 [1 - [1 - \cos \phi (1 - e^{-TD/T_2})] e^{-TI/T_2}] \sin \alpha$

contrast-4c

MAGNETIZATION TRANSFER CONTRAST

- protons in macromolecules & bound to membranes have wide range of resonant freqs ("bound") } → T₂ = 1 msec

v3.



↳ i.e. signal but invisible w/ usual TE

- free protons in blood, CSF, water have narrow range of resonant freqs ("free") } → T₂ = 50 msec

- mag transfer pulse sequence

1) off center freq pulse to hit "bound" (but don't hit water too hard)

2) wait for magnetization transfer from saturated longitudinal M_L of "bound" → M_L of "free"

3) result of transfer → attenuation

yes: WM, cartilage, muscle
no: blood, CSF, fat

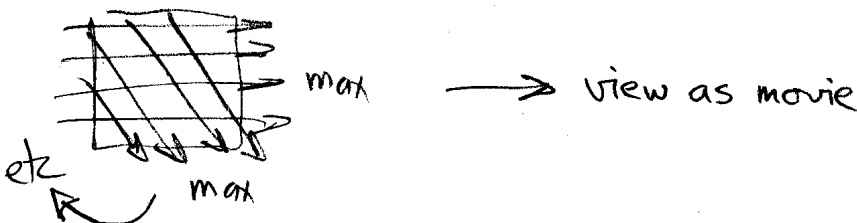
↳ N.B. this always happens a little (cf. T₁-weighted, T₂-weighted) something to keep in mind if hard pulse (wide freq)

- used to increase contrast in TOF

TOF (not explained) bright vessels from inflow fresh spins

MT - contrast added: suppress tissue but not blood

- view w/ MIP: maximum intensity projection along lines



contrast-5
SIGNAL-TO-NOISE, CONTRAST-TO-NOISE

- signal-to-noise defined as: $SNR \equiv \frac{\overline{S}}{\sigma_n}$ (avg obj signal / s.d. non-object region)
- temporal SNR: $tSNR \equiv \frac{\sum_{i=1}^N S_i}{\sigma_n}$
- "Contrast" is a difference
- contrast-to-noise ratio:

$C_{AB} \equiv \overline{S}_A - \overline{S}_B$
 (eg., WM-GM [activated-rest])

$CNR_{AB} \equiv \frac{C_{AB}}{\sigma_n} = \frac{\overline{S}_A - \overline{S}_B}{\sigma_n} = SNR_A - SNR_B$

Haacke

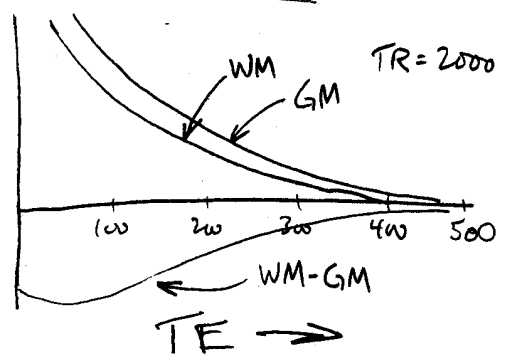
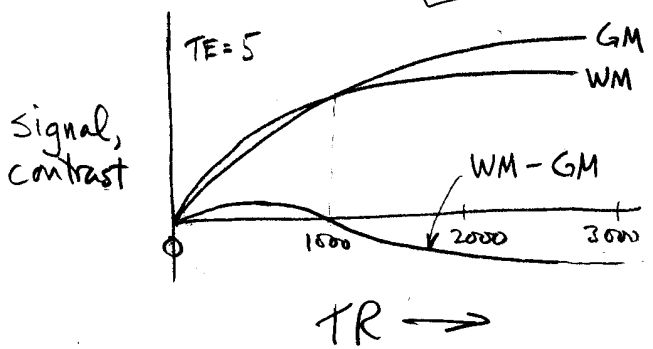
| Tissue | T1 (1.5T) | | PD |
|--------|-----------|---------|-------|
| | T1 | T2 | |
| GM | 950 | 100 | 0.80 |
| WM | 600 | 80 | 0.65 |
| CSF | 4500 | 2200 | 1.00 |
| blood | 1200 | 100-200 | water |

Lauterbur

| Tissue | T1 | | PD |
|--------|------|-----|------|
| | T1 | T2 | |
| GM | 760 | 77 | 0.69 |
| WM | 510 | 67 | 0.61 |
| CSF | 2650 | 280 | 1.00 |

- spin-echo:

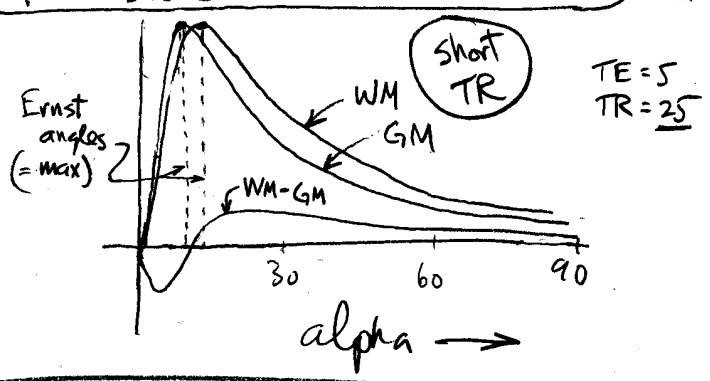
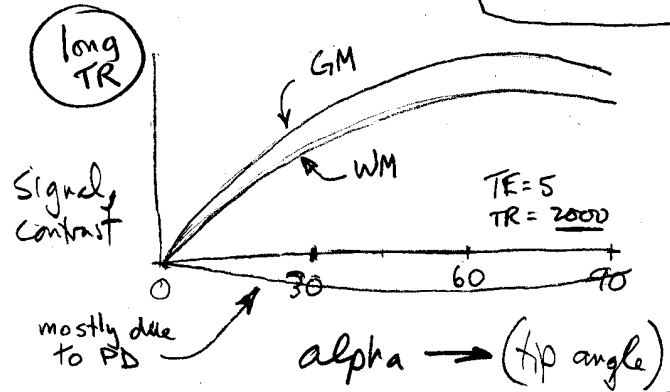
$A_E = M_z^0 (1 - e^{-TR/T1}) e^{-TE/T2}$



- gradient echo:

$A_E = \frac{M_z^0 (1 - e^{-TR/T1})}{1 - \cos \alpha} \sin \alpha e^{-TE/T2}$

1.5T
 $T2^*_{GM} = 50$
 $T2^*_{WM} = 40$



- general rules: spin-echo, long TR GE

| | | |
|-------------------------|-------------------------------------|---|
| proton-density weighted | TR $\uparrow\uparrow$ (no T1 diffs) | TE $\downarrow\downarrow$ (no T2 diffs) |
| T1-weighted | TR \approx T1 (big T1 diffs) | TE $\downarrow\downarrow$ (no T2 diffs) |
| T2-weighted | TR $\uparrow\uparrow$ (no T1 diffs) | TE \approx T2 (big T2 diffs) |

Contrast - 6

SIGNAL-TO-NOISE S/N

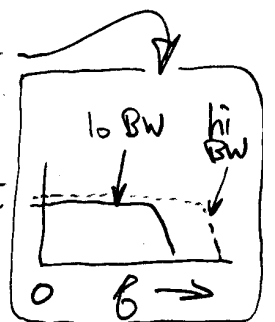
- generalized dependence of SNR on 3D imaging parameters

$$\text{SNR/voxel} \propto \underbrace{\Delta x \Delta y \Delta z}_{\substack{\text{voxel size} \\ \text{(of same number)}}} \underbrace{\sqrt{N_{acq}}}_{\substack{\text{num} \\ \text{repeats}}} \underbrace{N_x N_y N_z}_{\substack{\text{number of} \\ \text{voxels (of} \\ \text{same size)}}} \underbrace{\Delta t}_{\substack{\text{read} \\ \text{timestep}}}$$

- size (volume) of voxels (with the number of voxels held constant), linear effect on S/N
 - ↳ e.g., $3 \times 3 \times 3 \text{ mm} \rightarrow 4 \times 4 \times 4 \text{ mm} \rightarrow \frac{64}{27} = \underline{2.37 \text{ times better S/N}}$
- more voxels (with size of voxels, Δt per read step constant)
 - \sqrt{N} effect on S/N
 - ↳ e.g., $64 \times 64 \rightarrow 128 \times 128 \rightarrow \frac{\sqrt{128 \times 128}}{\sqrt{64 \times 64}} = \underline{2 \text{ times better S/N}}$
- # acquisitions \sqrt{N} better S/N
 - ↳ e.g., $1 \text{ acq} \rightarrow 2 \text{ acq} \rightarrow \frac{\sqrt{2}}{\sqrt{1}} = \underline{1.41 \text{ times better S/N}}$
- longer timestep during readout, $\sqrt{\Delta t}$ better S/N

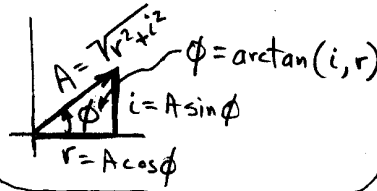
$\Delta t = \frac{1}{\text{BW}_{\text{read}}}$, digitization timestep during echo acquisition

- BW_{read} determined by cutoff freq, analog low pass filter
- Δt controls BW because low pass cutoff has to be set higher for smaller (higher freq-detecting) Δt
- must filter out freq's $> f_{\text{max}} = \frac{1}{2\Delta t}$ because they alias



fourier-0
COMPLEX ALGEBRA

- don't confuse freq, angle!
 $e^{-i\omega t}$
 makes linear var. into circular variable
 freq. x current = (lin. var.) / time
 angle (lin. var.)
 complex/circular var.

- how to convert:
 $(r, i) \leftrightarrow (A, \phi)$


real/imaginary

add: $(r_1, i_1) + (r_2, i_2) = (r_1 + r_2, i_1 + i_2)$
 mult: $(r_1, i_1) \times (r_2, i_2) = (r_1 r_2 - i_1 i_2, r_1 i_2 + i_1 r_2)$

ampl./phase

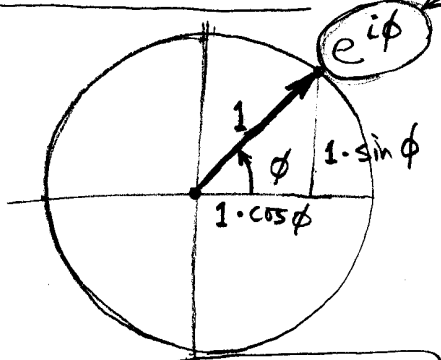
add: $(A_1, \phi_1) + (A_2, \phi_2) = (A_1 \cos \phi_1 + A_2 \cos \phi_2, A_1 \sin \phi_1 + A_2 \sin \phi_2)$
 multiply (commutative): $(A_1, \phi_1) \times (A_2, \phi_2) = (A_1 A_2, \phi_1 + \phi_2)$
 divide: $(A_1, \phi_1) \div (A_2, \phi_2) = (A_1/A_2, \phi_1 - \phi_2)$

N.B.: 3rd kind of vector mult. different than dot product and cross product (and G, A. non-commutative pseudoscalar multiply)

complex to real power: $(A, \phi)^n = (A^n, n\phi)$

the real "e" to "purely imaginary" power

$e^{i\phi} = \begin{cases} \text{expand as series} \\ \text{recognize cos, sin series} \end{cases}$
 $= \cos \phi + i \sin \phi$
 $= \cos \phi, \sin \phi$
 $= \text{vector on unit circle}$



shorthand for a unit vector (2D) pointing in the direction of phi

- for arbitrary amplitude, multiply $A e^{i\phi}$

- change in phase is freq
 $\frac{d\phi}{dt} = \omega$

- phase is integral of freq. variable
 $\phi = \int \omega dt$

Fourier transform

Convolution

$H(f) = \int_{-\infty}^{\infty} h(t) e^{-i2\pi f t} dt$
 $H(f) = \int_{-\infty}^{\infty} h(t) e^{i2\pi f t} dt$

$f(x) = g(x) * h(x) = \int_{-\infty}^{\infty} g(z) \cdot h(x-z) dz$
Cross-correlation
 $f(x) = g(x) \otimes h(x) = \int_{-\infty}^{\infty} g(z) \cdot h(x+z) dz$

Convolution Theorem

$F[g(x) \cdot h(x)] = G(k) * H(k)$

the Fourier transform of two functions multiplied by each other equals the convolution of the Fourier transform of each function

because of FFT, faster if kernel not small

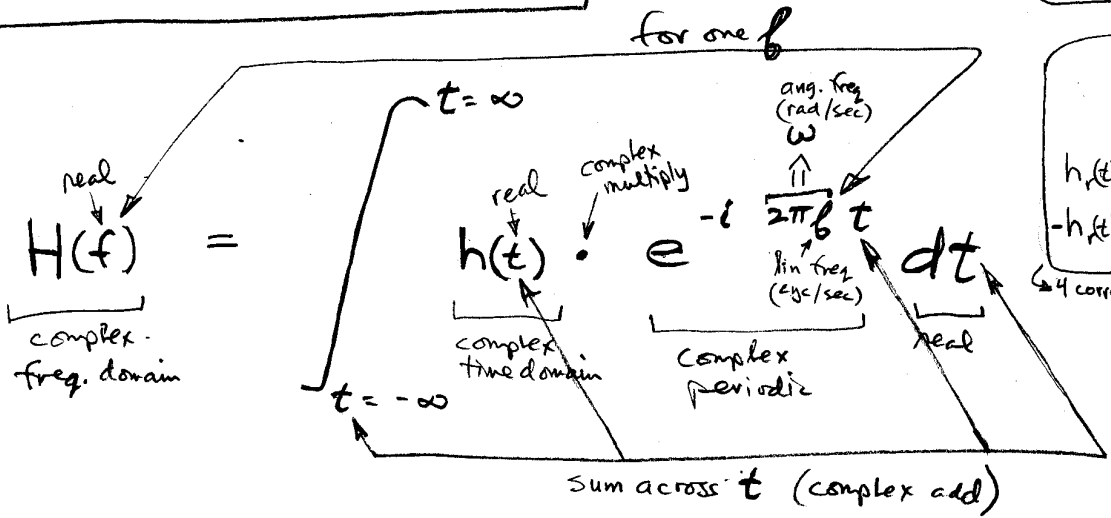
Fourier-1

Fourier transform (1)

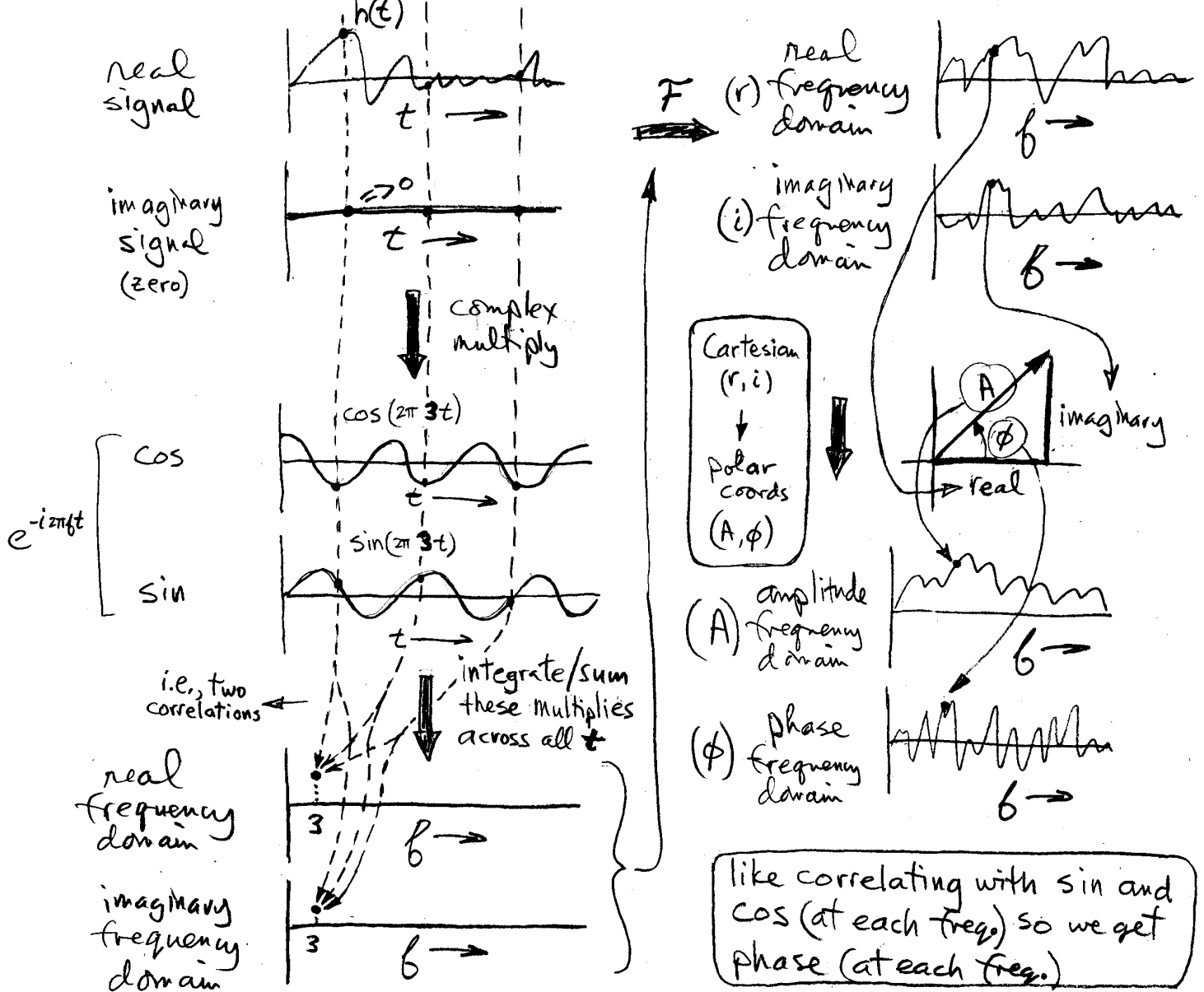
ft is a phase angle
 $b \cdot t = ft$
 cyc/sec \cdot sec = cyc

Fourier integral terms written out
 $h_r(t) \cos(2\pi ft) + h_i(t) \sin(2\pi ft)$
 $-h_r(t) \sin(2\pi ft) + h_i(t) \cos(2\pi ft)$
 ↳ 4 correlations

Fourier integral w/ real signal
 $h_r(t) \cos(2\pi ft)$
 $-h_r(t) \sin(2\pi ft)$
 ↳ 2 correlations



- How to calculate $H(f)$ for one f ($f=3$):
 (real signal: only need 2 correlations)



Fourier transform (1b)

- neg complex exponents/freq
- orthogonality

$$e^{i\phi} = \cos \phi + i \sin \phi$$

$$e^{-i\phi} = e^{i(-\phi)}$$

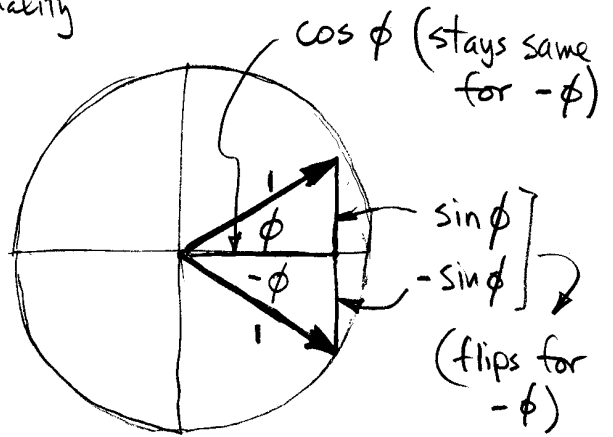
no effect (see below) →

→ move outside

$$= \cos(\phi) + i \sin(\phi)$$

$$= \cos \phi - i \sin \phi$$

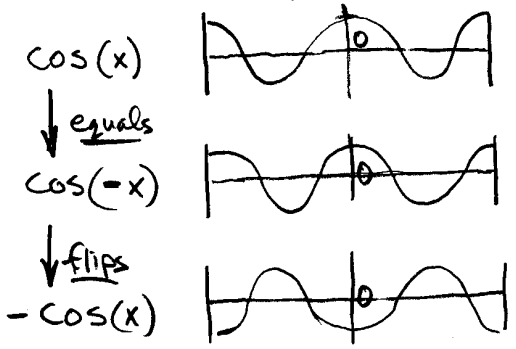
graphically



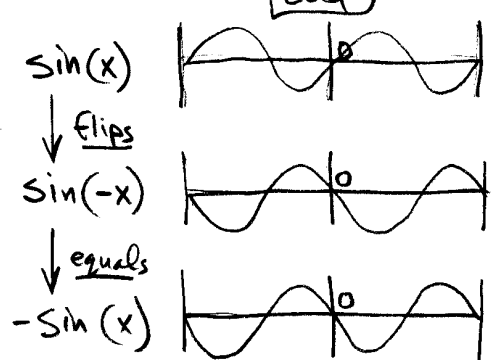
- cos is an "even" function, sin is an "odd" function

even

odd



if a function is mirror-symmetric along the x-axis around zero:
 $f(x) = f(-x)$
 it is even



An orthogonal decomposition

- think of discretely sampled $\sin(bx)$, $\cos(bx)$ as vectors
- $\text{Corr}(\vec{v}_1, \vec{v}_2) \equiv \text{projection of } v_1 \text{ onto } v_2 \equiv \vec{v}_1 \cdot \vec{v}_2$

$\text{Corr}(\cos b_1 x, \sin b_1 x) = 0$
 $= \sin \neq \cos$ of same frequency are orthogonal

$\text{Corr}(\sin b_1 x, \sin b_2 x) = 0$
 $=$ different integer freqs of sin (or cos) are orthogonal

$\text{Corr}(\cos b_1 x, \sin b_2 x) = 0$ [as above]

- in the continuous case, orthogonal functions defined as:

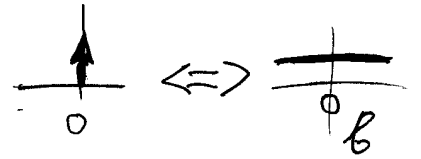
$$\int_{x=l_0}^{x=h_1} f(x) g(x) dx = 0$$

fourier-1c

UNDERSTANDING INVERSE FOURIER TRANSFORM AS ANOTHER CASE OF CORR W/ COS, SIN

- start with spike in image domain
- take example of spike at $x=0$

$\cos(x), \cos(2x), \cos(kx)$ all equal 1 there
all freq's correlate w/ spike at $x=0$



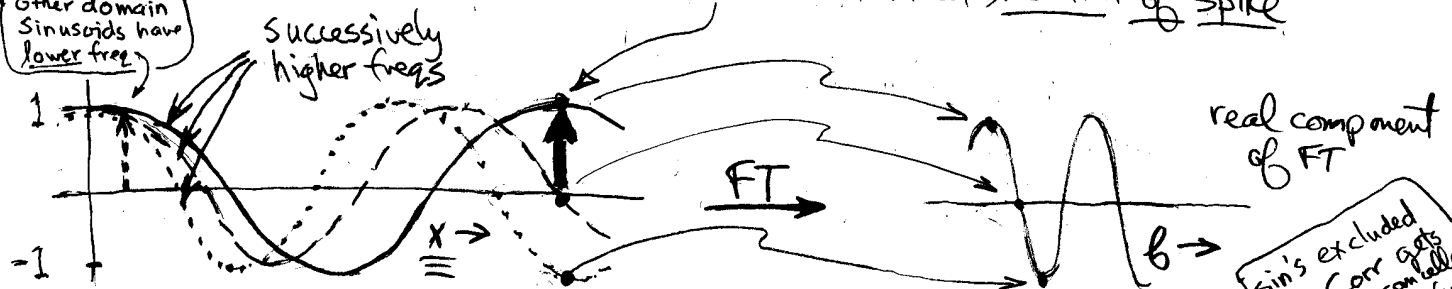
- if spike is moved away from zero, the frequency spectrum obtained by correlating cos with spikes oscillates

N.B. opposite direction sin spike are on imaginary axis



- to see why this is, since spike is all zero except at spike, the dot product for a given frequency only depends on the value of the $e^{-i2\pi kx}$ cos and sin at location of spike

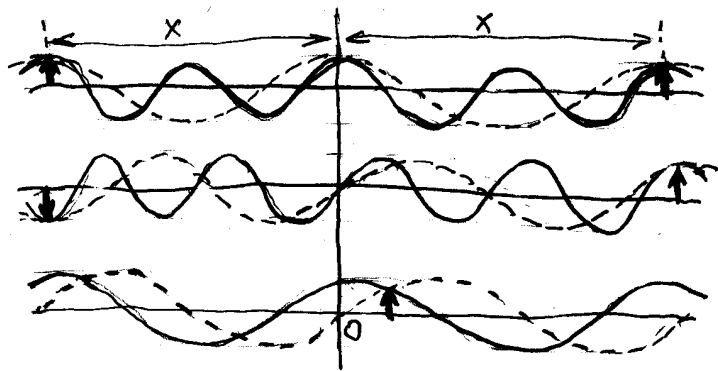
for spike here, other domain sinusoids have lower freq



real component of FT

sin's excluded sin corr gets exactly cancelled w/ odd func

- pos. pair (real) spikes same dist. from origin
- pos/neg. pair (imaginary) spikes, same dist. orig.
- one spike at distance from origin



- pick just "even" cos's (multiple freqs!)
now cancels even func
- pick just "odd" sin's (multiple freqs!)
- pick both sin's and cos's
(again oscillates in other domain as above)

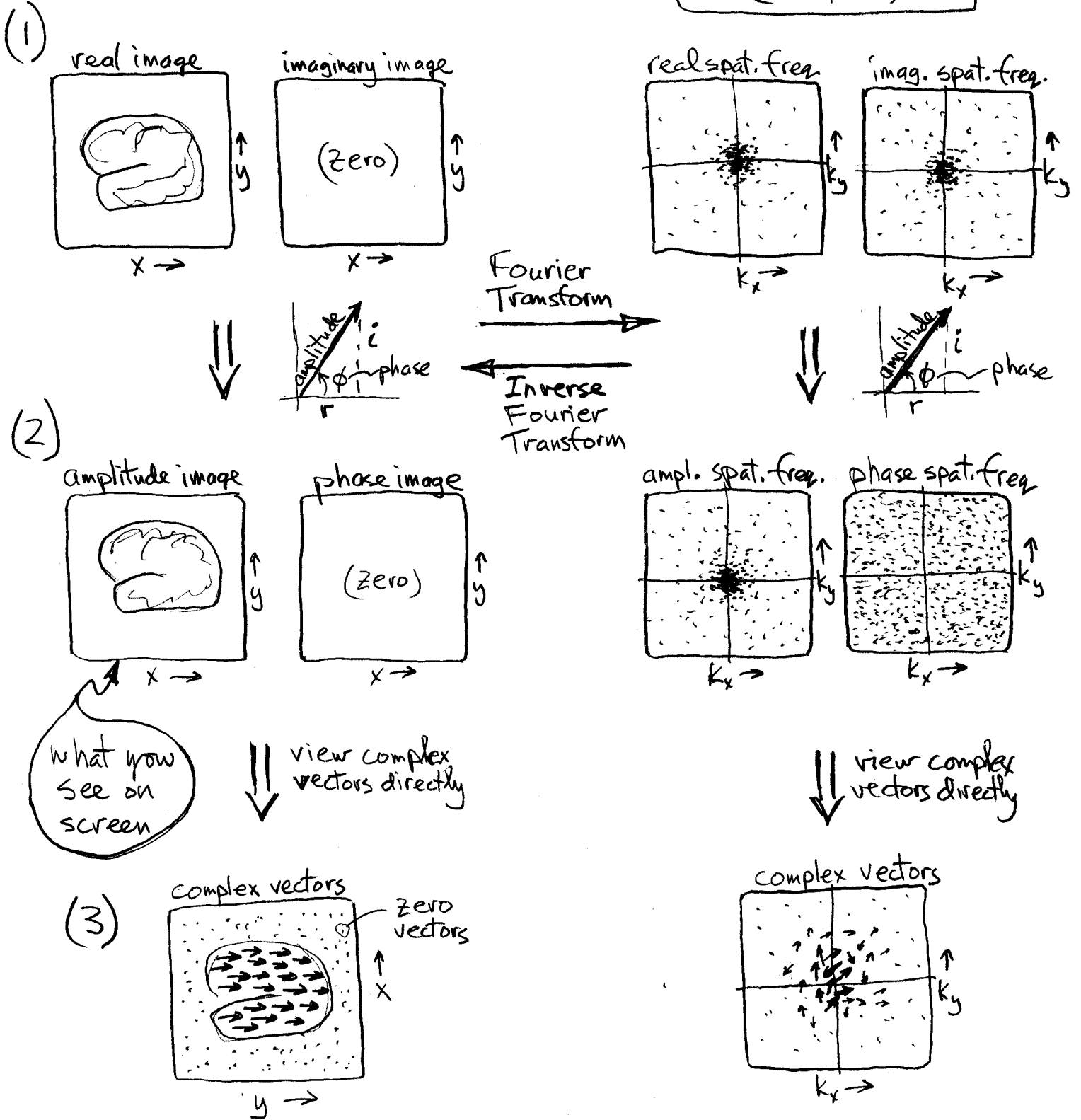
→ this is one way of thinking about what one point in k-space means, via correlating it w/ cos's, sin's to get periodic result in image space (inverse FT)

FOURIER TRANSFORM OF AN IMAGE (2)

IMAGE
(image space)



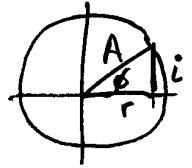
SPATIAL FREQ
(k-space)



-3 equivalent representations of image & spat. freq. space

Fourier-3

FOURIER TRANSFORM OF REAL IMAGE (3)



- what a single k -space point looks like (actually pair of points) for real image (polar coordinates A, ϕ instead of r, i)

image space

k -space (spatial freq. space)

offset of stripes is k -space phase

Brightness of stripes proportional to k -space amplitude

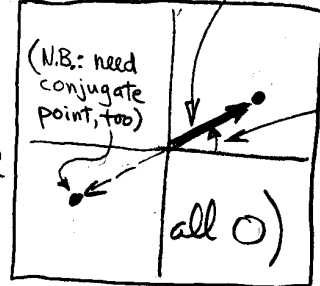
distance from center is stripe spacing

angle of point perpendicular to angle of stripes

amplitude



amplitude



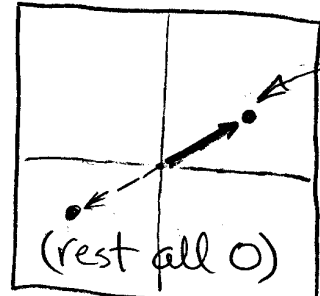
inverse Fourier transform (image recon.)

value from 0 to 360°

phase

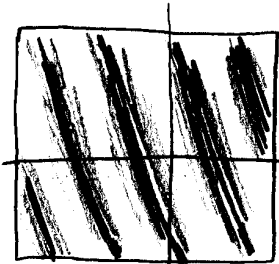
(Should be all zero not same as "stripe phase" above)

phase



- Cartesian dimensions of k -space - x - and y - spatial freq

N.B.: each dimension of spatial freq. space (k -space) from correlation w/ \sin & \cos - don't confuse k_x, k_y w/ \sin, \cos !



x -component of spatial freq (hi freq)

y -component of spatial freq (lo freq)

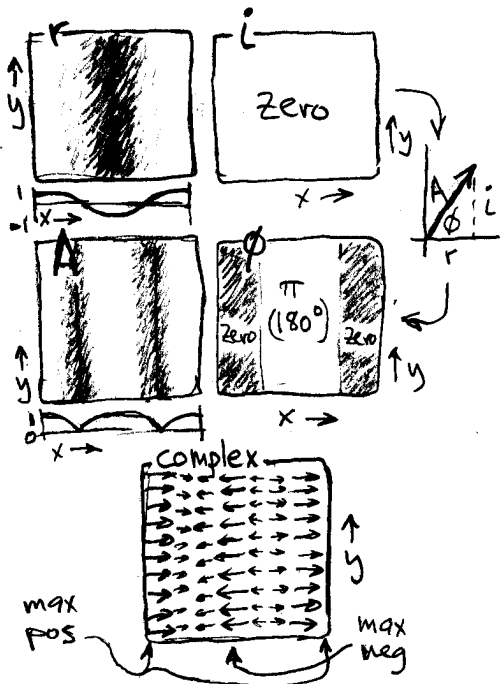
N.B. - increasing one 1D component increases the spatial freq of the 2D wave and rotates it

fourier-3b
FOURIER TRANSFORM OF IMAGE (4)

- 3 equivalent representations of complex numbers in image space and spatial-freq. space (k-space)
- example: cosinusoid in image space, then shifted in x-dir

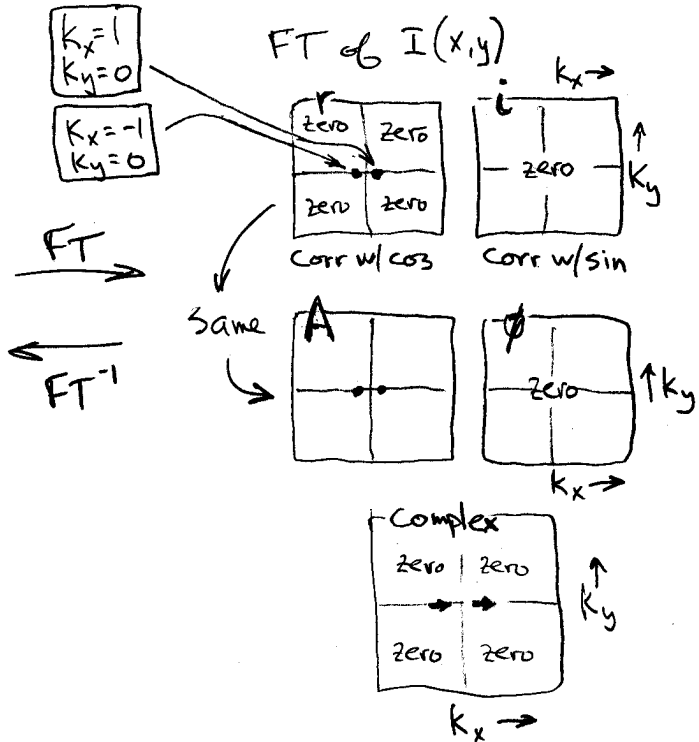
REAL IMAGE

$I(x,y) = \cos(x)$



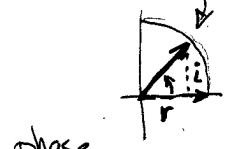
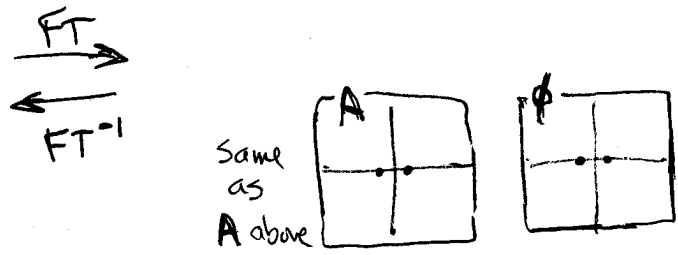
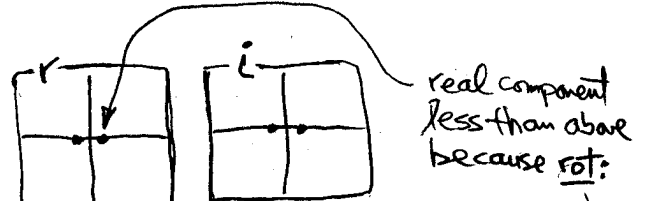
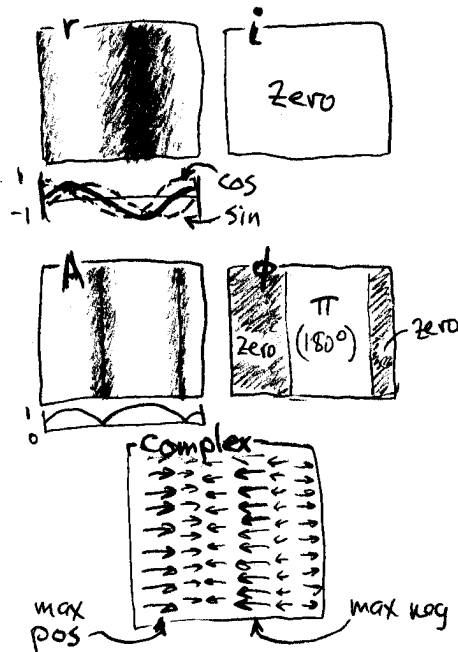
FT OF REAL IMAGE

Large values only here:



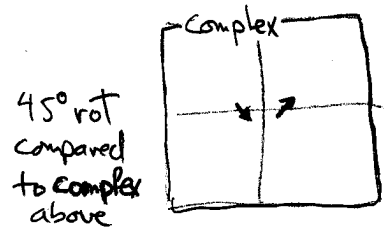
$I(x,y) = \cos(x - \pi/4)$

→ halfway between cos and sin (Shifted 45° to right)



phase now 45° at $k_x=1, k_y=0$ (-45° at $k_x=-1, k_y=0$)

N.B.: an example of the "Fourier Shift Theorem" (see below)



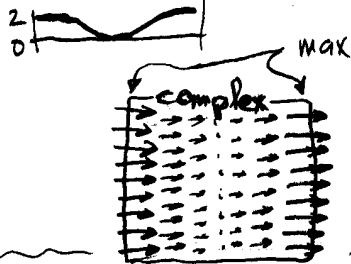
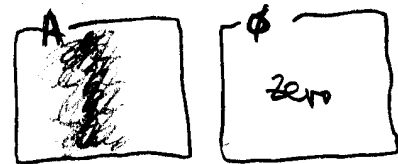
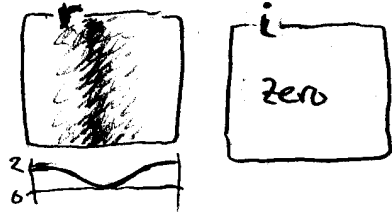
fourier-3c

FOURIER TRANSFORM OF IMAGE (S)

- (cont.) center of k-space (real image)
- complex image

REAL IMAGE

$$I(x,y) = \underline{1} + \cos(x)$$



center of k-space:

$$H(k) = \int_x h(x) \cdot e^{-i2\pi kx} dx$$

avg image brightness $\Leftarrow 1$ (real)

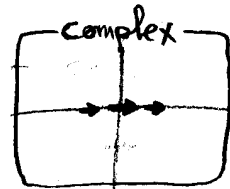
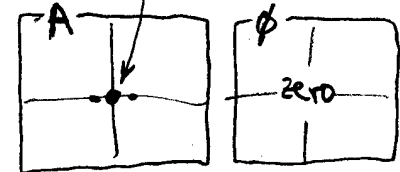
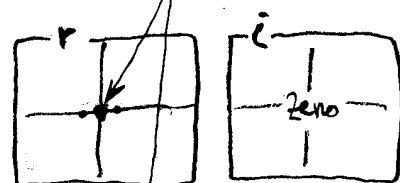
FT \rightarrow

\leftarrow FT⁻¹

[the center of k-space is zero w/ pure sin or cos image b/c avg. brightness = 0]

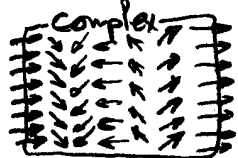
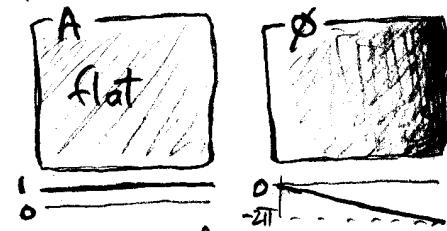
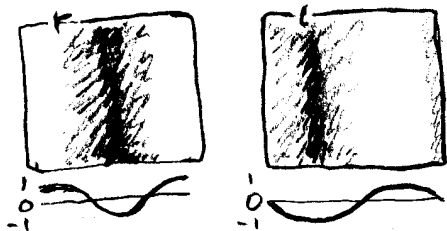
FT OF REAL IMAGE

positive center k-space



* COMPLEX IMAGE

$$I(x,y) = \cos(x) - i \sin(x) = e^{-ix}$$



FT, FT⁻¹

["missing" spike results in single spike correlating with cos and sin]

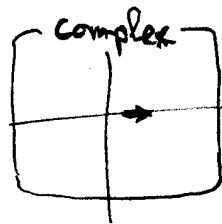
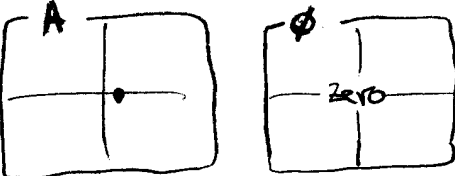
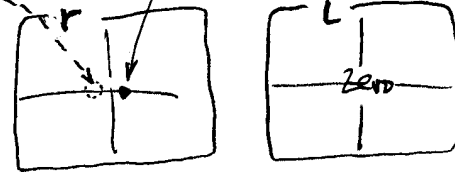
N.B.: this k-space is non-Hermitian:
k-space will only have Hermitian symmetry if image is real:

Hermitian symm. when complex conjugate (= complex num w/ sign flipped in imag. part) is equal to funct value w/ neg arg:

1D: $H(-k) = H^*(k)$
2D: $H(-k_x, k_y) = H^*(k_x, k_y)$

FT OF COMPLEX IMAGE

spike only on one side of k-space



[N.B. this is like what an artifact "spike" does tho it would have rand. phase]

[N.B. this is also exactly what a gradient does to image space!]

fourier-3d

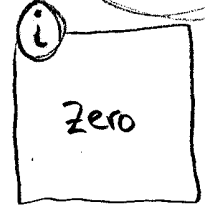
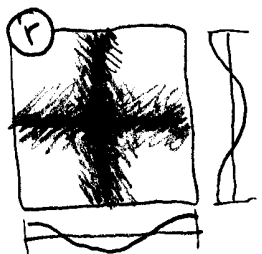
FOURIER TRANSFORM OF IMAGE (6)

- (cont.) x- and y-spatial freqs.
- special case: real image from sum of reals

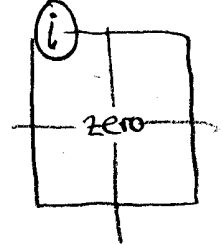
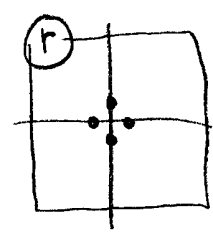
REAL IMAGE

$I(x,y) = \cos(x) + \cos(y)$

N.B. adds but doesn't rotate stripes



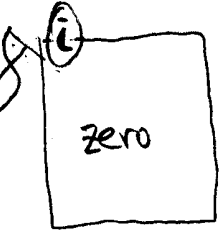
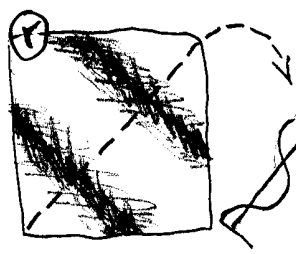
FT
FT⁻¹



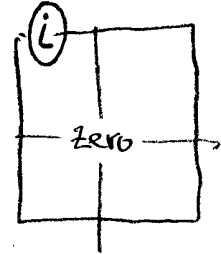
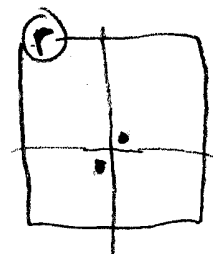
FT OF REAL IMAGE

$I(x,y) = \cos(x+y)$

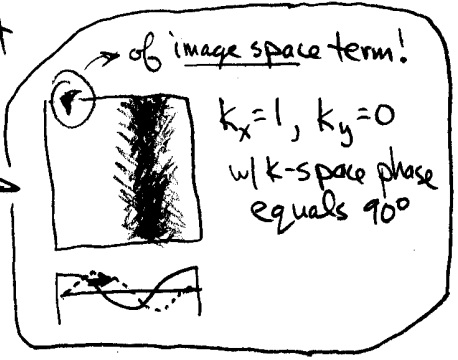
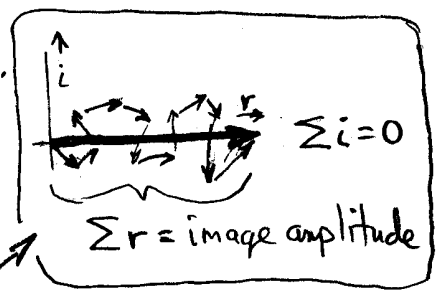
rotates stripes!



FT
FT⁻¹



- remember, single k-space point transforms to complex img.
- but if Hermitian symmetry, imaginary components cancel
- since all we want in image space reconstruction is real component, can just add real components of complex vectors at each image space point for every complex image corresponding to each k-space point
- N.B.: the k-space phase will affect offset of real valued image space cosinusoid
- therefore for real-valued image, we can visualize inverse FT as real-valued sum of offset real-valued cosinusoids
- N.B. cannot do this with MRI k-space data since phase errors (incl. multiple wraps) mess up real component \rightarrow must use amplitude img




$\frac{A \cdot e^{i\phi}}{r}$

GRADIENT COILS

- gradient coils for x, y, z generate approximately * a linear gradient in the strength of the z -component of the magnetic field B_z

all effects of gradients discussed before were in z -direction (parallel to B_0)



- for example, the x gradient coil induces a ramp in z -component of the magnetic field when moving in the x -direction:

$$B_{G,z} = G_x x$$

* - since a pure linear gradient of $B_{G,z}$ in only the $x, y, or z$ directions is not possible according to Maxwell equations, each gradient coil also induces a magnetic field that has components in the x - and y -direction ($B_{G,x}$ and $B_{G,y}$)

- the other magnetic field components are usu. ignored because they are so small relative to $B_{G,z}$, since $B_{G,z}$ is added to B_0 , and since B_0 is much stronger than $B_{G,z}, B_{G,y}, \& B_{G,x}$

2 to 3 orders of mag. less

- since standard reconstruction methods assume the existence of "non-Maxwellian" gradient fields, spatial distortion is introduced

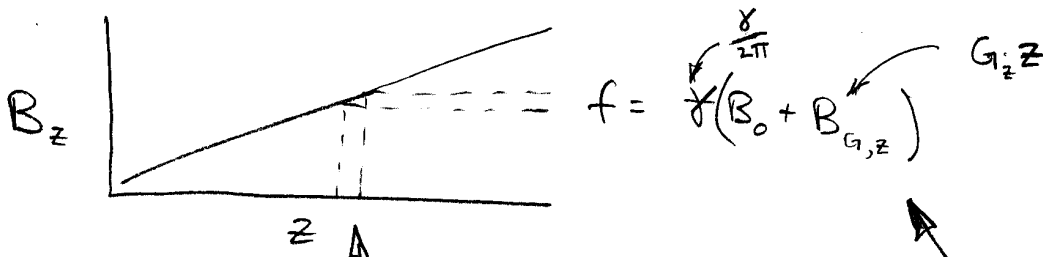
e.g. extra phase in z -dir \perp to x -grad

$$\Delta \phi_{G_x}(\vec{x}) \approx \frac{-\gamma z^2 G_x^2 t}{2B_0}$$

- the Maxwellian terms $B_{G,x}, B_{G,y}$ are known; can be included in the recon. process

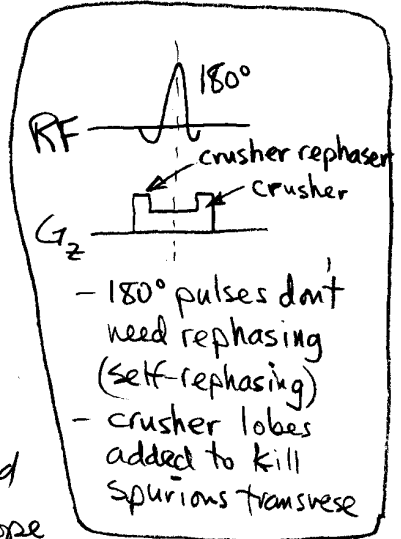
SLICE SELECTION (G_z)

- slice select gradient on during RF stim

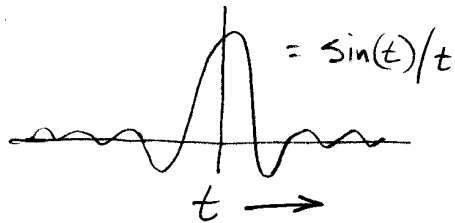


- protons here can only be excited by a narrow band of radio frequencies

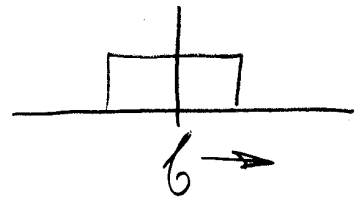
- to apply a pulse containing a narrow band of frequencies, we use a sinc pulse envelope (Fourier transform of a narrow freq. band)



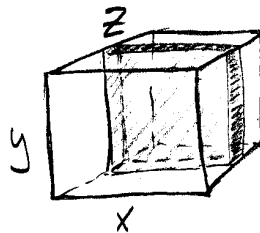
in practice, Gaussian pulse envelope good, too



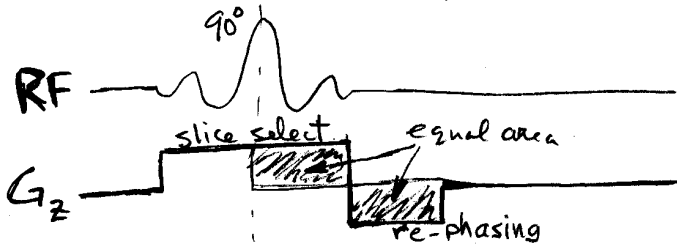
Fourier Transform \longleftrightarrow



- this excites protons in a narrow slab



- since the slice-selection gradient introduces (space-dependent) phase shifts (see freq encode) these have to be removed by a post-excitation rephasing z -gradient



- approximation from assuming tip occurs instantaneously in middle
- valid for small tip: $90^\circ \rightarrow 52\%$
- in practice: adjust to max, use crusher to kill spurious transverse on 180°

slice-3 PULSES FOR SLICE SELECTION

Fourier approach details

- Fourier transform approach to slice-selective pulse (linear approx. even tho tipping is non-linear)

$$\vec{B}_1(t) \propto \int_{f=-\infty}^{f=\infty} p(f) \cdot e^{-i 2\pi f t} df$$

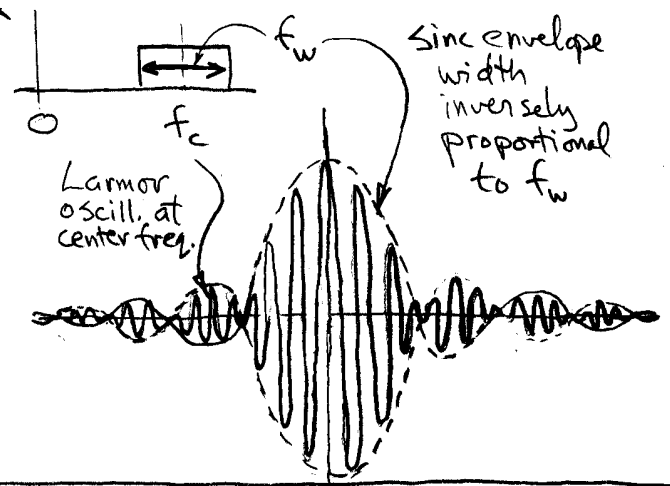
time dependent RF stimulation (complex) frequency selection function

i.e., time-dependent complex (= quadrature) pulse waveform in Fourier transform of frequency spectrum of RF pulse

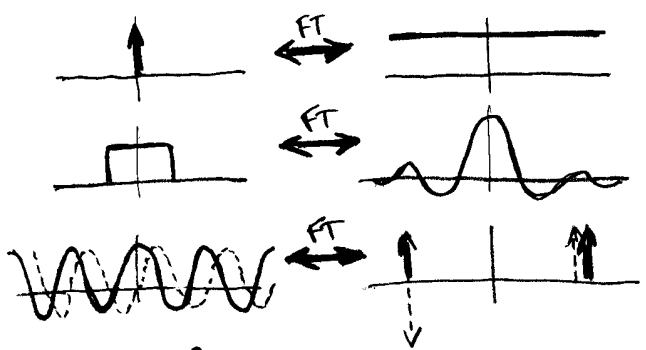
Solve with: $p(f) =$ frequency band:

$$\vec{B}_1(t) = A \cdot f_w \cdot \text{sinc}(\pi f_w t) \cdot e^{-i 2\pi f_c t}$$

amplitude controlling flip angle freq. width (controls slice width) sinc envelope determined by freq. width, f_w (N.B. wider f_w is narrower sinc) modulation (complex) at center freq., f_c



Fourier Transform Pairs, Rules



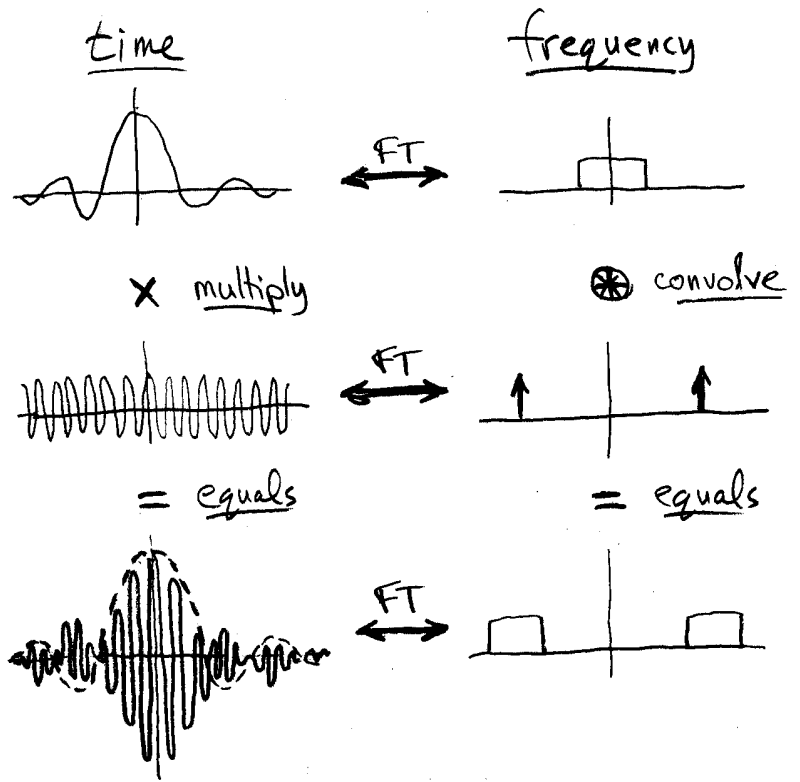
- multiplication in one domain equals convolution in other:

$$F[g(t) \cdot h(t)] = G(f) \otimes H(f)$$

means do FT

- convolution with delta funct impulse moves other function to impulse center

Fourier Transform Solution to: $\frac{1}{b} \rightarrow$



slice-4
SLICE SELECT RF PULSES

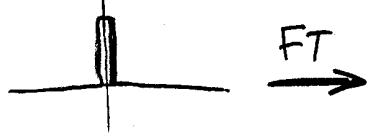
Interleaved Acquisition → better S/N b/c imperfect slice profile
 → spin history prob if motion

Common RF pulses

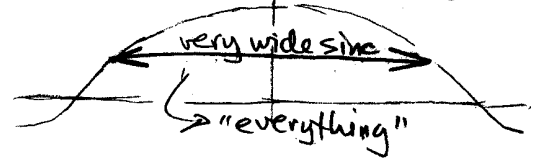
pulse envelope

freq spectrum (≈ slice profile)

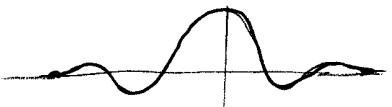
non-selective pulse ("hard" pulse)



FT →



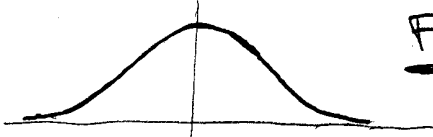
standard slice select sinc



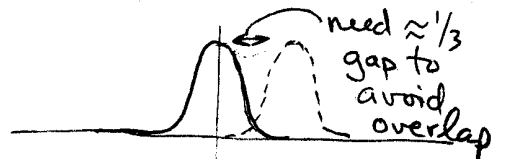
FT →



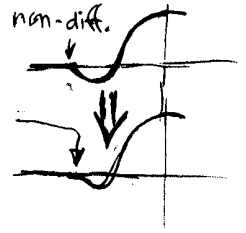
Gaussian



FT →



→ pulses need to be "apodized" (have "foot" removed)
 ↳ multiply by function so begin/end of pulse is differentiable



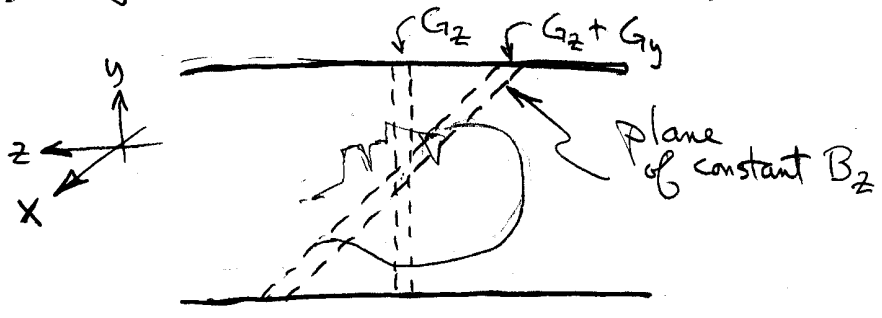
Fat Saturation

- fat protons have chemical shift causing resonant freq offset
- add phase offset not due to gradients, RF
- fix by off-water-resonance 90° (saturation) pre-pulse centered on fat freq
 ↳ need high quality (narrow freq) pulse to avoid saturate water!

- HOWTO
- 1) fat sat pulse
 - 2) wait T2 so fat signal decays, but no T1 regrowth of fat
 - 3) RF stim for water "protons - of interest"



Adding Another Gradient Tilts Slice



- with 3 gradients on, can excite arbitrary angle plane
- translate plane by changing either gradient amplitude or RF freq band: $f \rightarrow f + \frac{1}{R}$

freq. encode-0

WHY "FREQUENCY-ENCODING" IS A MISNOMER

- comes from original analogy in Lauterbur (1973):

Spectroscopy

Imaging

- 1) chemical shift change freq → gradient changes freq.
- 2) stimulate w/ broadband RF → same
- 3) time-sample FID containing multiple freqs → same
- 4) FT of FID to get spectrum → FT of FID to get Δx offsets

- this is technically correct (FT of FID) but highly misleading
 ↳ e.g., phase-encoding (turning a different gradient ON and OFF before recording FID) seems to be something completely different since OFF gradient can't affect freqs in FID

- the "k-space" perspective is a "Copernican Turn"
 ↳ idea is that data is not a set of samples of a time domain signal generated by multiple chemical-shift like frequencies

N.B.: sometimes useful to go back to orig spectroscopic analogy for debugging noise sources since freq encode lines still FT (or FT⁻¹) to spectra

→ rather, it is a set of samples of a frequency-domain signal, each sample generated by multiple spatial locations, (which are analogous to multiple time points)

- i.e., the 'direction' of the FT (Fourier transform) is reversed:

| | Signal | | result |
|--------------|---|--------------------|---|
| spectroscopy | samples of oscillations in <u>time-domain</u> | FT → | <u>frequency-domain</u> spectrum of shifts |
| MRI | samples of spat. freq. in <u>freq. domain</u> | FT ⁻¹ → | spatial object (like a <u>time-domain</u> signal) |

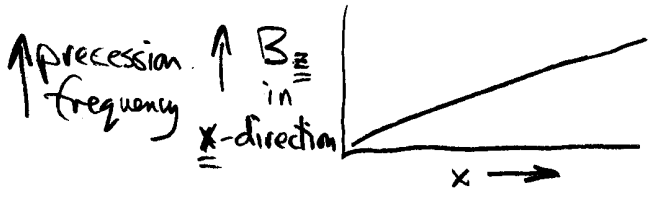
N.B. not full set all freqs like gradient makes!

- the original analogy only 'works' because $FT \approx FT^{-1}$ (except sign change)

freq encode-1
FREQUENCY ENCODING (1)

avoid this mistaken intuition!

- frequency encode gradient (G_x) causes precession rates to vary linearly in x-direction



↳ correct (remember that strength of G_x causes variation of slope of B_z in x-direction)

- different frequency signals are mixed together and recorded as a 1-D signal over time

↳ correct, but remember, we are recording summed local magnetization vectors after de-modulation

- a Fourier transform, which can convert back and forth between x-position (cf. time) and spatial frequency (cf. temporal freq) is done on signal

↳ correct

- spatial frequencies get confused/conflated with precession frequencies

↳ wrong!!

- therefore, the Fourier transform is used to convert position-dependent precession frequencies into spatial position

↳ conceptually wrong!!

↳ FT actually converts spatial frequencies to spatial position

- the spatial frequency increases for each time point in the readout
- the precession freq ramp is constant each timestep

** N.B.: gradient
 freq ramp does not need to be on during recording!!

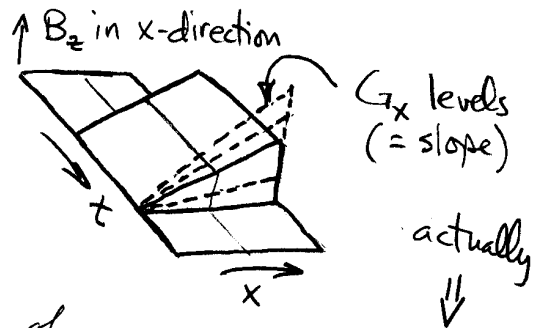
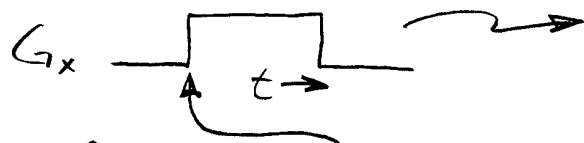
exactly same as

freq encode - 2

FREQUENCY ENCODING (2)

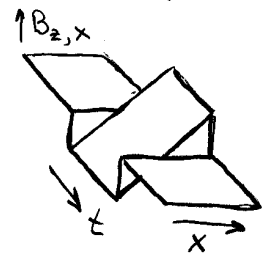
correct intuition - why phase critical

- "frequency"-encode gradient (G_x) turned on during during echo causes precession rates to immediately vary with x-position

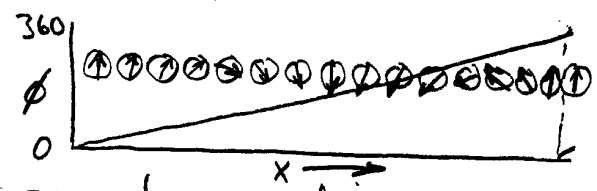
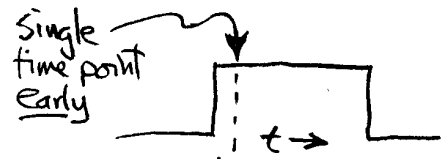


- at beginning of gradient on, the phase of signal coming from each x-position is the same

Summed phase angle is what we measure

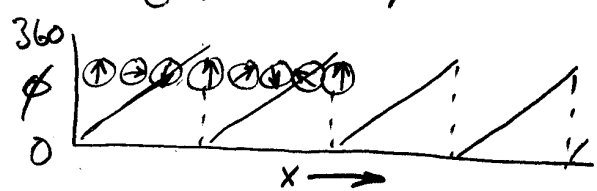
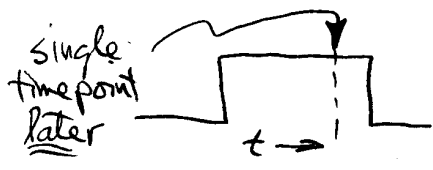


- early after gradient on, phase advances (because of faster precession frequency) arise with greatest phase advance at largest x-position



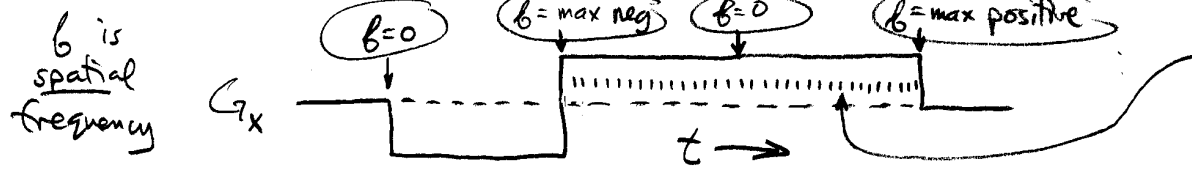
=> one cycle of spatial frequency of phase angle (= low spatial freq)

- later during gradient on, phase advances cause multiple wraparounds of phase angle across space



=> multiple cycles of spatial frequency of phase angle (= hi spatial freq)

- in practice, the lowest spatial frequency (= 0) occurs in the middle of the gradient on time because the phase is "wound" negatively by a preparatory gradient (to the highest negative spatial frequency) before data collection occurs



individual RF data samples (after demodulation)

freq encode-3

FREQUENCY ENCODING (3) why each datapoint is 1 spatial freq

Standard Fourier transform : (Temporal freq ↔ time)

$$H(f) = \int_{t=-\infty}^{t=\infty} h(t) \cdot e^{-i 2\pi f t} dt$$

Labels: $H(f)$ is freq domain; $h(t)$ is time domain; t is time; f is frequency; $e^{-i 2\pi f t}$ is sum across all time.

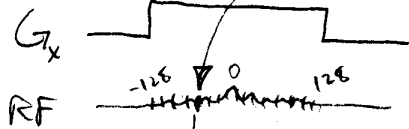
"k" is often used instead of "f" for the frequency variable

Imaging equation : (Spatial freq. ↔ space)

$$S(f) = \int_{x=-\infty}^{x=\infty} I(x) \cdot e^{-i 2\pi f x} dx$$

Labels: $S(f)$ is spatial frequency; $I(x)$ is signal strength at one x-position; x is space; f is spatial frequency; $e^{-i 2\pi f x}$ is sum across x of object.

one data point (i.e., one spatial freq) during readout (2 components)



get this single readout point by summing signal across x-position (RF coil records sum)
 even though variable is f , it represents one time point during readout

Signal strength at one x-position (brightness of image point)
 spin density (spectral dens.)

to make image, do inverse Fourier transform of recorded signal $S(f)$

Sum across x of object
 this is done by RF coil recording sum

Oscillations come from readout phase wrapping, where f is single spatial freq (e.g. 5) and x goes across object
 FID: $G_x t$
 SE: $G_x (t - TE)$
 $f = G_x t$, that is, spatial freq depends on amount of time gradient was on (this f increases with time!)

don't confuse with instantaneously changed precession freqs which are constant across entire readout time (for each x position)

freq encode - 4

ALTERNATE DERIVATION (incl. effects of G_x) SIGNAL EQ

- oscillators at $\omega = \gamma B$ at each position (just x for now)

$$S(t) = \int m(x) e^{-i\phi(x)} dx$$

- by definition, freq, ω is rate of change of phase, ϕ

$$\frac{d\phi(x,t)}{dt} = \omega(x,t) = \gamma B(x,t) \quad \text{and integrating} \quad \phi(x,t) = \int_0^t \omega(x,t) dt = \gamma \int_0^t B(x,t) dt$$

- assuming phase initially 0, B affected by gradients

$$B(x,t) = B_0 + G_x(t) \cdot x$$

$$\phi(x,t) \stackrel{\approx 0}{=} \gamma \int_0^t B_0 dt + \left[\gamma \int_0^t G_x(t) dt \right] x$$

$$= \omega_0 t + 2\pi k_x(t) x$$

k is time integral of gradient waveform

- demodulation removes the B_0 -caused carrier frequency $e^{-i\omega_0 t}$ from the first equation

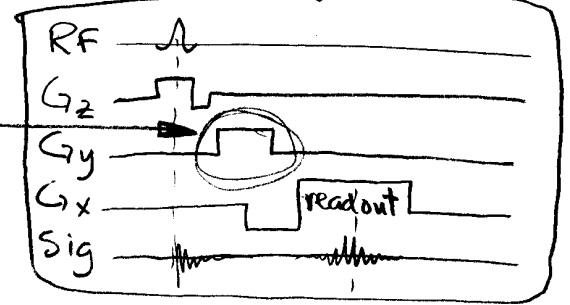
$$S(t) = \int_x \underbrace{m(x)}_{\text{amplitude of each oscillator}} e^{-i 2\pi k_x(t) x} dx$$

gradient-controlled phase

phase-1

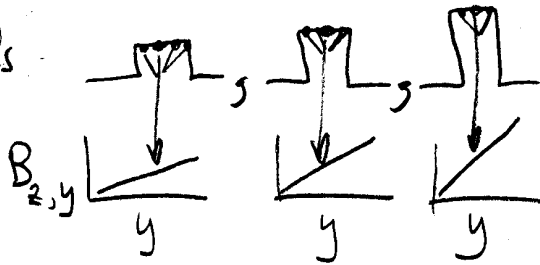
PHASE-ENCODE GRADIENT G_y

Pulse Sequence



- turn on gradient after excitation but before readout

- different levels of G_y



- higher levels of G_y (slope of B_z in y-direction!)

↳ higher spatial freq. (more phase wraps) in y-direction

- phase wraps persist after phase-encode gradient off

- read-out gradient (G_x) phase wraps then add to phase-encode phase

2D Imaging Equation

$$S(k_x, k_y) = \int \int I(x, y) \cdot e^{-i2\pi(k_x x + k_y y)} dx dy$$

$S(k_x, k_y)$: signal recorded at single time point (one readout point)
 ↓
 complex signal (from phase-sensitive detection)

$I(x, y)$: image (= strength of magnetization at each x-y pnt)
 ↓
 scalar (what we try to reconstruct)

$k_x = G_x t$: fixed strength, readout time
 $k_y = G_y$: increases each TR

Phase (vector of unit length and particular angle which is function of G_x and G_y)
 ↓
 phase angle (of scalar magnetization!) in rotating frame, set by gradients

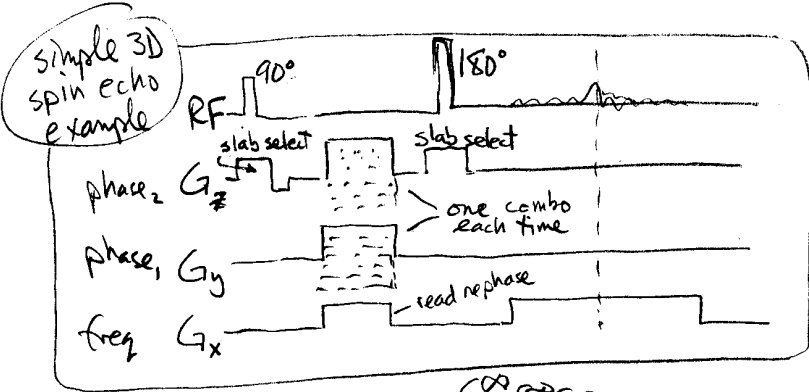
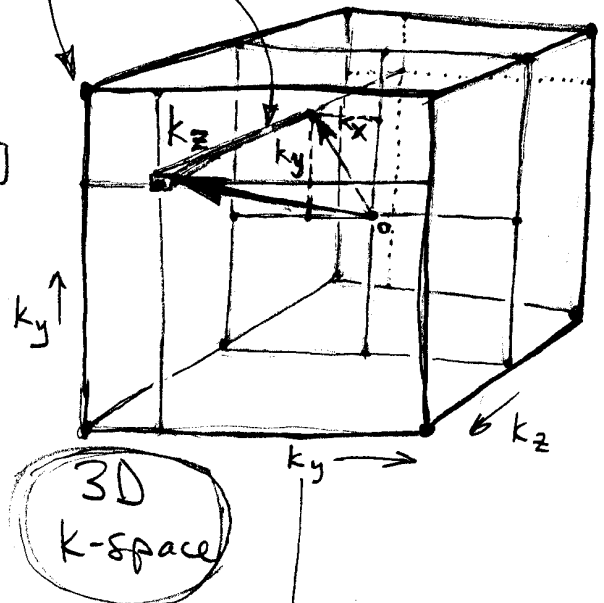
- ignoring relaxation, spatial frequency k_x and k_y have no "inertia" — they stay wherever the gradients last left them

phase - 2

3-D IMAGING - two phase-encode gradients

- use z-gradient for 2nd phase-encoding instead of slice selection
- excitation of whole slab (slice-select is whole brain)
- simple spin echo example (in real life, usu. done with echo trains [FSE] or small flip angle to allow short TR [SPGR])

total spatial freq. greater than in any 2-D k-space point (really a sphere is optimal)
 2nd phase encode add (onto orig freq. encode phase)



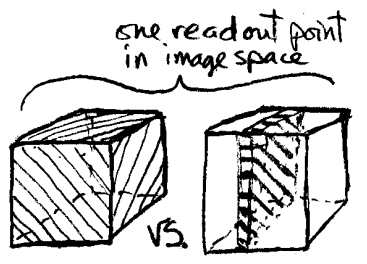
$$S(k_x, k_y, k_z) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} I(x, y, z) e^{-i2\pi (k_x x + k_y y + k_z z)} dx dy dz$$

signal recorded at single point of readout

- i.e., freq-encode phase, first phase-encode phase, and second phase-encode phase all just add (= 3D rotation of phase stripes)

N.B, this ignores relaxation effects for now

- S/N much better than 2-D because each entire excited volume contributes to signal from each pulse instead of just slice
 ↳ phase stripes created throughout volume vs. slice:



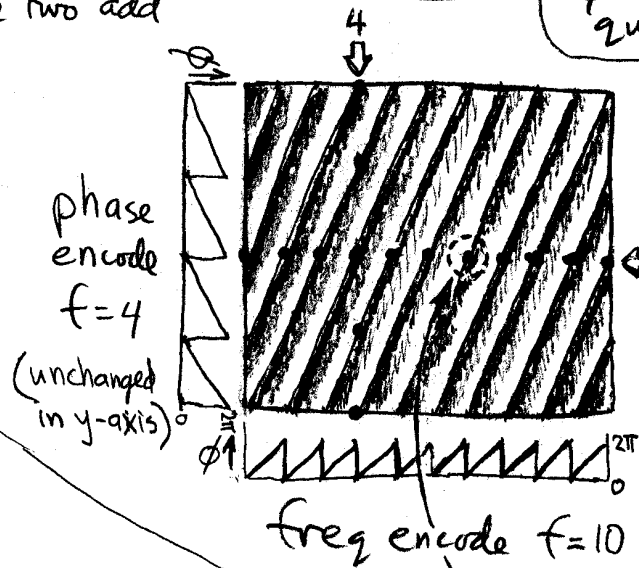
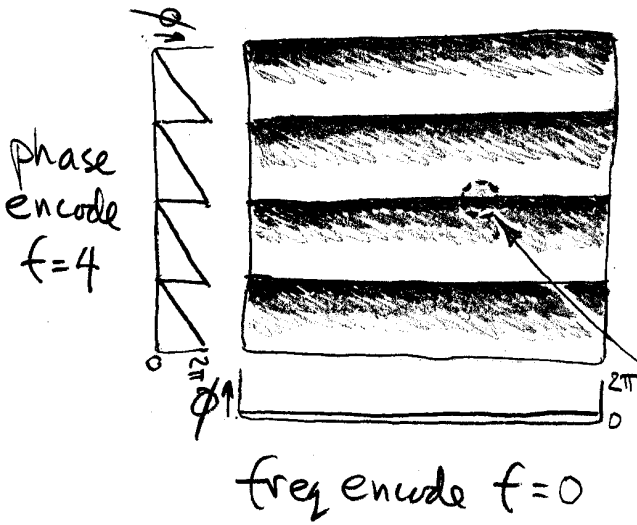
Phase - 3

PHASE & FREQ, 2D & 3D

Pictures of phase in image space

N.B.: stripes have sharp edges from phase wrap (not sinusoid since ϕ from 2-comp quadrature!)

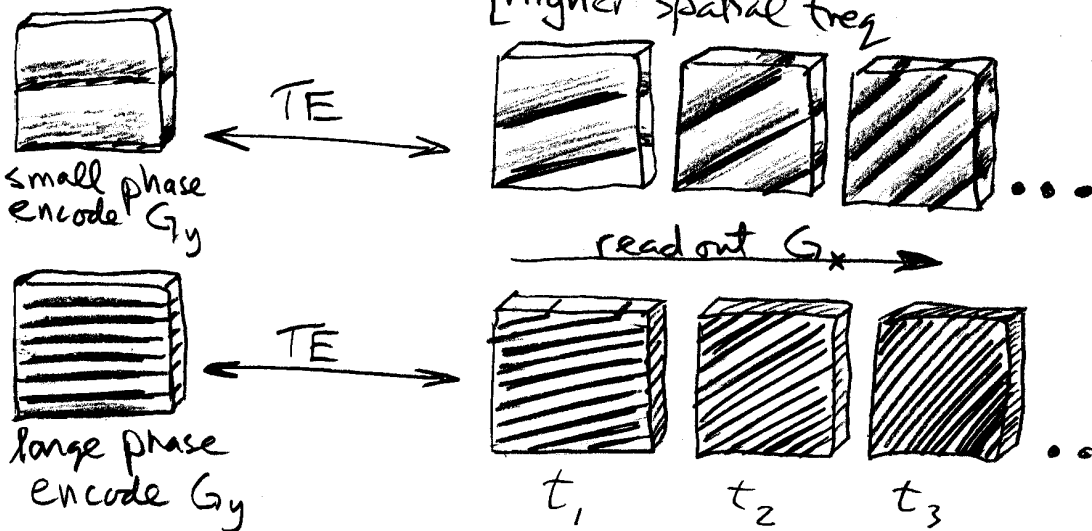
- since the phase-encode gradient and the freq encode gradient both affect phase the result is a rotation of phase "stripes" when the two add



stripes here represent complex value

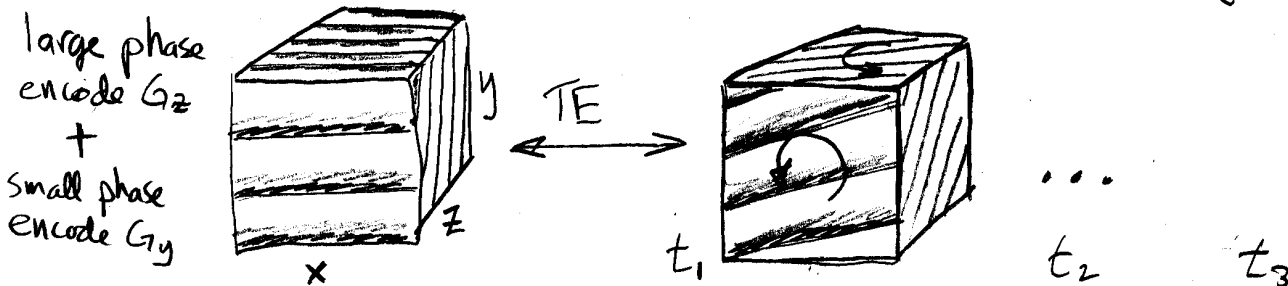
phase of whole image summed to one (complex) number by RF coils

- successive read out steps:



e.g., after y-gradient, spins at a point might be 2 cyc ahead while after x-gradient spins at same point 8 cyc ahead: but counting wraps in y-direction, still only 2 ahead

- 3D phase encode w/ G_y and G_z starts rotated in y-z plane



GRADIENTS MOVE K-SPACE LOCATION OF DATA POINT

- k-space (spatial-frequency space) location is set by integral of gradient over time up to recording point

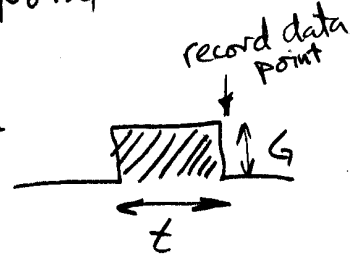
$$k = \gamma \int_0^{t=\text{recordtime}} G(t) dt$$

spatial freq recorded at $t = \text{recordtime}$
gradient strength as function of t

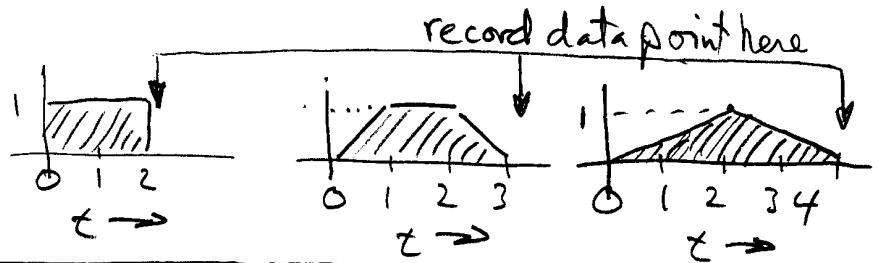
simple form of integral w/ boxcar gradient

$$k = Gt$$

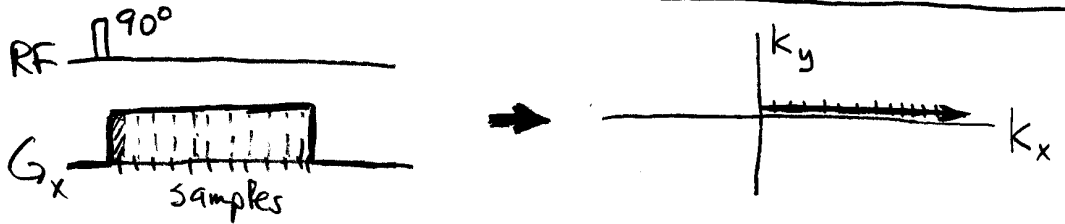
(k is area under curve)



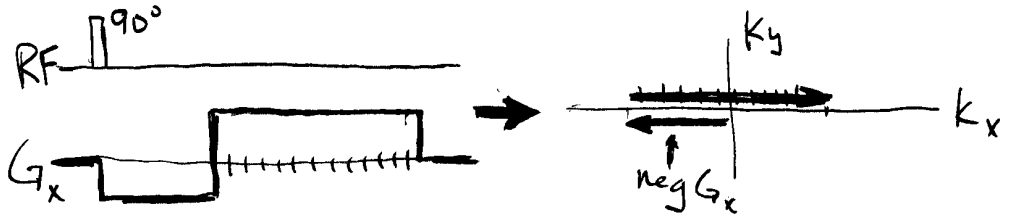
- all of the following gradients end up at the same point in k-space:



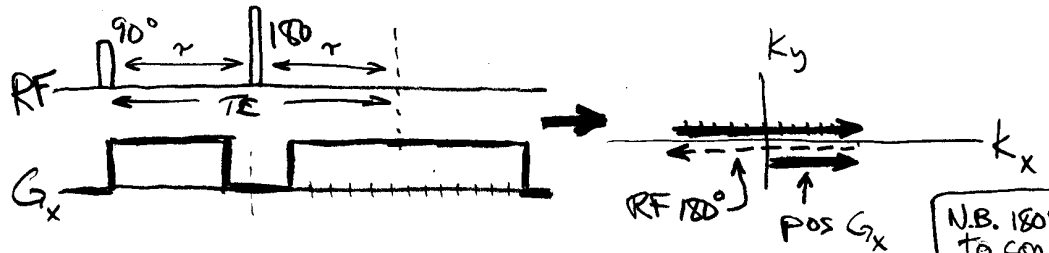
Frequency-encode FID



Frequency-encode gradient echo



Frequency-encode spin-echo (plus gradient echo!!)



N.B. 180° moves to conjugate pt.

Phase-encode then frequency encode gradient echo

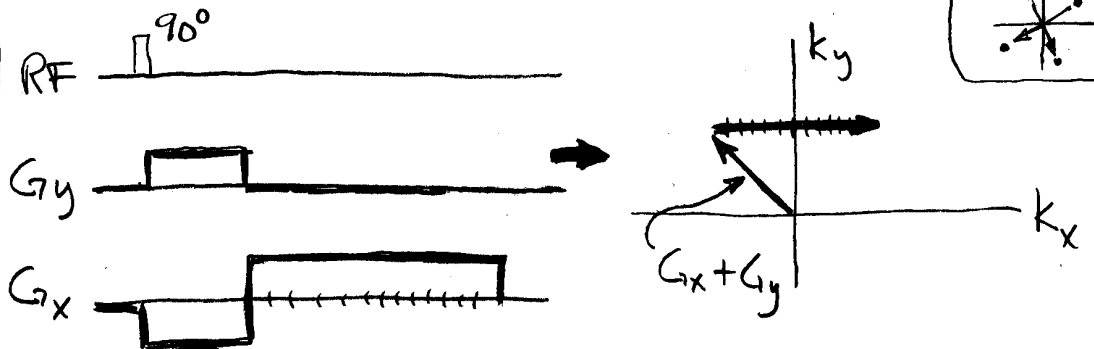


IMAGE RECONSTRUCTION

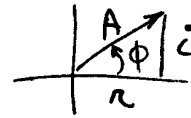
$$S(k_x, k_y) = \iint_{\text{RF coil sums}} I(x, y) e^{i 2\pi (k_x x + k_y y)} dx dy$$

$S(k_x, k_y)$: signal (complex)
 $I(x, y)$: brain spin density (real)
 gradient-caused phase wraps (complex) in transverse magnetization
 ↳ N.B.: assumes perfect sinusoids! (they're not)

$$I(x, y) = \iint_{k_y, k_x} S(k_x, k_y) e^{+i 2\pi (x k_x + y k_y)} dk_x dk_y$$

$I(x, y)$: screen image
 $S(k_x, k_y)$: signal (complex)
 sin, cos

ideally → image is real
 in practice → complex
 use amplitude image:



adding exponents same as multiplying two $e^{i 2\pi kx}$'s

$$= \iint_{k_y, k_x} S(k_x, k_y) e^{i 2\pi x k_x} e^{i 2\pi y k_y} dk_x dk_y$$

same as two sequential 1D FFT's (actual code)

$$= \int_{k_y} \left[\int_{k_x} S(k_x, k_y) e^{i 2\pi x k_x} dk_x \right] e^{i 2\pi y k_y} dk_y$$

- in practice, finite number of samples, N and M , are collected k_x and k_y directions of k -space (integral → discrete sum)

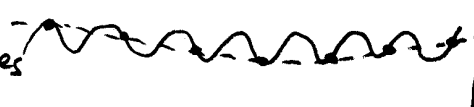
↳ $b/c M/2$ belongs to next replica

$$I(x, y) = \sum_{m=-M/2}^{M/2-1} \left[\sum_{n=-N/2}^{N/2-1} S(n, m) e^{i 2\pi \frac{\text{was } k_x}{\Delta k_x} n \Delta k_x x} \right] e^{i 2\pi m \Delta k_y y \Delta k_y}$$

$|x| < \frac{1}{\Delta k_x}$
 $|y| < \frac{1}{\Delta k_y}$
 sampling interval in k -space

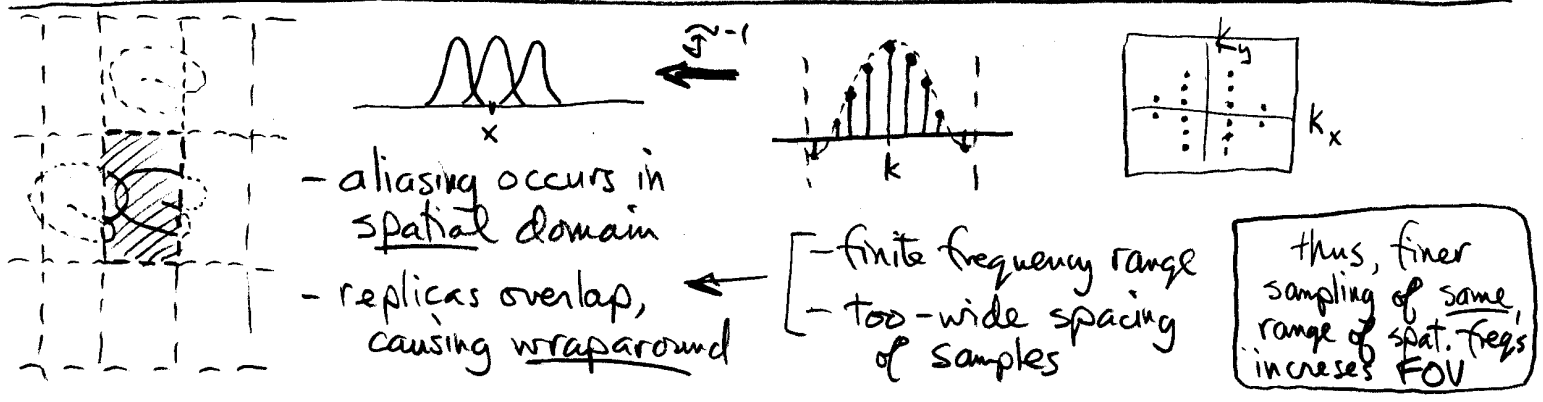
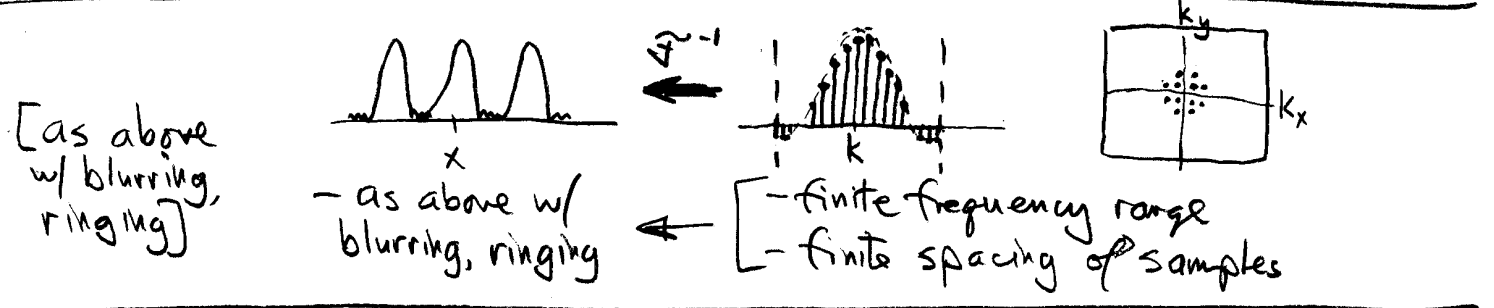
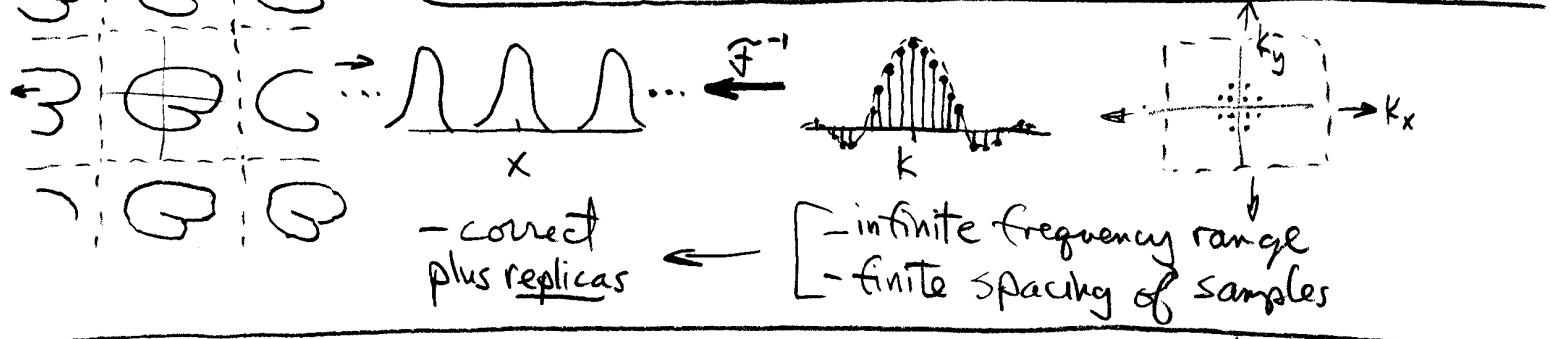
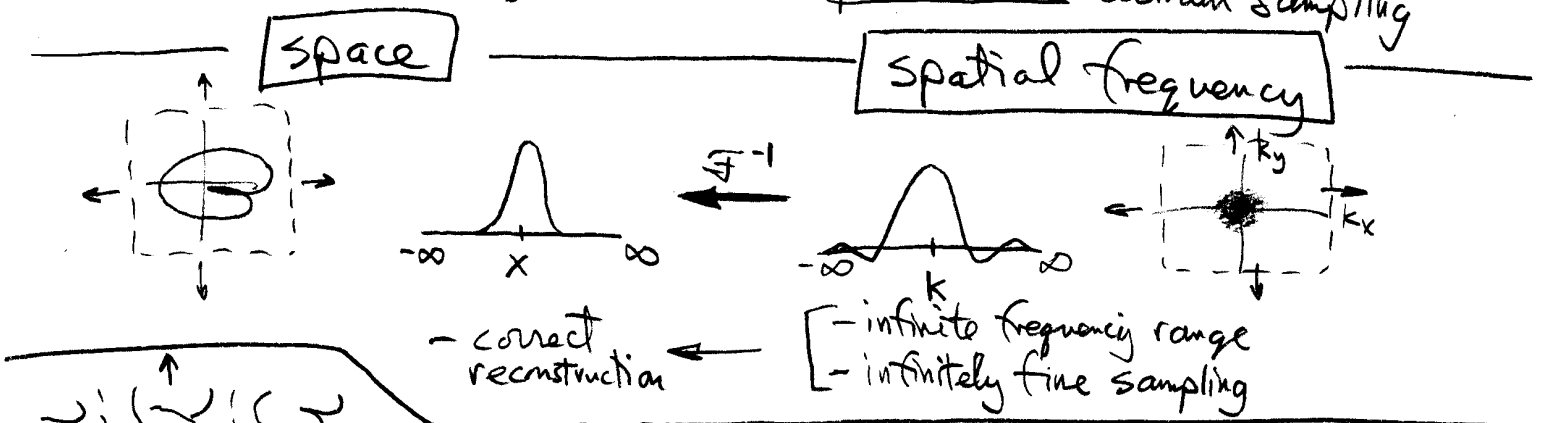
SAMPLING

aliasing, FOV

aliasing from insufficient samples in time domain 

- must consider effects sampling limited points in k-space
 - [limited in range of frequencies sampled ($k_{min} \rightarrow k_{max}$)
 - [limited in rate of sampling (Δk)

- N.B. aliasing less familiar when result of limited frequency domain sampling than limited space or time domain sampling



recon 2b

UNDER/OVER SAMPLE

more examples

$$FOV_x = \frac{1}{\Delta k_x}$$

FOV (distance to repeat) is reciprocal of spatial frequency sampling interval

$$\delta_x = \frac{FOV_x}{N} = \frac{1}{N \Delta k_x}$$

pixel size is FOV divided by k-space sample count

3 more examples (not incl. less samples to same spat. freq [bottom last page])

Basic Image

Same num samp. to 2x spat. freq.

2x num. samples to same spat. freq.

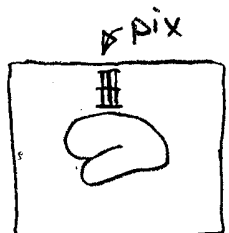
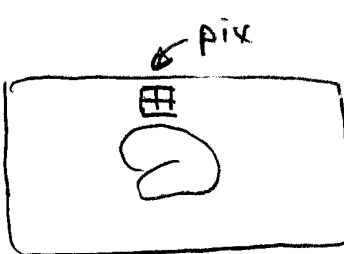
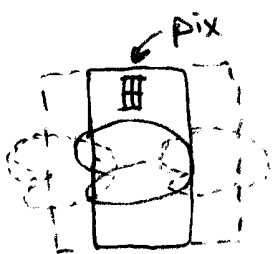
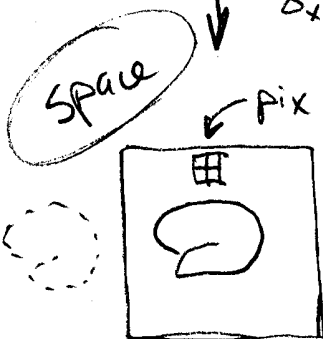
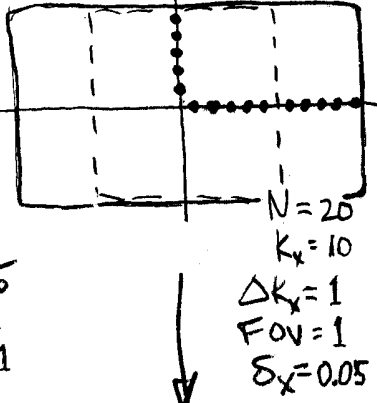
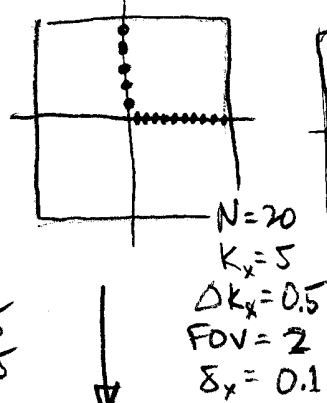
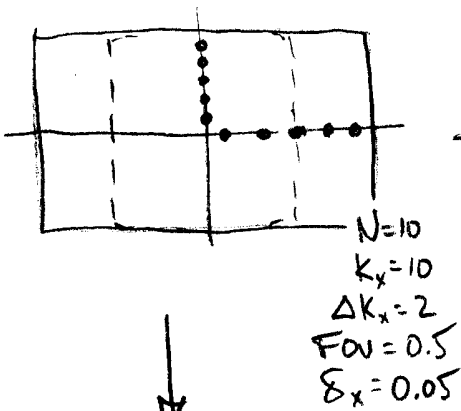
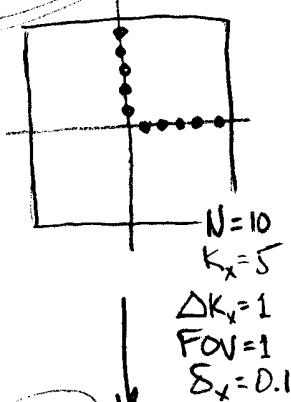
2x number samples to 2x spat. freq.

(i.e. gradients stronger or time ON longer)

(i.e. gradients weaker or time ON shorter)

(i.e. gradients stronger or time ON longer)

Spatial freq. k-space



- basic image
- square pix

- x-pix half width
- replicas intrude
- [Scanner makes square image "wrap" occurs]

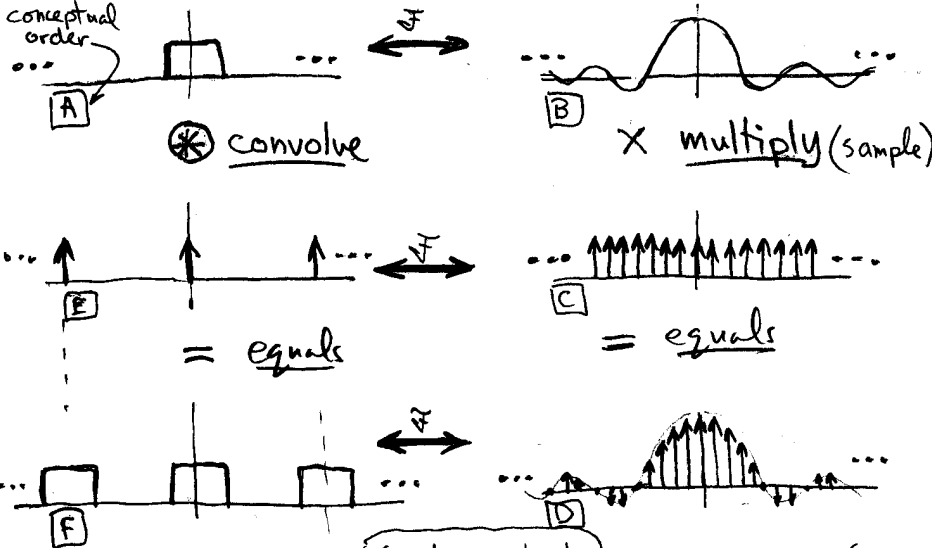
- square pix
- twice x-pix count so FOV = 2x
- this is "phase oversamp"
- [Scanner crops to square replicas move out]

- x-pix half width
- twice x-pix count
- same FOV
- this is decrease pixel size w/o change FOV

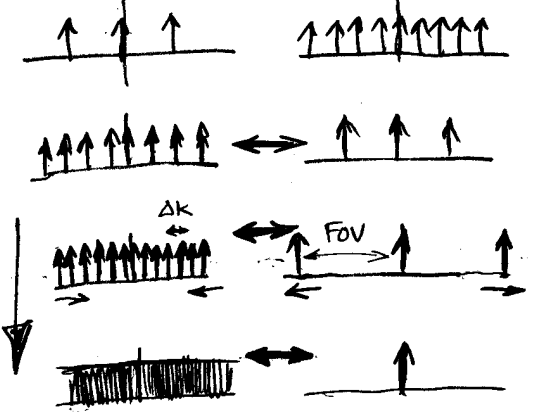
Fourier Transform Solution to Replicas

① image/brain space

② sampled data spatial frequency



- limit approach to Fourier transform of combs



$$FOV = 1/\Delta k$$

$$\Delta k = 1/FOV$$

Useful FT's

See also normalized Sinc w/ zero crossings at 1, 2, 3...

$$= \frac{\sin(\pi k)}{\pi k}$$

$$\text{sinc}(k) = \begin{cases} 1 & \text{at } k=0 \\ \frac{\sin(k)}{k} & \text{otherwise} \end{cases}$$

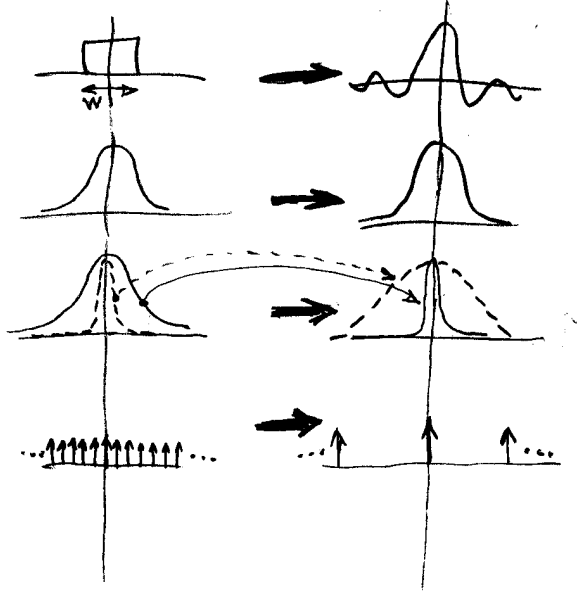
rect $\xrightarrow{\mathcal{F}}$ $\text{rect}\left(\frac{x}{w}\right) \xrightarrow{\mathcal{F}}$ $w \cdot \text{sinc}(\pi w k)$

Gaussian (special case) $e^{-\pi x^2} \xrightarrow{\mathcal{F}}$ $e^{-\pi k^2}$

larger \Rightarrow narrower

Gaussian (adj width) $e^{-ax^2} \xrightarrow{\mathcal{F}}$ $\sqrt{\frac{\pi}{a}} e^{-\frac{\pi^2 k^2}{a}}$

comb $\sum_{n=-\infty}^{\infty} \delta(x - \frac{n}{\Delta k}) \xrightarrow{\mathcal{F}}$ $\Delta k \sum_{p=-\infty}^{\infty} \delta(k - p \Delta k)$



recon-4
POINT-SPREAD FUNCTION

$$\hat{I}(x) = \Delta k \sum_{n: \{-N/2, N/2\}} S(n \Delta k) e^{i 2\pi n \Delta k x}$$

- set true image to δ -function, then measured signal is:

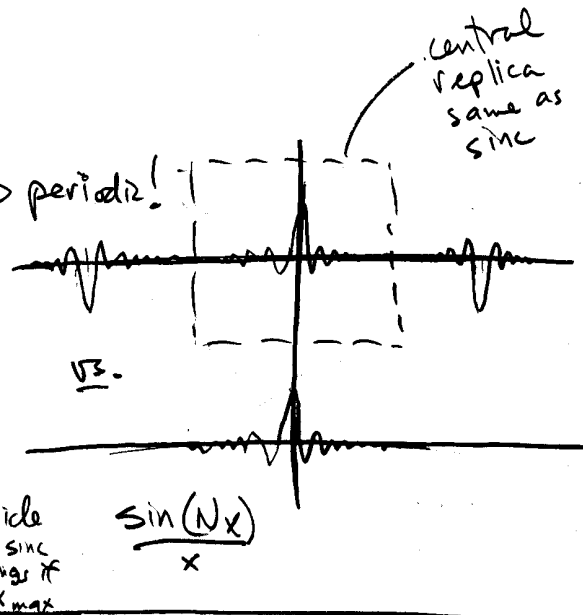
$$S(n \Delta k) = 1$$

- substitute into recon to get PSF:

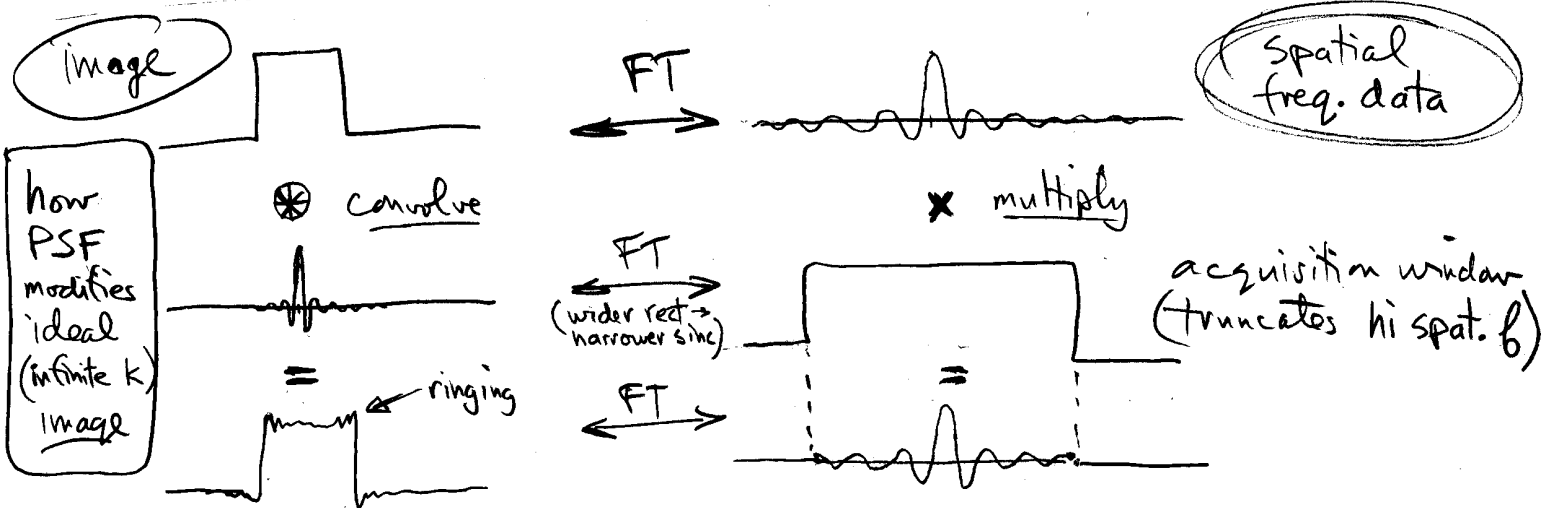
$$h(x) = \Delta k \sum_{n: \{-N/2, N/2\}} e^{i 2\pi n \Delta k x}$$

- simplify

$$h(x) = \Delta k \frac{\sin(\pi N \Delta k x)}{\sin(\pi \Delta k x)} \Rightarrow \text{periodic!}$$



- that is, image is reconstructed from a sum of sinc's, because the FT of a boxcar pixel in k-space is an image sinc



recon-5 GENERAL LINEAR INVERSE RECON FOR MRI

$$S(k_x) = \int_x I(x) e^{-i 2\pi k_x x} dx$$

perfect spin phase "stripes"
modeling real life imperfect ones

Signal eq. → fwd problem

$$I(x) = \int_{k_x} S(k_x) e^{+i 2\pi x k_x} dk_x$$

perfect "stripes"

Recon eq. → inv. problem

$$\vec{s} = \mathbf{F} \vec{i}$$

$$\begin{bmatrix} s \\ \vdots \\ s \end{bmatrix} = \begin{matrix} x,y \rightarrow \\ \downarrow k_x \\ \mathbf{F} \end{matrix} \begin{bmatrix} i \\ \vdots \\ i \end{bmatrix}$$

Linear "forward solution"
matrix & vectors have complex entries
can build in any measurable priors

$$F_{x,y,z} = \underbrace{g(x,y)}_{\text{coil gain at this location}} e^{-i\phi(x,y)} \underbrace{e^{-(nT \pm m\Delta t + TE)/T_2}}_{\text{T2 decay}} \underbrace{e^{-i\gamma \Delta B(x,y, nT \pm m\Delta t)}}_{\text{B}\phi \text{ error (x,y dep.)}} \underbrace{e^{-i2\pi(m\Delta k_x x + n\Delta k_y y)}}_{\text{freq + phase (complex)}}$$

one readout time 1st readout

could insert x-y-dependent gradient non-lin.

multi-coil

$$\begin{bmatrix} s \\ \vdots \\ s \\ \vdots \\ s \end{bmatrix} = \begin{matrix} x,y \rightarrow \\ \downarrow k_x \\ \mathbf{F} \\ \text{coil 1} \\ \vdots \\ \text{coil 2} \end{matrix} \begin{bmatrix} i \\ \vdots \\ i \end{bmatrix}$$

naturally incorporates undistorted field map
different sensitivity function for each coil
contains additional info about source loc.
but, need reference scan, low-res ok
(need phase corrections for each coil)

$$\vec{i} = \mathbf{F}^+ \vec{s} \quad \text{over-determined}$$

Moore Penrose inverse

$$\mathbf{F}^+ = (\mathbf{F}^T \mathbf{F})^{-1} \mathbf{F}^T \quad (xy)^2 \rightarrow \text{"small"}$$

$$= \mathbf{F}^T (\mathbf{F} \mathbf{F}^T)^{-1} \quad (x \cdot y \cdot \text{coils})^2 \rightarrow \text{16x bigger for 4 coils}$$

$([\mathbf{F}^T] [\mathbf{F}])^{-1} [\mathbf{F}^T]$

$[\mathbf{F}^T] ([\mathbf{F}] [\mathbf{F}^T])^{-1}$

$$\vec{i} = [(\mathbf{F}^T \mathbf{F})^{-1} \mathbf{F}^T] \vec{s}$$

slice-by-slice
assume slice select swamps $\Delta B\phi$

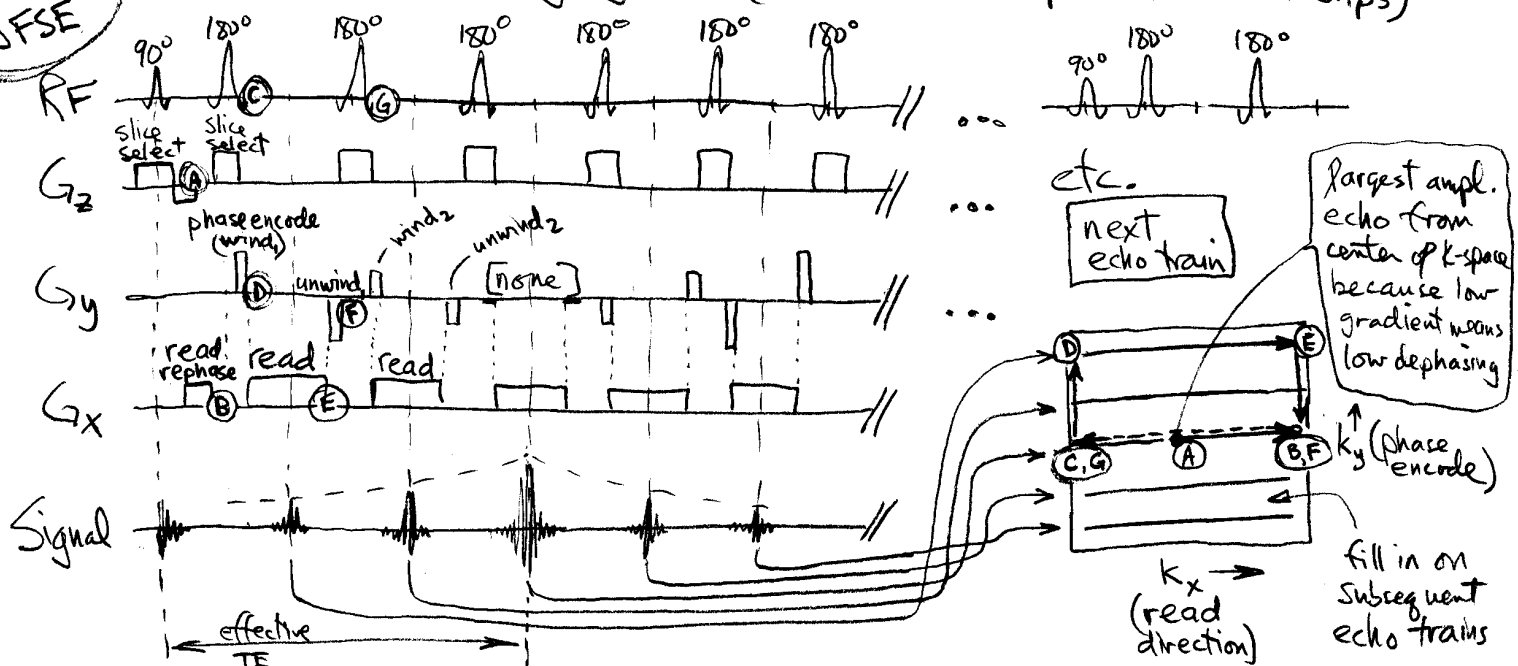
FAST SPIN ECHO (FSE)

RARE, FSE, 3DFSE

→ "echo train"

- one 90° pulse followed by multiple 180° pulses (e.g., 8) each with a different phase-encode gradient
- each phase "winder" is "unwound" because leftover phase would be re-focused away by 180° (vs. EPI where it persists between blips)

2DFSE



largest ampl. echo from center of k-space because low gradient means low dephasing

next echo train

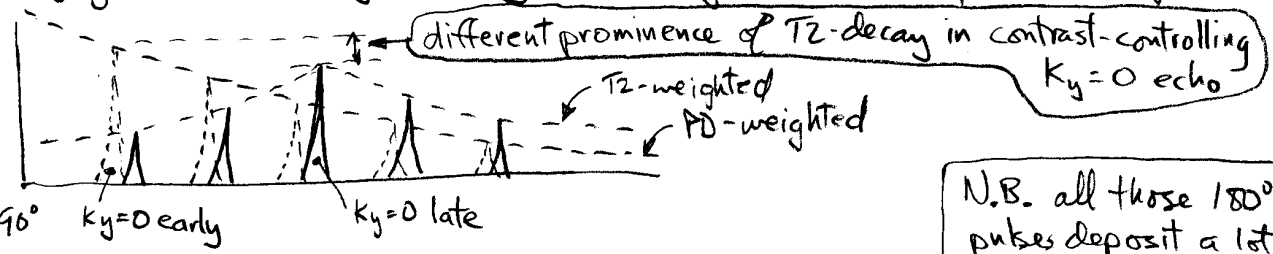
fill in on subsequent echo trains

- the "effective TE" is the TE when center of k-space is collected (largest effect on contrast, largest echo)

N.B.: only one read rephase subsequent 180's reset from right to left

- each subsequent echo has more T₂ decay: $E_n = e^{-nTE/T_2}$ $n = 1, 2, \dots, M$

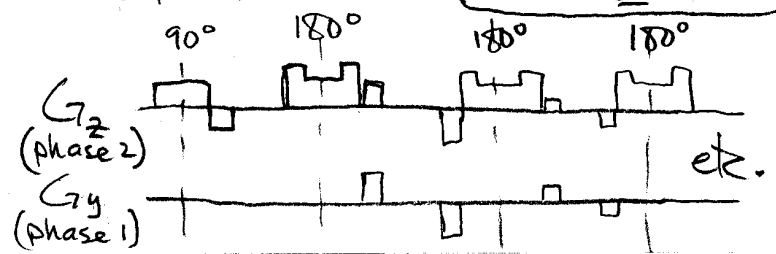
- by arranging to collect k_y=0 early, PD-weighted instead of T₂-weighted



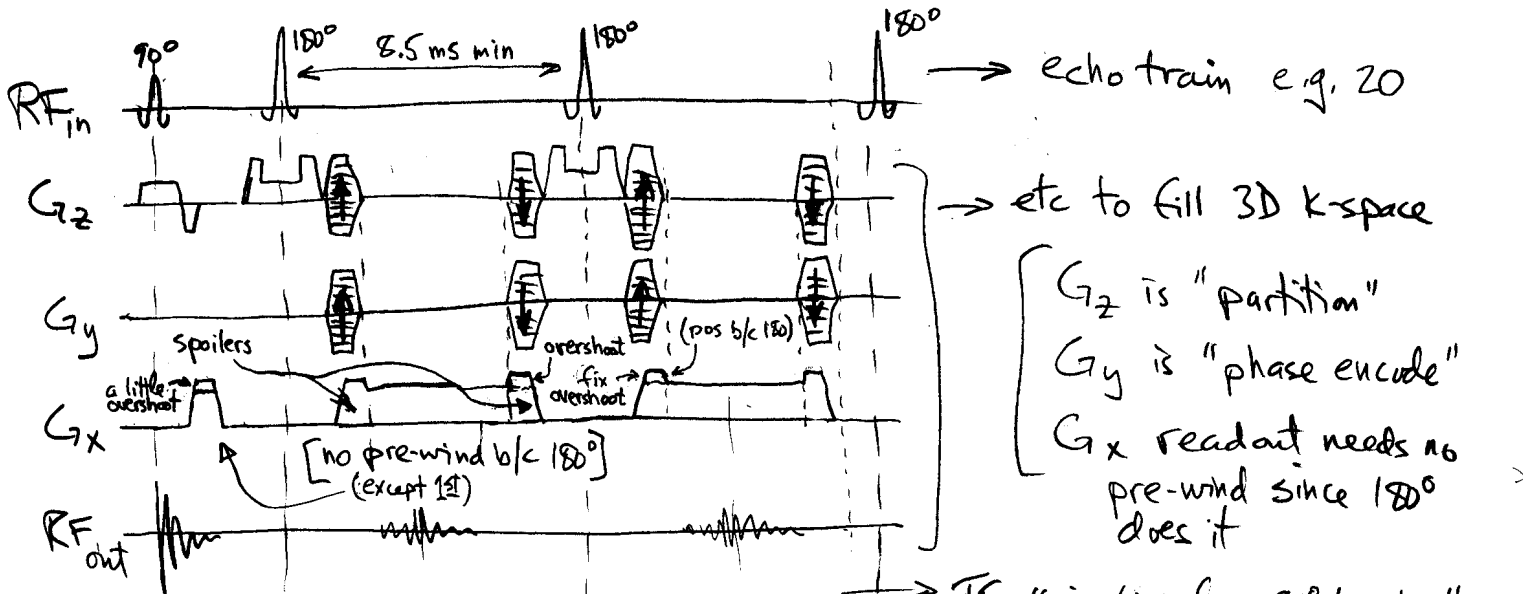
N.B. all those 180° pulses deposit a lot of RF power: 90°+180° = 45x Power 30°

- possible to correct different T₂-weighting of echoes by estimating T₂ curve from G_y=0 echo train

- 3DFSE - like 2D except wind/unwind added to thick slice select (w/crushers on 180°)



pulse-1b
MULTI-SLAB 3DFSE, PROBLEMS



- echoes die out quickly by e^{-t/T_2}
- since echoes after 90° limited to < 30, can't fill 3-D k-space in a reasonable time

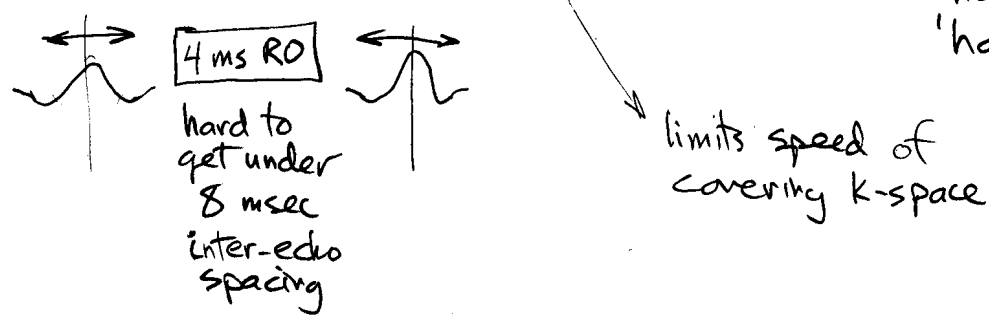
- SAR constraint $SAR \propto B_0^2 \theta^2 \Delta t$ rough approx. for non-adiabatic standard pulses
 ↳ 180° pulses deposit 4-6x power of 90°

- "multi-slab" is halfway between slices and single-slab



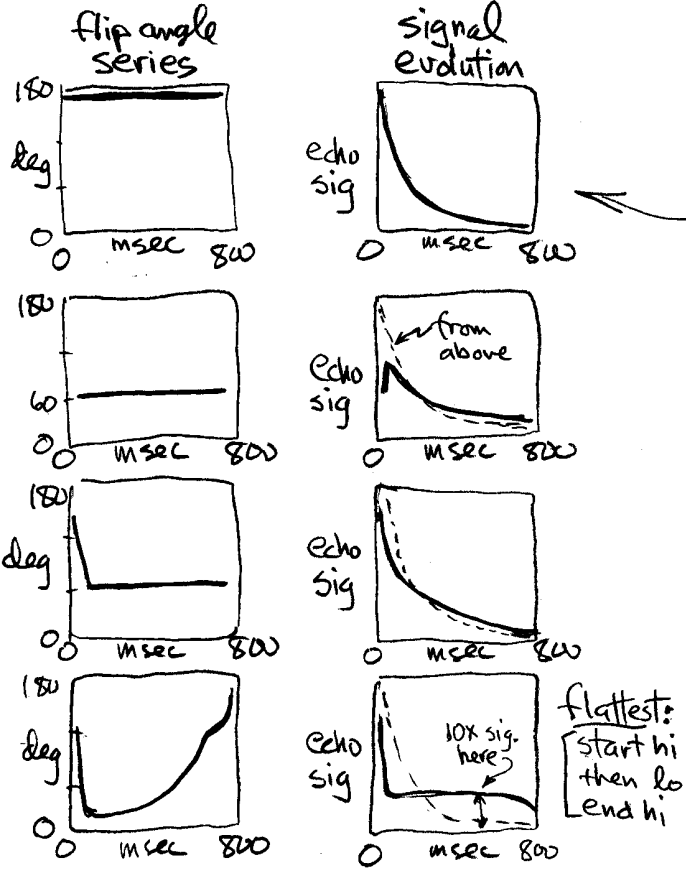
- problem at slice boundaries — esp. movement

- multislabs requires slice selective RF pulses → longer than non-selective 'hard' pulses



pulse-1c
SINGLE-SLAB 3D FSE (SPACE)

from Mugler (2014) J Mag Res Img



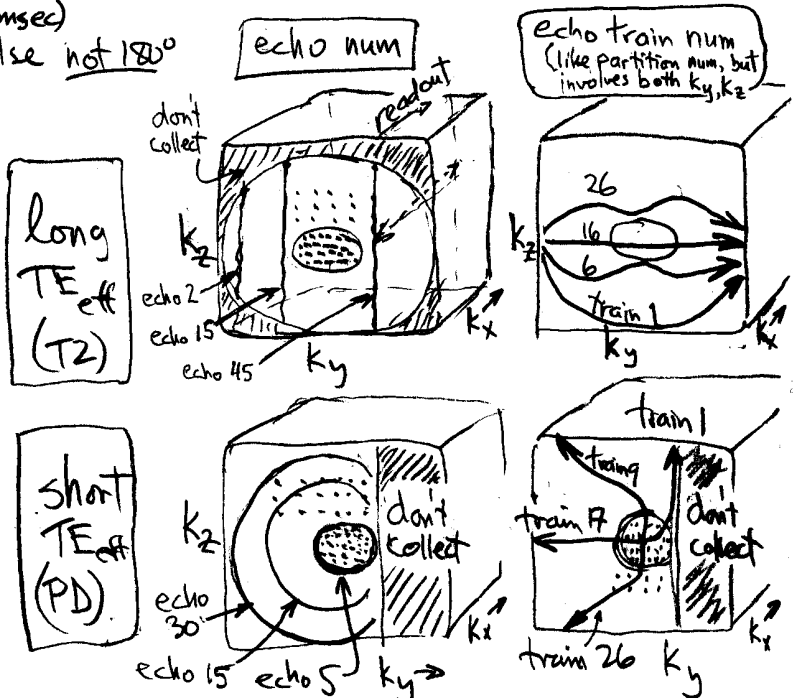
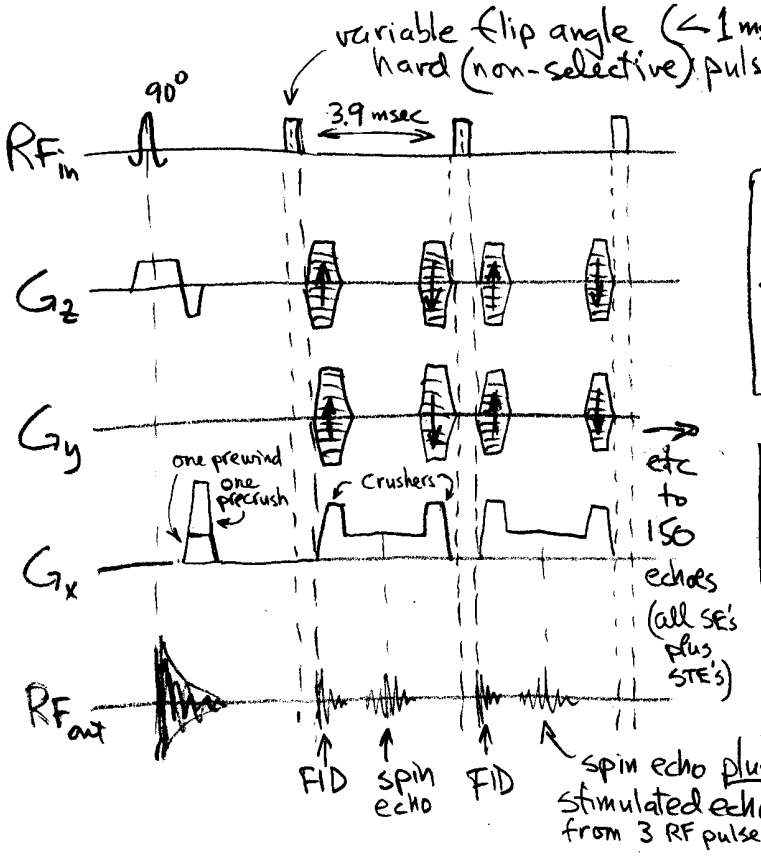
- regular FSE (180° pulse train)
- Sub 180° pulses cause each successive pulse to also generate a stimulated echo (STE)
- ↳ this "storage" in z-axis preserves magnetization for longer time
- smaller flip angles allow much longer echo trains
- ↳ enough to collect whole plane of 3-D k-space +
- different than hyper echoes (not symmetric)
- contrast must consider STE

- single-slab 3D FSE pulse seq.

N.B.: T1 !!

$$SE = \sin \alpha_1 \sin^2 \frac{\alpha_2}{2} e^{-2\tau_1/T_2}$$

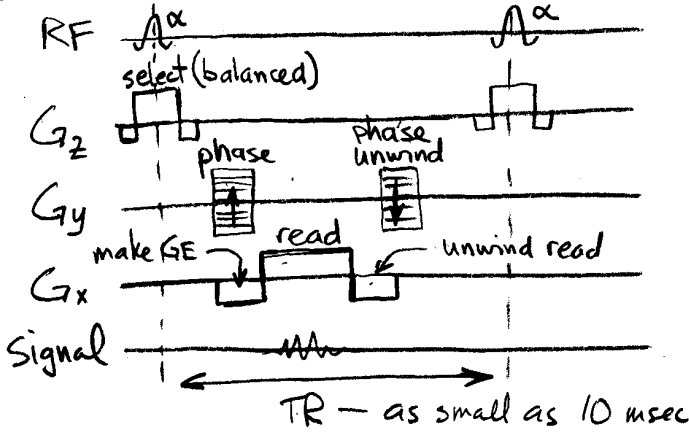
$$STE = \frac{1}{2} \sin \alpha_1 \sin \alpha_2 \sin \alpha_3 e^{-\tau_1/T_1} e^{-2\tau_2/T_2}$$



NB: time to cent k-space is $\approx 5x$ apparent contrast time b/c of "storage" (e.g. $TE_{eff} = 585$ ms looks like FSE $TE = 140$ ms)

Pulse-2 FAST GRADIENT ECHO (GRASS | FLASH | FISP | SPGR | MPRAGE)

- small tip so TR can be greatly reduced (e.g. 10 msec, less than T₂)
- 'leftover' undecayed transverse magnetization ["unwind" and re-used "spoiled" before next shot]



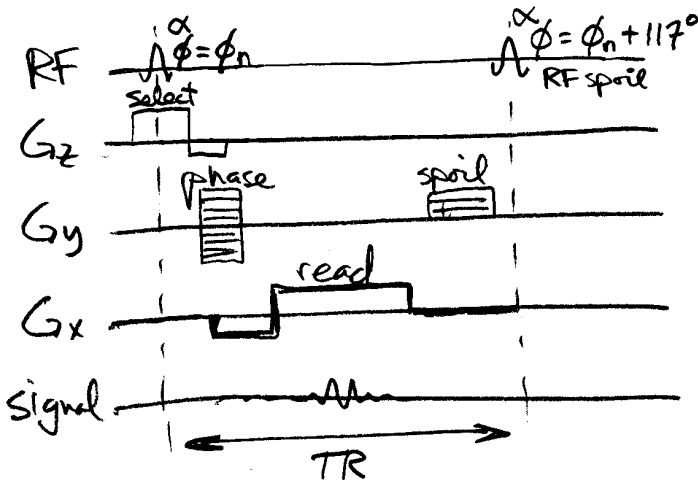
STEADY-STATE COHERENT (GRASS, FISP)

- unwind phase from phase-encode M_T before next pulse (there because TR < T_E)
- unwind read gradient, too

$$S = k \sin \alpha \left[\frac{1}{1 + \cos \alpha + (1 - \cos \alpha) T_1/T_2} \right] e^{-TE/T_2}$$

↳ T₂/T₁-weighted contrast (bright CSF)

| tissue | T ₂ /T ₁ |
|--------|--------------------------------|
| brain | 0.11 |
| fat | 0.3 |
| CSF | 0.7 |

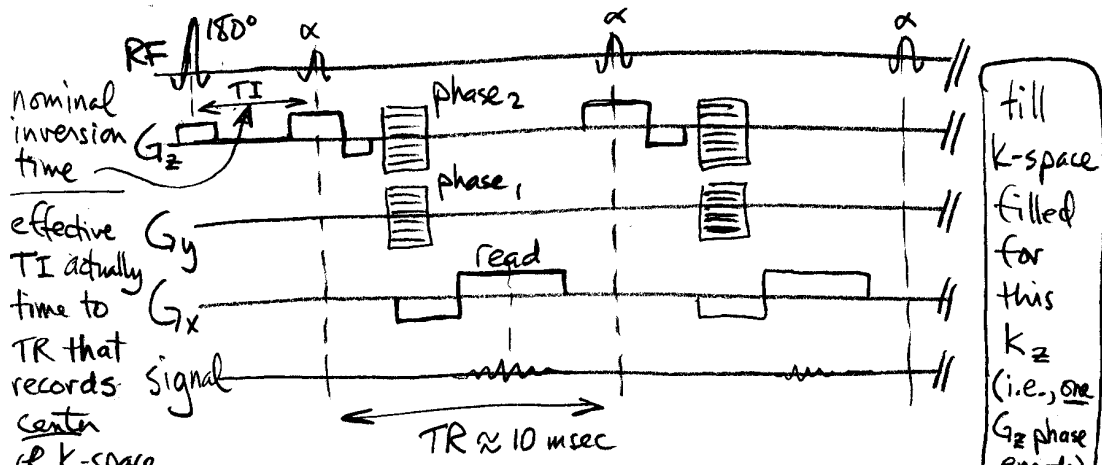


STEADY-STATE SPOILED (SPGR, FLASH)

- spoil with random gradient (but this still allows some alpha refocusing)
- spoil with gradient plus incremented phase of RF pulses (RF spoiling)
- good gray-white contrast (T₁-weighted)

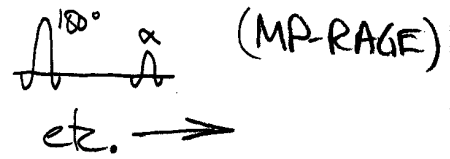
(shown as 3D sequence - possible with ones above, too)

NON-STEADY STATE, MAGNETIZATION-PRP.



nominal inversion time
effective TI actually time to TR that records center of k-space (k_y=0)

- preparation-pulse → strong T₁-weighting
- contrast varies in spatial-freq-dependent way



- longitudinal mag. not affect much by low angle pulses



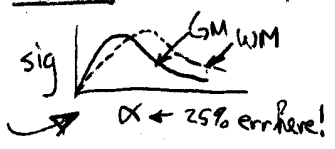
pulse-2b

QUANTITATIVE T1 — INTRO, METHODS

Motivation

HOW TO FIX:
Collect more than one copy of vol.

- image values are arbitrary/relative (diff seq's, manufacturers)
- uncorrected coil fall-off (receive inhomogeneity) can result in 2-3x differences in voxel brightness
- uncorrected variation in local B1 field can cause contrast variation
 - ↳ at 3T, B1 can vary by 25% across the brain
 - ↳ this can invert contrast in a fast gradient echo



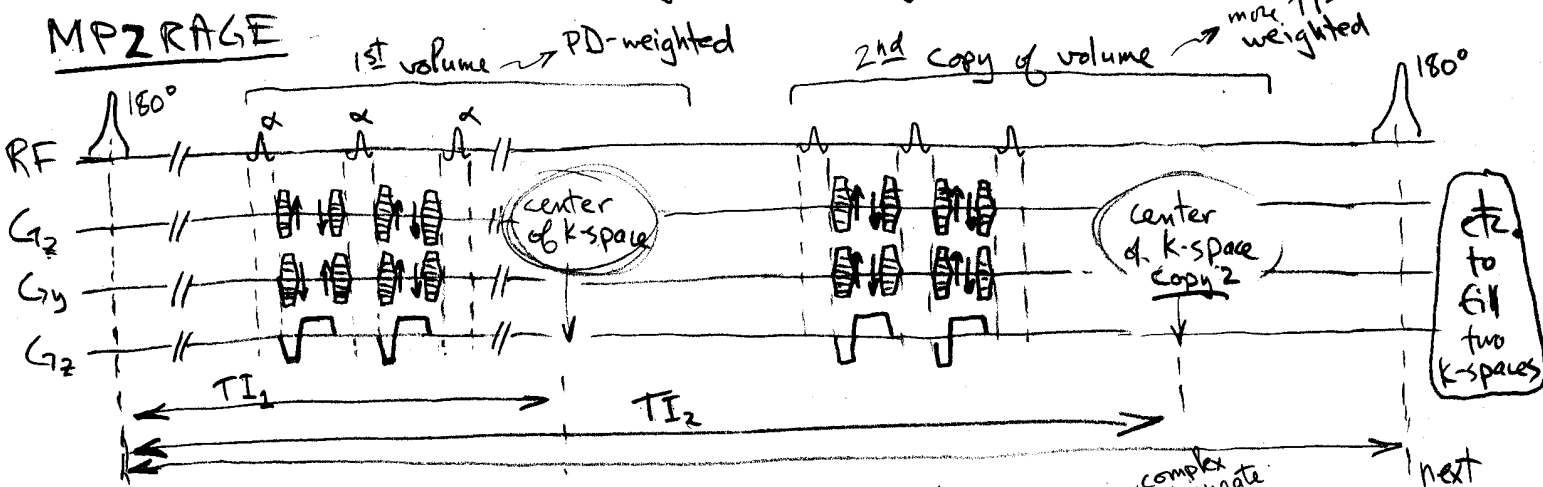
Pre-scan normalise

- collect lo-res GE image, receive w/ body coil (no coil fall-off)
- set parms. to get low GM/WM contrast
- collect data scan (e.g. MPRAGE) w/ surface coils, strong GM/WM
- use ratio between scans to generate smooth correction field

T1 divided by T2

- MPRAGE → strong T1-contrast
- SPACE → T2-weighted (no T1 weighting)
- T1/T2 removes coil fall-off
- Problems
 - ↳ distortion different in GE (MPRAGE) and SE (SPACE)
 - ↳ noise in regions of low signal

MP2RAGE



- N.B. SSFP-like in partition, phase-encode directions
- convert to -0.5 to 0.5 image: $S = \text{real} \left[\frac{\vec{S}_{TI_1}^* \cdot \vec{S}_{TI_2}}{\|\vec{S}_{TI_1}\|^2 + \|\vec{S}_{TI_2}\|^2} \right]$
- calc. PD & T1 from above cf. 2 flip angles

$$S = \text{real} \left[\frac{\vec{S}_{TI_1}^* \cdot \vec{S}_{TI_2}}{\|\vec{S}_{TI_1}\|^2 + \|\vec{S}_{TI_2}\|^2} \right]$$

pulse-2c

QUANTITATIVE T1 - HELMS 2-FLIP ANGLE METHOD

- start w/ gradient echo signal eq., dropping T2-decay $\rightarrow e^{-TE/T2}$

$$S_{Ernst} = A \cdot \sin \alpha \cdot \frac{1 - e^{-TR/T1}}{1 - \cos \alpha \cdot e^{-TR/T1}}$$

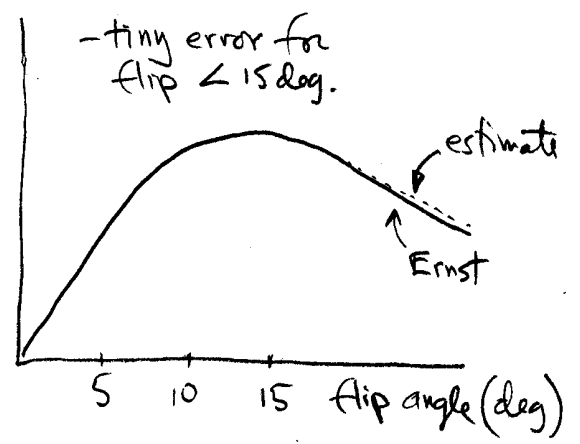
Ernst eq.
 (max: $\cos \alpha_E = e^{-TR/T1}$)
 "Ernst angle"
 ($\alpha_E = \cos^{-1}(e^{-TR/T1})$)

- Simplify/linearize/estimate

$TR \ll T1$
 linear approx. of exponentials
 Taylor expansion simplification of sin, cos, drop small terms

Helms et al. (2008)

$$S \approx A \cdot \alpha \cdot \frac{TR/T1}{\alpha^2/2 + TR/T1}$$



- solve for T1 and A (proton-density) given signals from 2 diff flip angles

(max: $\alpha^2/2 = TR/T1$)

2 flip angles

$$T1_{est} = 2TR \frac{S_1/\alpha_1 - S_2/\alpha_2}{S_2\alpha_2 - S_1\alpha_1}$$

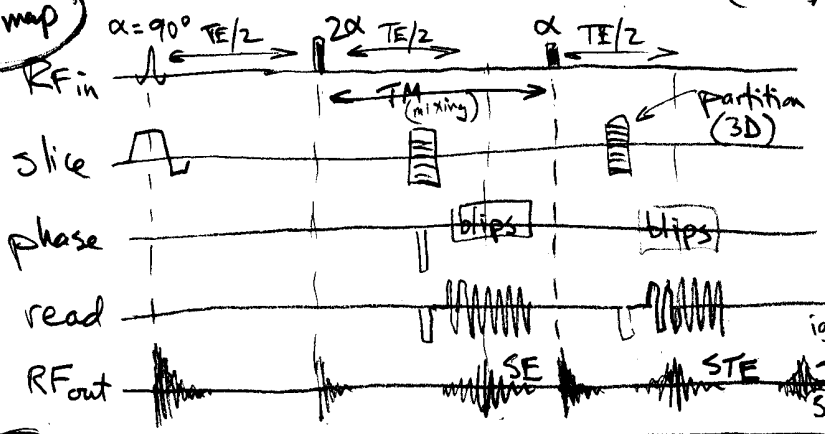
$$A_{est} = \frac{S_1 S_2 (\alpha_2/\alpha_1 - \alpha_1/\alpha_2)}{S_2 \alpha_2 - S_1 \alpha_1}$$

- problem: flip angle varies a lot at 3T (e.g. 25%) from nominal/requested (e.g. flip series)

B1 map

- acq. spin-echo and stimulated echo (EVI)

estimate T1, T2
 solve for 2 eqs
 insert $(\sin \alpha \cdot \sin^2(\frac{2\alpha}{2}))$



$$S_{SE} = k \cdot \sin^3 \alpha \cdot e^{-TE/T2}$$

$$S_{STE} = k/2 \cdot \sin^2 \alpha \cdot \sin 2\alpha \cdot e^{-TE/T2} \cdot e^{-TM/T1}$$

$$\alpha = \cos^{-1} \left(\frac{S_{STE} \cdot e^{-TM/T1}}{S_{SE}} \right)$$

T2* est

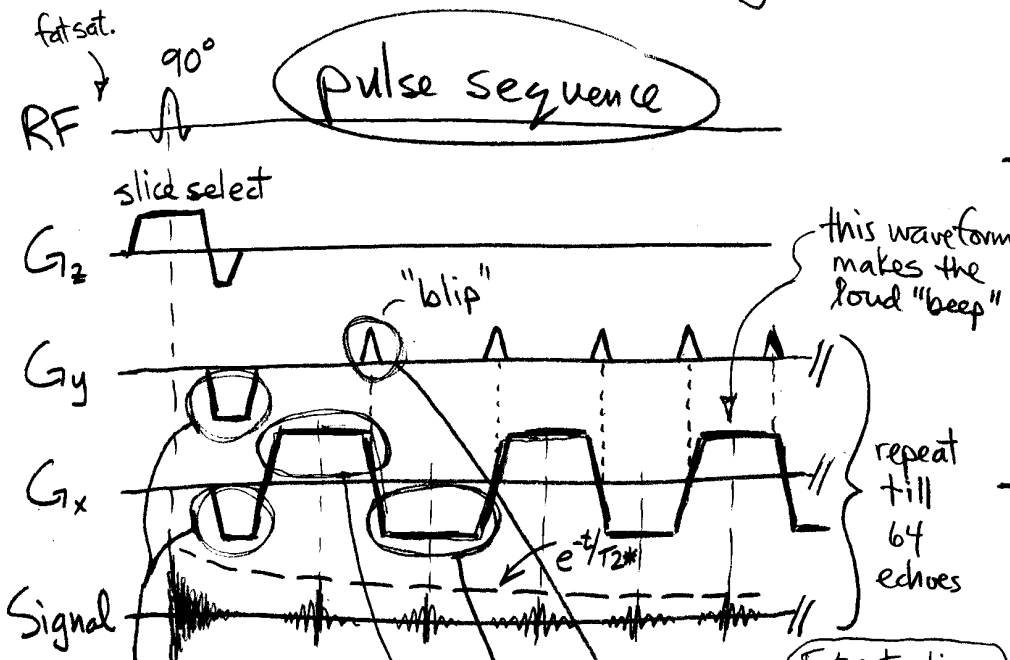
- add EPI-like echo train to each FLASH excit.

Jiru & Klose (2006)

Pulse-3

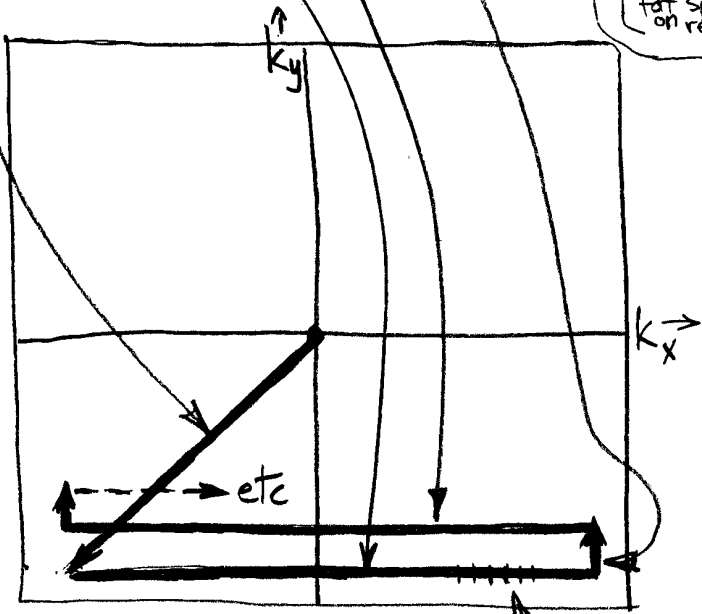
ECHO PLANAR IMAGING EPI (another fast gradient echo)

- single shot EPI collects all k-space lines (e.g. 64) after a 90° RF pulse using a train of gradient echoes



Fat saturation
 - before main 90°
 (fat res. 90°
 fat slice select
 fat spoiler grad on readout)

- since there is only one RF pulse per slice, spins never get reset to all-the-same (= zero freq, center of k-space)
- therefore, the recording point (Δt) in k-space (= spin phase stripe pattern) stays wherever the x and y gradients last left it



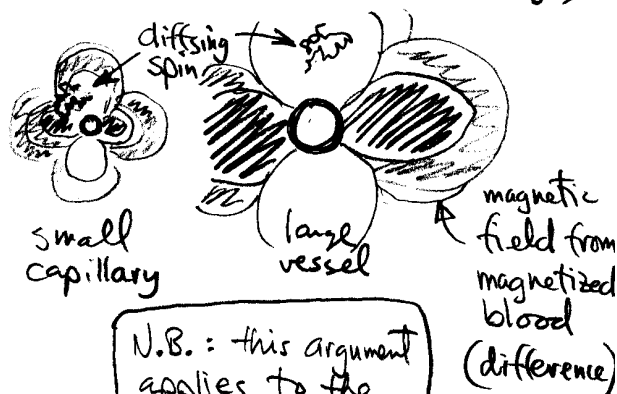
k-space traversal

individual time points of recording of one echo

- that explains why successive y phase-encode steps are achieved without changing the size of the G_y "blips"
- echoes are $T2^*$ -weighted (gradient echo)
- contrast mainly determined by echoes near center of k-space, which are only recorded after about 32 echoes

SPIN ECHO EPI why SE-BOLD may be selective for capillary bed

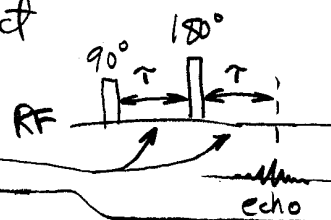
- standard EPI is a gradient echo method, which results in T_2^* -weighting
- deoxyhemoglobin is paramagnetic, which reduces signal in a T_2^* -weighted image due to greater dephasing
- the excess of oxyhemoglobin (probably the result of the need to drive O_2 into tissue, which requires more O_2 in the blood than is actually used) leads to the positive BOLD effect
- spin echo corrects (cancels) static T_2^* (T_2') dephasing, incl. deoxy
- if all spins stayed in the same position, spin echo would eliminate the BOLD effect by eliminating dephasing
- diffusion exposes spins to different fields (reducing gradient echo dephasing!)



N.B.: this argument applies to the extravascular signal

- magnetic field gradients produced by large vessels are smoother across space than those produced by small vessels
- for $TE \approx 100$ ms, spins diffuse 10's of μm , which is larger than diameter of small capillary, meaning that spins will likely experience different fields over time

- therefore, spin echo will be less successful at canceling BOLD effect near small vessels (BOLD effect will be reduced near large vessels where diffusion less likely to expose spin to different fields here)

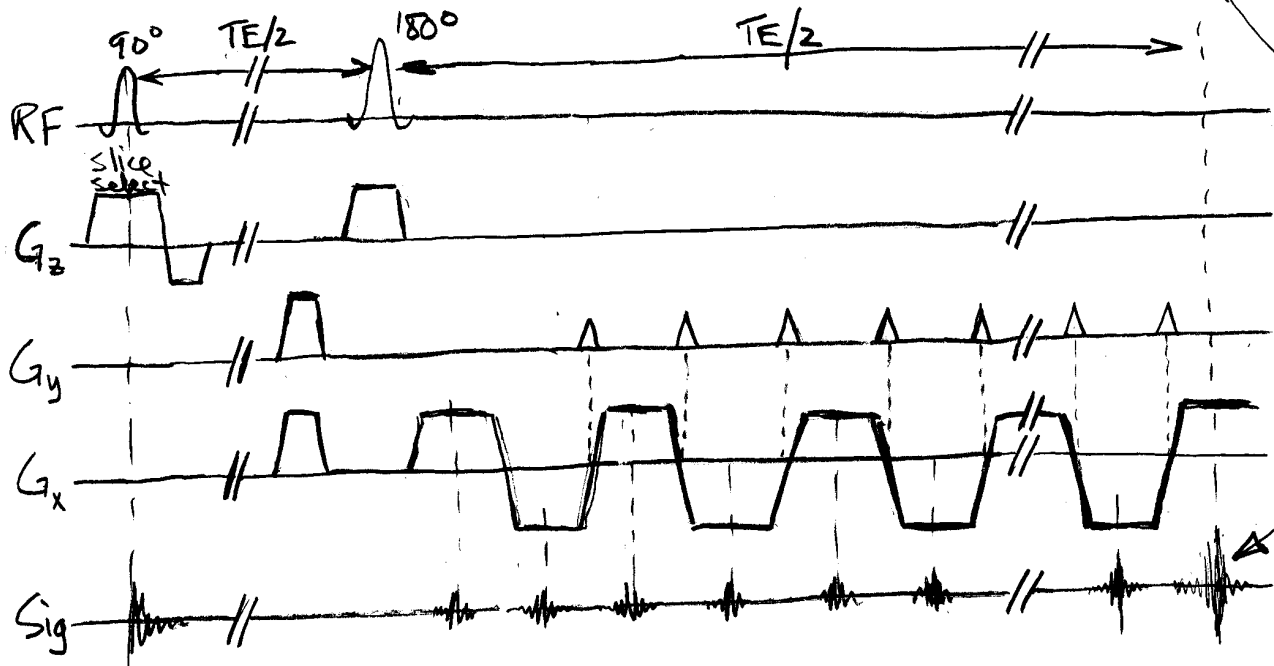
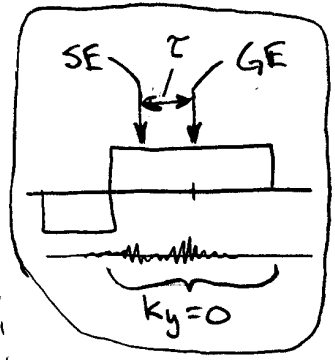


- this argument only works for extravascular spins — intravascular signal in BOLD is large (despite being only 4% by volume) because large gradient produced around red blood cells

→ measure intra/extra w/ bipolar pulse which kills signal in faster moving blood in moderate and larger vessels ⇒ over half of SE-BOLD at 1.5T is venous...

SPIN ECHO EPI

- EPI is a multi-gradient echo pulse sequence
- "spin-echo EPI" uses a 180° pulse to add a single spin echo to the contrast-controlling gradient echo through the center of k-space
- "asymmetric spin-echo EPI" arranges for the spin echo to occur τ msec before the gradient echo, which gives more T_2^* -weighting (for $k_y=0$ echo)



etc until k-space filled

combined gradient echo plus spin echo for $k_y=0$

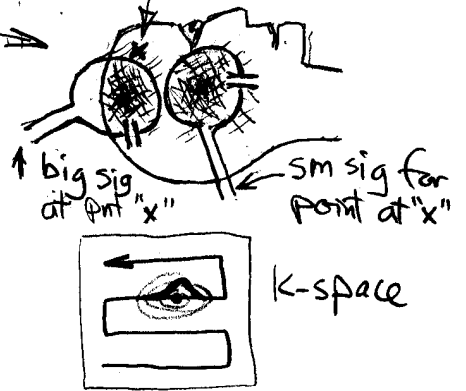
- the 180° -pulse rephasing reduces the T_2^* signal, which is why the partially rephased asymmetric spin echo has been more commonly used
- at higher fields, spin echo EPI is more promising
 - signal to noise is higher so we can take spin echo hit
 - contribution from venous blood is reduced, since blood T_2 is so short, we can let it decay away before recording

pulse-5b

COIL FALL-OFF / UNDERSAMPLE / GRAPPA / SENSE

- coil fall-off intuitively contains info about location
 if same brain location imaged by different coils w/ diff. fall-offs

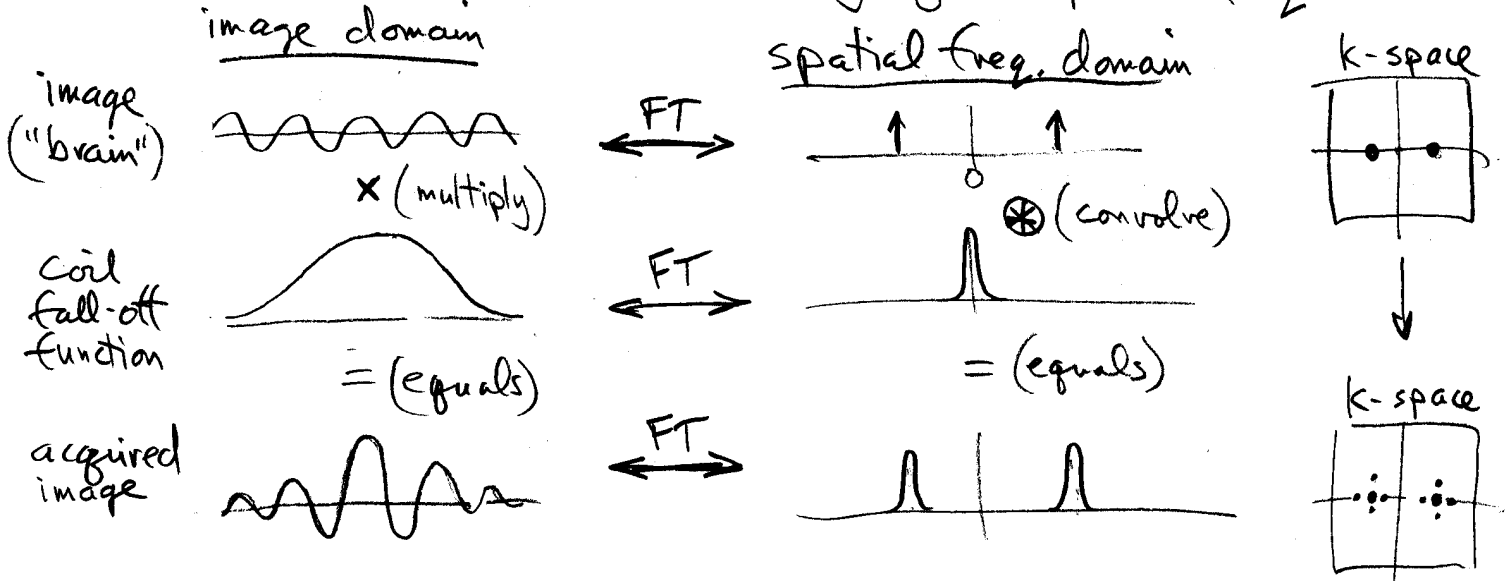
↳ but what does this look like in k-space?



- slow variation in RF-field fall-off (e.g. 1-4 cyc/FOV) causes a blur in acquired data in k-space
 (N.B. not addition!)

- to see this, consider multiplication by coil fall-off function in image space, which equals convolution (w/ FT of that function) in k-space - at all spatial frequencies !!

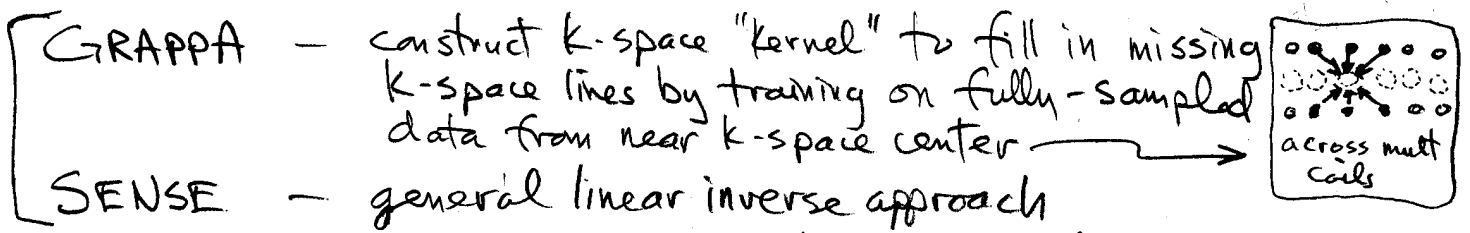
- simple example w/ "brain" consisting of one spatial freq.



- N.B. inverse FT of k-space data "smeared" in spat freq. space is sharp image w/ fall-off (not blurred img.)

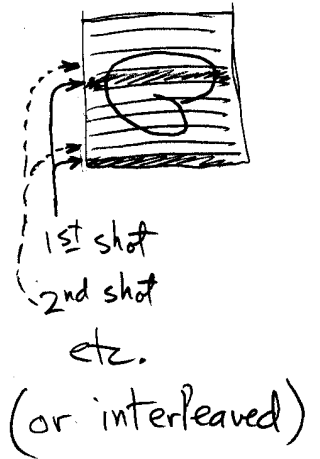
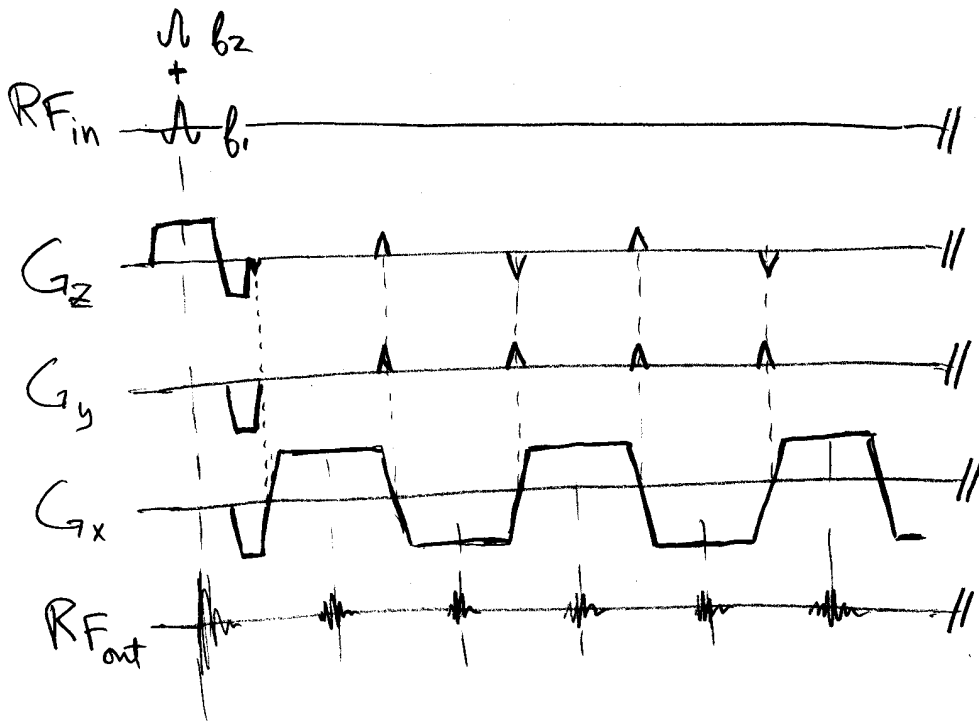
So can undersample k-space!!

- "smear" means normally orthogonal spat. freq's "leak" to adj. freqs.

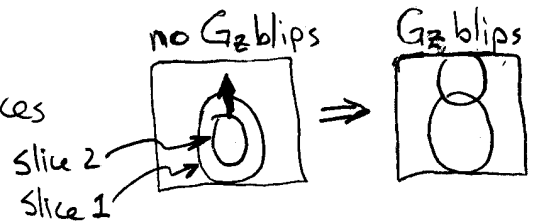


- N.B.: neither would work unless normally orthog. spat. freqs. blurred!

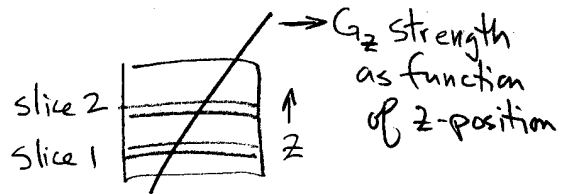
^{pulse-Seq}
SMS / MULTIBAND / blipped CAIP1



- excite multiple slices at once
- function of G_z blips is to shift slices in G_y direction



- this occurs because for given slice, a phase pedestal is added to the entire slice



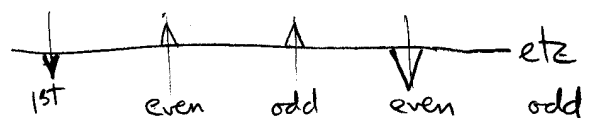
↳ this "Fourier Shift Theorem"
 ↳ [N.B.: different than B₀ defect-induced incremented phase errors]

- problem w/ all up G_z blips → phase error builds up

trick #1 - start w/ 2 slices, one at $z=0$, other above
 ↳ if π (180°) phase shift used, blip up/down same! (no effect at $z=0$)
 ↳ i.e., move top or bottom replica

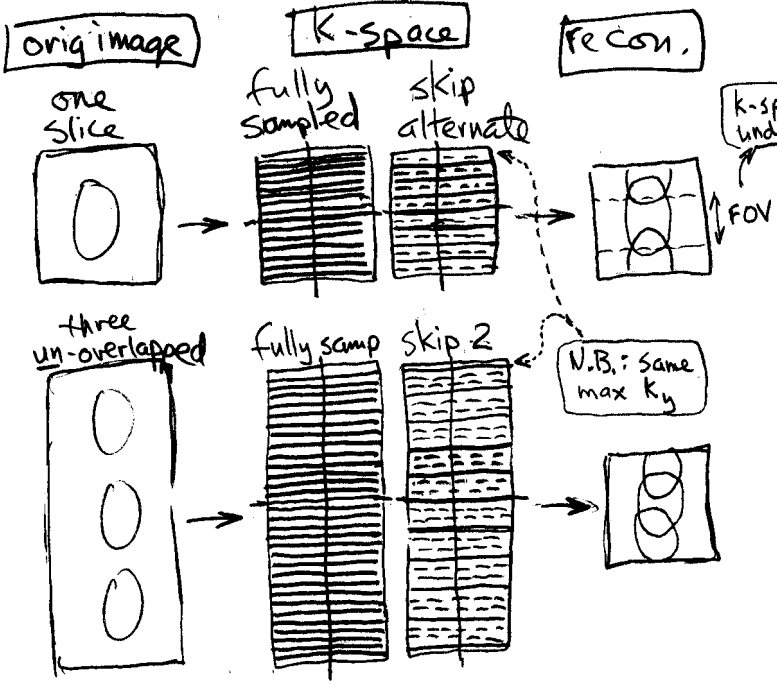
trick #2 - for multiple slices not all at $z=0$, phase no longer same for even/odd
 ↳ but can add phase to equilibrate to k-space before recon.

trick #3 - for more than 2 slices :



pulse-5d
MULTI BAND / BLIPPED CAIPI (cont.)

- relation between leave-one-out aliasing and nominally fully-sampled SMS



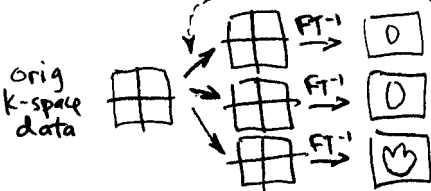
- leave alternate lines out wraps image
- SENSE/GRAPPA can fix (fill in) b/c local coil view smears k-space data to adjacent spatial frequencies
- nominally, w/ SMS we record every line of k-space
- but equivalent to leave alternate out b/c our multi-slice FOV was not big enough

- slice-GRAPPA

reg GRAPPA → fill in missing lines

slice GRAPPA → fill in multiple k-spaces for each overlapped slices by training on fully-sampled data at beginning of scan

i.e. not SMS



- interslice "leakage block"

when training GRAPPA kernel on fully-sampled data, also minimize interslice leakage (split-slice-GRAPPA)

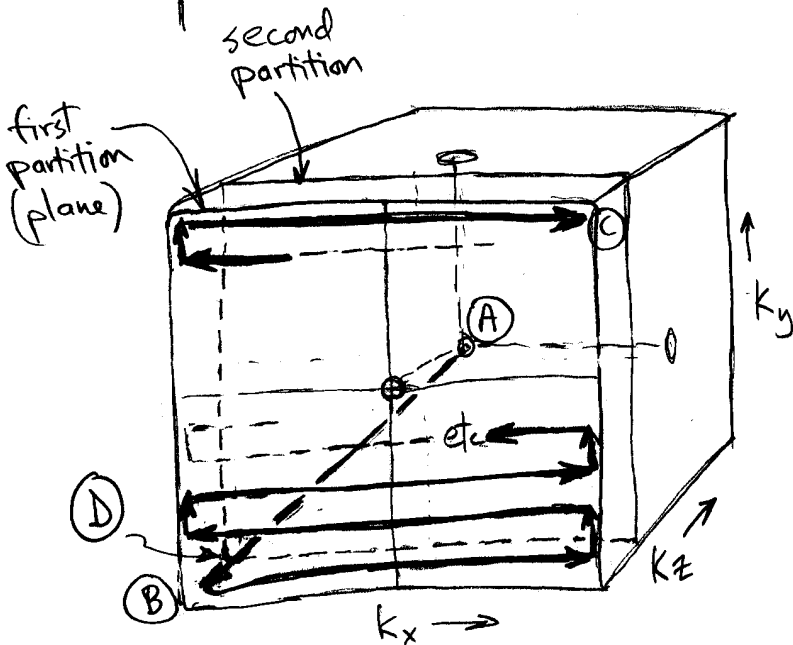
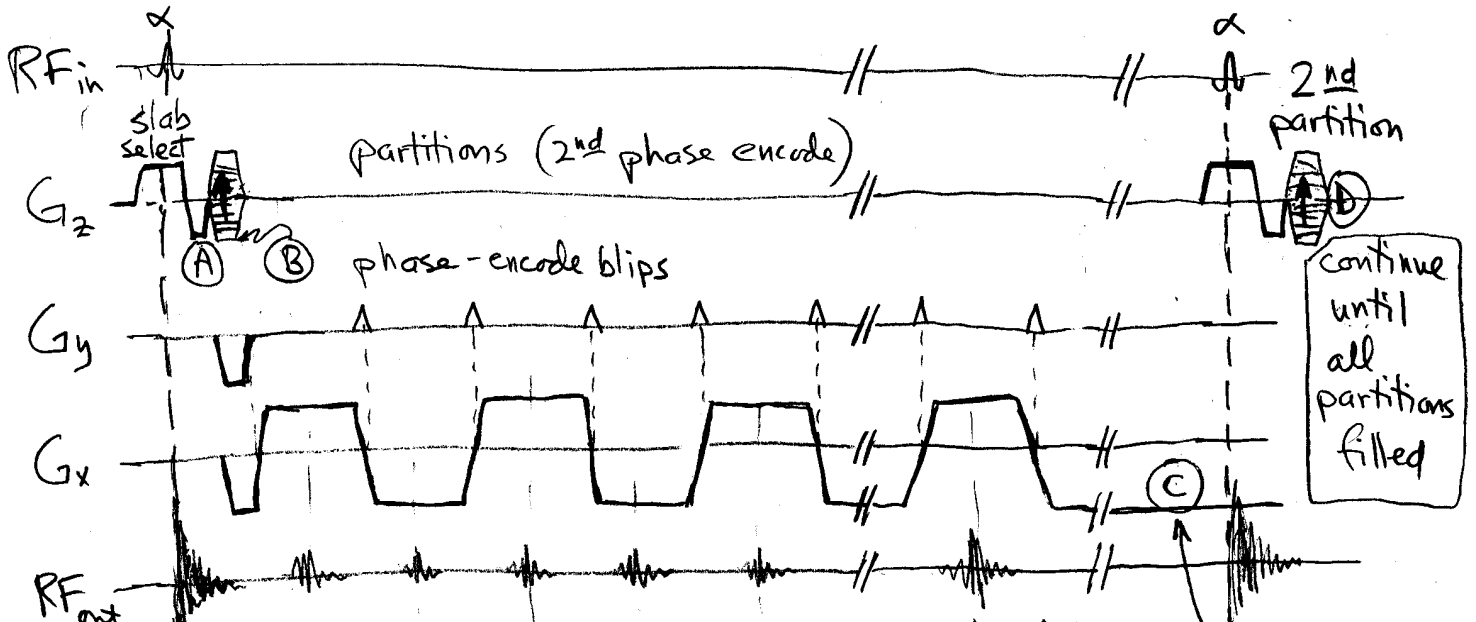
can also do regular GRAPPA on top of this

reason: for diffusion, loss in S/N from undersample cancelled by shorter TE readout (bigger signal)

also, gain from reduced moire distortion from shorter k_y readout

^{pulse-se}
ECHO-VOLUME IMAGING EVI

- multi-shot (like FLASH) but acquiring one plane of 3-D k-space per shot (can do spin echo, too)



center of k_x, k_y for this k_z partition: TE_{eff}

finished the first partition

- main issue is movement artifact since data assembled from many shots over several secs
- breathing-induced B_0 problems in different partitions may cause blur

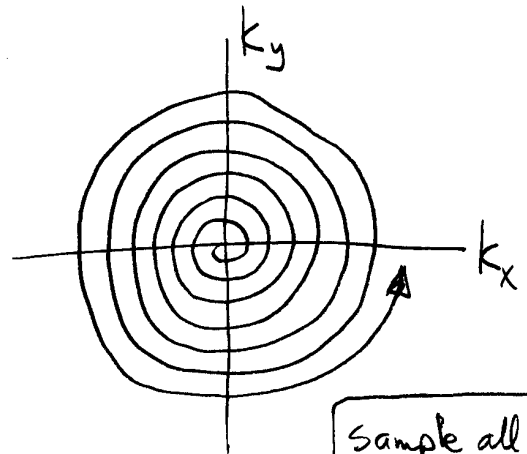
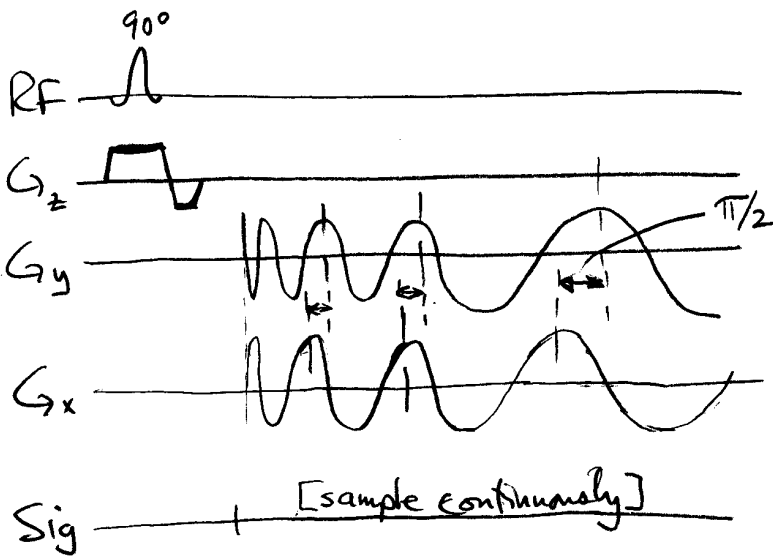
- entire k-space must be filled before 3D image is reconstructed
- since entire volume is excited each shot, potentially higher S/N
- must use smaller flip angle to avoid killing M_L since entire volume excited every partition (e.g every 80 msec)

SPIRAL IMAGING

- by using smoothly changing gradients (sinusoids) less gradient power required than w/ trapezoids (less eddy currents)

earlier EPI hardware like this: sinusoidal gradient waveform from resonant circuit w/ non-uniform sampling to get constant Δk_x

- sinusoids in both G_x and G_y give spiral k-space trajectory



Sample all orientations of each spatial frequency while slowly increasing spatial freq.

- constant angular velocity goes too fast at large k_x, k_y
- constant linear velocity better but impractical near $k_x=0, k_y=0$
- compromise: start constant angular, end constant linear \rightarrow

Constant angular velocity

$$\omega(t) = \omega_0 t$$

$$\mathbf{k}(t) = A t e^{i\omega_0 t}$$

$$\mathbf{G}(t) = \frac{1}{\gamma} \frac{d}{dt} \mathbf{k}(t)$$

$$= A e^{i\omega_0 t} + i A t \omega_0 e^{i\omega_0 t}$$

$$G_x(t) = A \cos \omega_0 t - A t \omega_0 \sin \omega_0 t$$

$$G_y(t) = A \sin \omega_0 t + A t \omega_0 \cos \omega_0 t$$

Constant linear velocity

$$\omega(t) = \omega_0 T E$$

$$\mathbf{k}(t) = A T E e^{i\omega_0 T E}$$

$$\mathbf{G}(t) = \frac{1}{\gamma} \frac{d}{dt} \mathbf{k}(t)$$

$$= \frac{A}{2T} e^{i\omega_0 T E} + \frac{A}{2} \omega_0 e^{i\omega_0 T E}$$

$$G_x(t) = \frac{A}{2T} \cos \omega_0 T E + \frac{A}{2} \omega_0 \cos \omega_0 T E$$

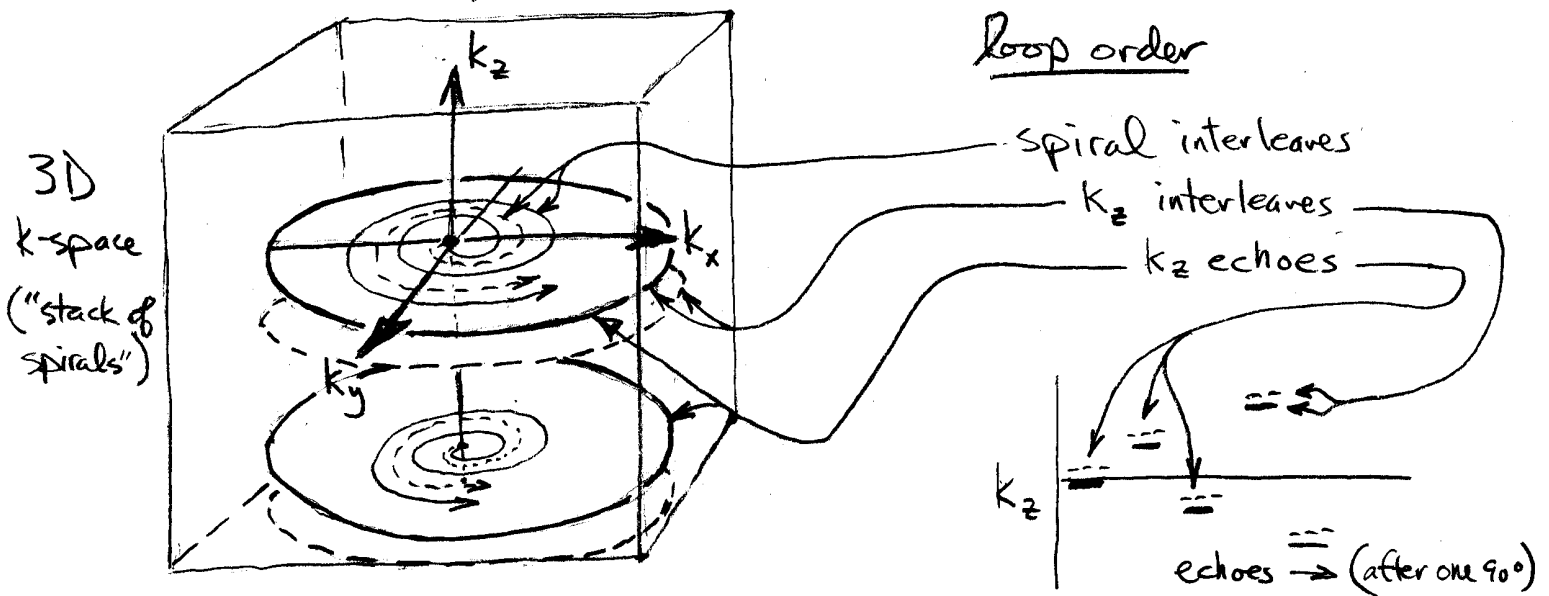
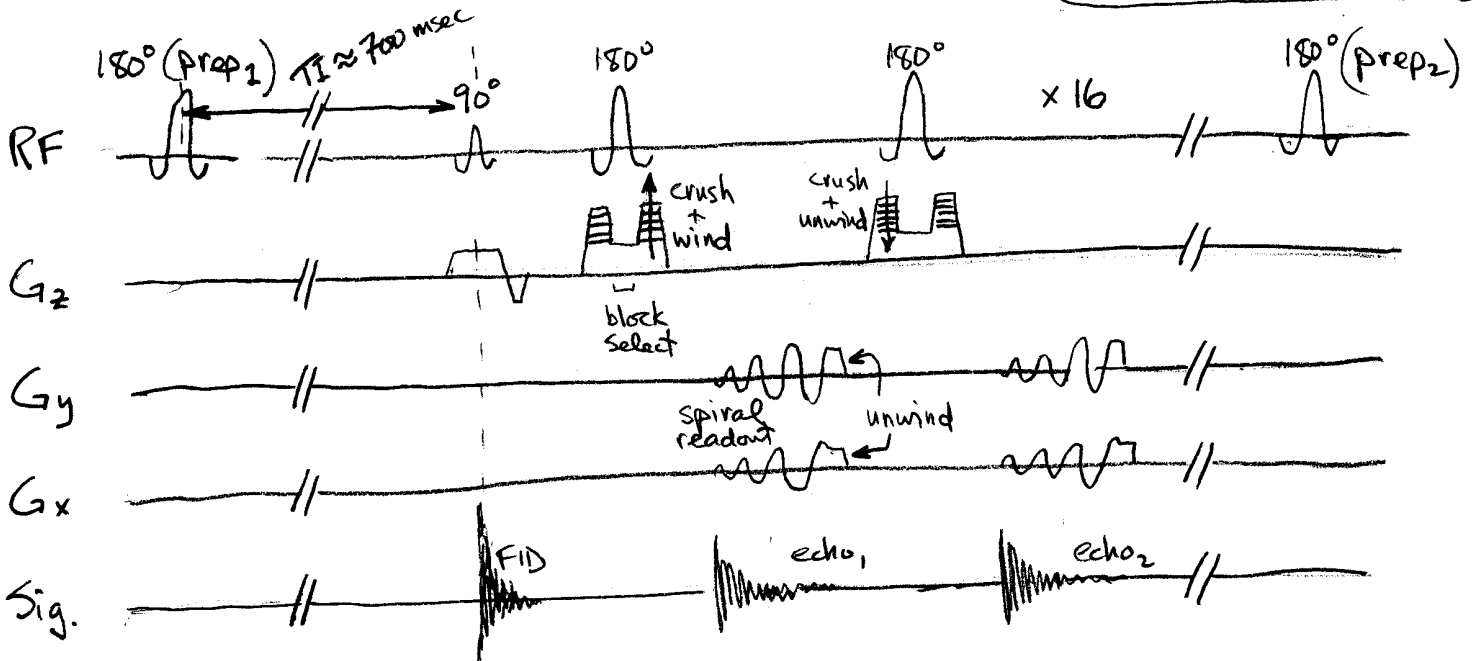
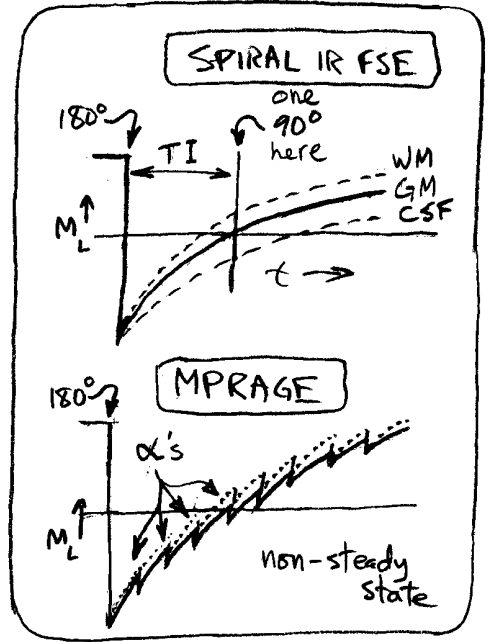
$$G_y(t) = \frac{A}{2T} \sin \omega_0 T E + \frac{A}{2} \omega_0 \sin \omega_0 T E$$

pulse - 7

SPIRAL 3D IR FSE (from Eric Wong)

- 3D: block select vs. slice select
- FSE: multiple echoes from one 90°
- spiral: multiple spirals vs. multiple lines
- interleaved spirals (like FSE interleaves)
- true IR (vs. MPRAGE)

all echoes after 90° derive from mag w/ same T1 contrast (vs. non-steady-state)
- possible to preserve sign
- high, uniform contrast, but lots of waiting (TI), high BW



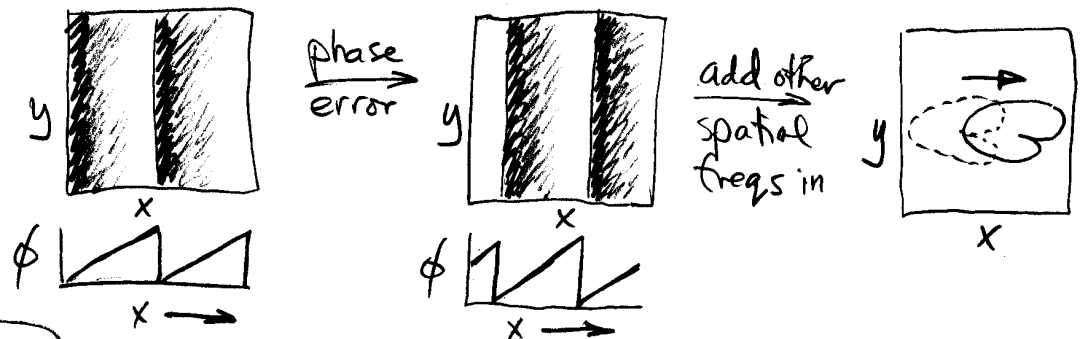
PHASE ERRORS & ECHO-CENTERING ERRORS

Phase Errors

anything that causes a deviation of the B_z field strength from the expected value ($B_{0,z} + G_{x,z}x + G_{y,z}y + G_{z,z}z$) changes precession frequency and therefore, expected phase angle

- incorrect phase of spatial frequency stripes results in a shift in space in the magnitude image after reconstruction

phase stripes in image domain (one k-space point)



Fourier (phase) shift theorem
phase shift in spatial freq. domain causes spatial shift in image domain

$$I(x-x_0) = \int_{k_x} e^{-i2\pi k_x x_0} S(k_x) e^{i2\pi k_x x} dk_x$$

x -offset in image phase shift in signal k -space signal

multiply by complex same as add to exponent: $x-x_0$

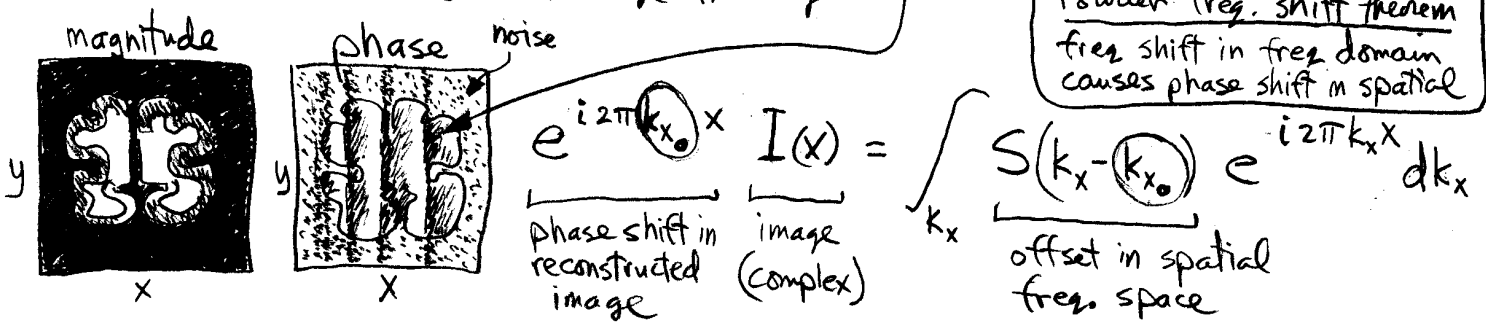
N.B.: this is a "pedestal" of phase, not a gradient

- first defense: freq prescan
- refine w/ shimming and B_0 -mapping/phase unwrapping before reconstruction

Echo Centering Error

- if realignment of all spins ($k_x=k_y=0$) doesn't occur at the middle of read gradient, echo is shifted
- since echo is in spatial frequency domain, this is frequency shift
- spatial frequency shift results in wrapping in phase image after reconstruction
↳ magnitude image unchanged

Fourier freq. shift theorem
freq shift in freq domain causes phase shift in spatial



FAST SCAN ARTIFACTS

EPI vs. Spiral

brain-induced field defects lead to phase errors

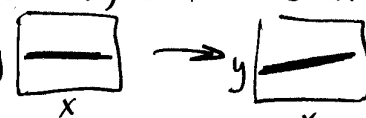
EPI

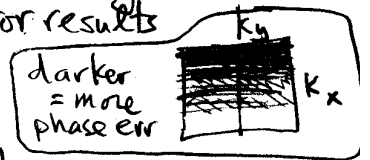
- G_x readout gradient strong \rightarrow [field defects smaller percentage
less deformation of k_x (vertical stripe components)]
- G_y "blips" are weak and total G_y record time much longer (5 times) than standard readout (50 ms vs. 10 ms)
- an extra gradient in the x-direction, for example, wraps and unwraps phase as a function of x-position
- but G_x big, so effect on freq.-encode direction is much less than on phase-encode direction, where error accumulates

the lack of blurring has led to a preference for EPI, despite the substantial image shifts

- for a given x-position, the strength of the spurious gradient is constant, so the accumulation of phase error results in a shift in the y-direction (=k-space spin-stripe displ.)

- the phase error causes a shift in the y-direction proportional to x-gradient strength (=shear) but no blurring

(N.B. shift varies w/x-position) 

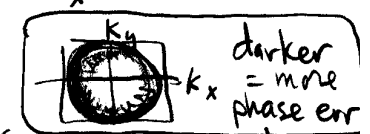
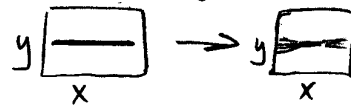


Spiral

- with center-out spirals phase errors accumulate in a radial direction \rightarrow

- thus, higher spatial frequencies have more error (=more shearing)

- for spurious x-direction gradient as above, there is a radial blurring, rather than a vertical shift because higher frequency phase stripes misaligned relative to low spatial freq



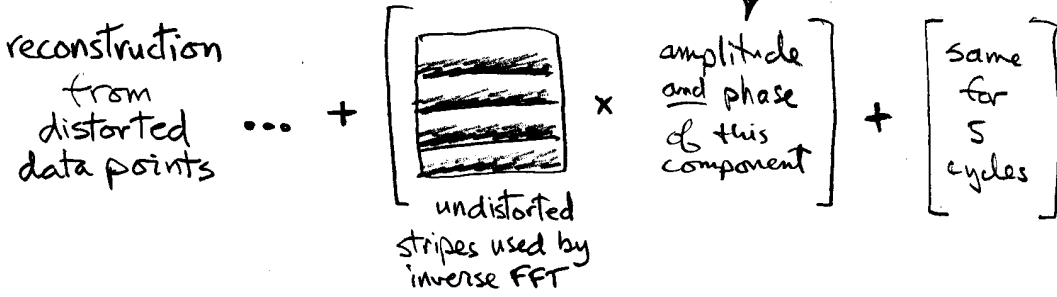
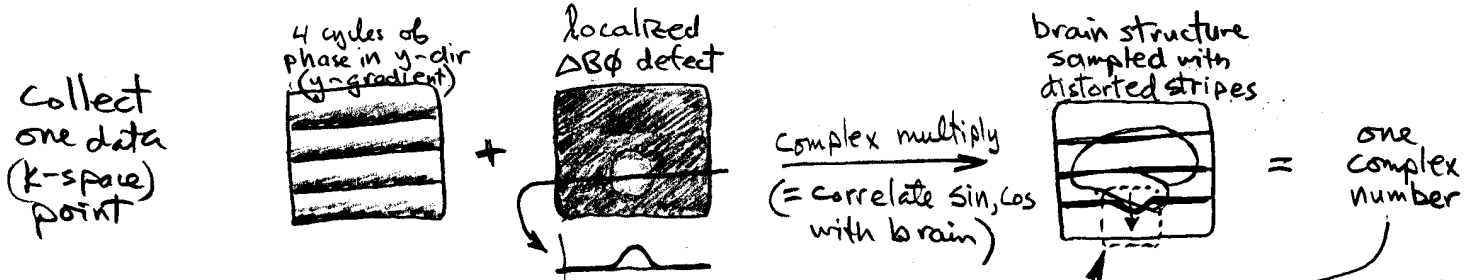
- for defects with more complex contours in the y-direction (than linear, as above) the vertical shifts (for EPI) will vary with y-position, and may result in signals from different y-positions being reconstructed on top of each other

artifacts-1b

IMAGE-SPACE VIEW OF LOCALIZED B_0 DEFECT, EFFECT ON RECON

- localized B_0 defects often arise from air pockets embedded in tissue

[air in middle/outer ear \rightarrow indentation in inferior temporal lobe
 air under olfactory epithelium \rightarrow orbitofrontal ctx, ant. thal. compression



garden path:
 seems like this would cause spatial shift
 ↓
 - stripe compression is a local increase in spatial freq.
 - N.B.: if all freq's increased same amount, however, this is ex. of Fourier Freq. Shift Theorem \rightarrow i.e. no amp. image shift! (only ϕ)
 - But if phase error (stripe compression) incremented for successive freq's, shift occurs (See next page)

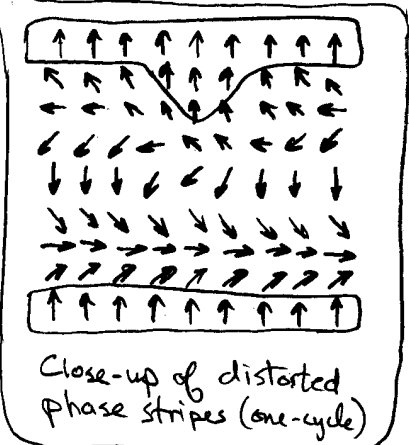
- same defect makes leftward dent in vertical phase stripes



- spatial information can be lost when continuous changes in phase are flattened by B_0 defect



- shifts can pile multiple pixels on top of each other into one bright pixel



- local estimates of ΔB_0 needed to correct images

- 1) fieldmap method: $\left\{ \begin{array}{l} \text{multiple TE's to est. local } \Delta B_0 \text{ from } \phi/TE \text{ slope} \\ \text{shift each image pixel proportional to } \Delta B_0 \text{ in phase-encode dir.} \end{array} \right.$
- 2) point-spread-function: $\left\{ \begin{array}{l} \text{extra phase encode to estimate P.S.F. (should be } \delta\text{-function)} \\ \text{deconvolve distorted image in phase-encode direction} \end{array} \right.$

LOCALIZED B_0 DEFECT, EFFECT ON RECON (2)

- when local B_0 defect disturbs image space phase stripes during signal acquisition, estimates of local spatial freq. are affected (compressed stripes = higher spat. freq.)

- if each successive k_y line recorded w/ same echo time (e.g. w/ single line phase encoding) this will correspond to constant spat. freq. offset in k-space

- a k-space freq. offset only results in image space phase shift (Fourier freq. shift theorem), which is invisible in amplitude image (cf. echo cent. error)

- however, with w/EPI, static B_0 defect causes more and more local displacement of image phase stripes for each additional k_y line

↳

- that is, later lines have greater spat. freq. offset
- effectively stretches k-space in k_y direction
- same num samples to higher spatial freq. shrinks FOV (squishes voxels - see FOV page)

- when image is reconstructed, region with local B_0 defect shifted oppositely

- Thus, local shift effect due to combination of 3 things:

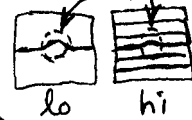
1) static local ΔB_0 defect

2) successive increases in phase error for successive spat. freq. measurements during long EPI readout

3) small size of k_y phase encode blips relative to B_0 defect (much less of this effect in freq. encode direction)

- respiration (which affect B_0) in 3D FLASH might cause similar effect within k_z partition (if successive spat. freqs.)

N.B. B_0 affects image phase of all spatial frequencies. If we add, e.g., 90° phase, this means higher freq. image stripes move less since each cycle covers less space: ΔB_0



artifacts - 2

GRADIENT NON-LINEARITIES

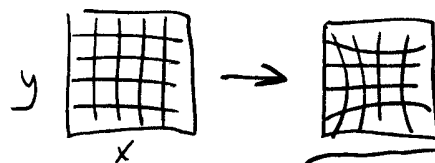
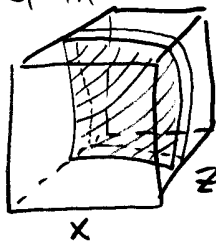
B_z
 B_x, B_y

- ideally the G_x , G_y , and G_z gradient coils attempt to impress a linear variation onto the z-component of the B field — B_z — in the x, y, and z-directions
- in practice, gradient coils are non-linear (esp. printed-circuit-like)
- non-linearities are worse in smaller coils, but also in higher performance coils, designed for post-processing correction of distortions
- non-linearities result in phase errors, which result in 3-D image distortion

these effects do not build up over time in phase-encode direction since they only occur when gradients are turned on.

Fourier shift theorem

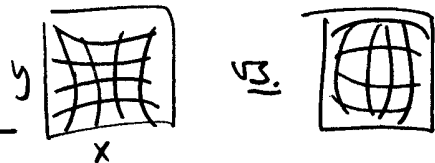
- a non-linear slice-select gradient will excite a curved slice
- non linear phase and frequency encode gradients will distort in-plane features



- some scanners correct these differently for 3-D scans (all directions), 2-D scans (just in plane), and EPI scans (no corrections!)

these distortions are predictable and can be corrected

- this can result in errors approaching 1 cm in funct-struct overlays
- different coil designs have different directions of distortion (!)



- the assumption of non-Maxwellian gradients results in additional phase errors

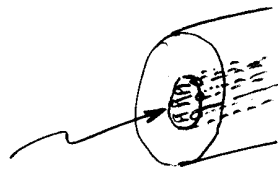
- these can also be corrected since the B_x and B_y components are known

that is, the assumption that gradients cause no field in the B_x and B_y direction

artifacts - 3

SHIMMING AND B_0 -MAPPING

- passive iron shims inserted to flatten B_0 field
- additional coils (usu. in the gradient coils) can be statically energized in an attempt to flatten the B_0 field (a few ppm good)
- primary use is to compensate for defects in flatness present without a sample in the magnet (geometric imperfections, impurities in metal, etc) (= several hundred ppm)

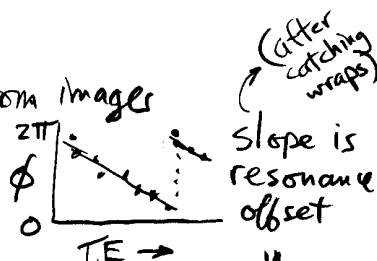


[linear shim coils impose gradients in x , y , and z
 higher order shims impose higher order spherical harmonic field components (e.g. z^2)]

- secondary use is to compensate for inhomogeneities caused by introducing the sample into the B_0 field

- local resonance offsets caused by B_0 defects estimated from images

↳ e.g., sample phase at multiple echo times



- fit defective field using combination of fields generated by shim coils. then add these corrections to base shim currents

↳ this only corrects spatially gradual field defects
 ↳ local defects due to air in sinuses much higher order than shims

- after shimming, field map measured again

because:
 longer time to echo means more time for phase to be retarded (or advanced) by B_0 defects

- image voxel displacements calculated from resonance offset map are used to unwarped the reconstructed magnitude image

- for EPI images, assume displacements all in phase-encode direction (since freq encode gradient is strong relative to defects)

artifacts-4

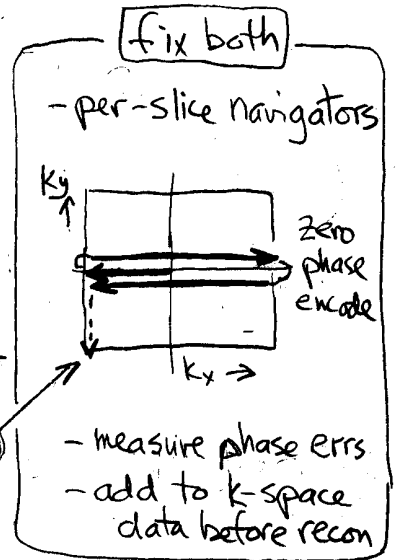
NAVIGATOR ECHOES

- 1D navigator

B ϕ drift problem

- slow up/down drifts in B ϕ continuously occur
- a pedestal in B ϕ is pedestal in phase (not gradient) which causes spatial shift (Fourier shift theorem)
- in EPI, mainly affects phase-encode dir b/c small blips / long readout
- result is successive volumes drift in phase encode dir

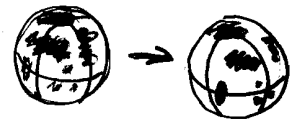
daily B ϕ decay (e.g. 0.05 ppm/hr)
passive shim heating by gradients



Gradient balance problem

- unequal L/R readout gradients cause L/R shift in position of even/odd lines in k-space causing N/2 (Nyquist) ghosting \rightarrow another phase error

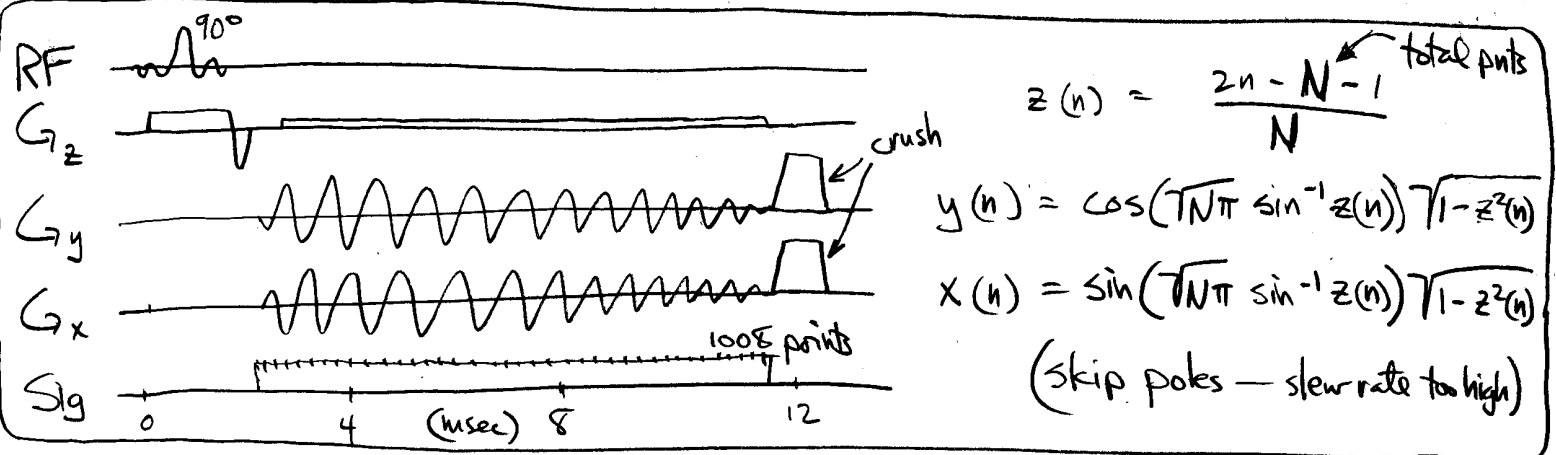
- 3D navigator: collect 3D sphere in k-space



rotation of object \rightarrow rotation of k-space amplitude pattern
translation of object \rightarrow phase shift of k-space phase (Fourier shift)

- sample at sufficient ^{k-space} radius to pick up high spatial freq features
- N.B.: excite whole volume
- do N,S hemispheres separately (less T $_2^*$, cancel EPI-like error accumulation)
 \hookrightarrow equator \rightarrow up, equator \rightarrow down

Welch et al. (2002) MRM \rightarrow



- can be used for prospective motion correction (rotate, translate w/ gradients)
- better estimate, because of speed, than full TR of EPI images (27 ms vs. 2-4 sec)
- may need to smooth rot, trans estimates across time (e.g. Kalman filter)

artifacts-5

RF FIELD INHOMOGENEITIES

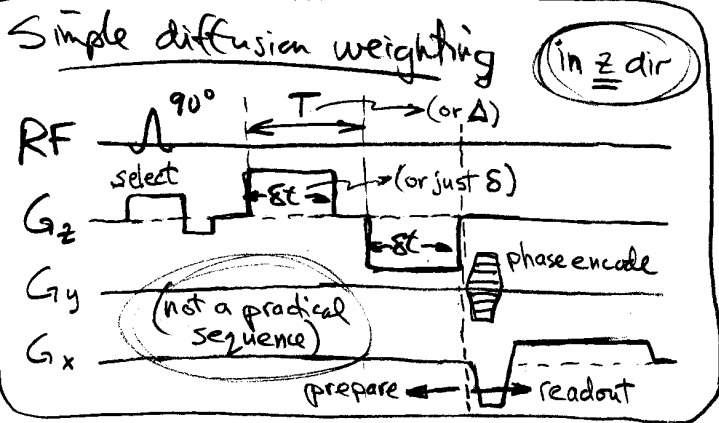
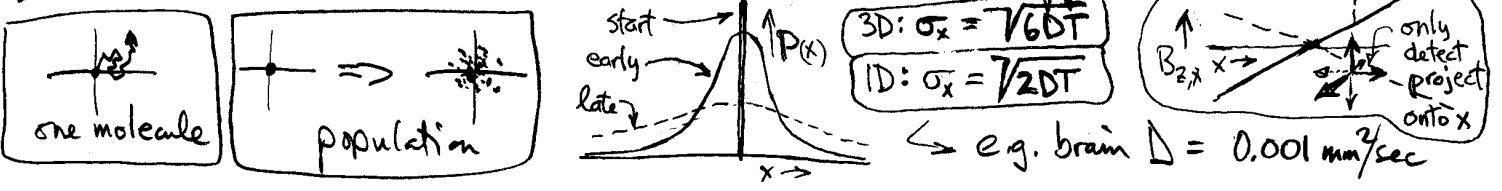
B_1 inhomogeneities

- receive coil inhomogeneities alter the amplitude of the received signal, altering the reconstructed proton density in a spatially varying way
 - ↳ variations can be used (cf. GRAPPA, SENSE) and/or corrected
 - transmit coil inhomogeneities affect the flip angle in a spatially varying way (can affect contrast: FLASH)
 - ↳ potentially worse (why local transmit is still in progress)
 - ↳ usu. fixed by using a large transmit coil (e.g. body coil)
 - RF penetration at higher fields (= higher RF frequencies) is less uniform:
 - 1) decreased RF wavelength (closer to size of head) at higher freq.
 - 2) increased permittivity (ϵ) and conductivity (σ) at higher field
 - 2nd advantage of the falloff in signal recorded with a small, receive-only RF coil is better signal-to-noise (less noise received from other parts of brain)
 - different sensitivity functions from different coils can be used to scan less lines in k-space (GRAPPA/SENSE/SPACE-RIIP)
 - ↳ lin inv after IDFT
 - Normalization ("pre-scan normalize")
 - record lo-res volume (b/c coil fall-off is smooth) through both body coil and small coil(s)
 - divide $\frac{\text{small coil}}{\text{body coil}}$ at each voxel to determine receive field
 - use receive field to normalize main image(s)
- [see also: gT_1 , MP2RAGE, T_1/T_2]



DIFFUSION - WEIGHTED IMAGING

classical diffusion coefficient
time for diffusion



- assume Gaussian diffusion
- spins acquire phase during first δt
- if spins diffuse (= move) along gradient by time T, signal is lost because negative δt doesn't re-phase

attenuation: $A(D) = \frac{\int_{-\infty}^{\infty} S_{\omega} d\omega}{\int_{-\infty}^{\infty} S_{\omega}^0 d\omega} = e^{-bD}$

where $b = \gamma^2 G^2 \delta t^2 (T - \delta t/3)$

Summarizes gradient amp, length, delay

- "apparent diffusion coefficient" → calculate from $b=0$ image and at least 6 b ="large" (e.g. 1000) images
- after obtaining 3×3 tensor, calc eigenvectors/values to find orientation & shape of diffusion ellipsoid
- two useful scalar values from 3 eigenvalues:

apparent diffusion coefficient mean diffusivity

$ADC = MD = (\lambda_1 + \lambda_2 + \lambda_3)/3$

fractional anisotropy

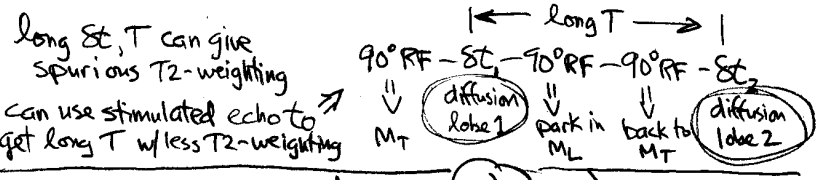
$FA = \sqrt{\frac{(\lambda_1 - \lambda_2)^2 + (\lambda_2 - \lambda_3)^2 + (\lambda_1 - \lambda_3)^2}{2(\lambda_1^2 + \lambda_2^2 + \lambda_3^2)}}$

(0-1)

- to get large b , need large $G, \delta t, T$

1) Anisotropic Diffusion (Gaussian)

- measure D along multiple axes
- have to measure tensor, not scalar
- ↳ even for determining one primary direction



$D = [u_x \ u_y \ u_z] \begin{bmatrix} D_{xx} & D_{xy} & D_{xz} \\ D_{yx} & D_{yy} & D_{yz} \\ D_{zx} & D_{zy} & D_{zz} \end{bmatrix} \begin{bmatrix} u_x \\ u_y \\ u_z \end{bmatrix}$

$DE_n = \lambda_n E_n$ get eigenvectors & eigenvalues, λ

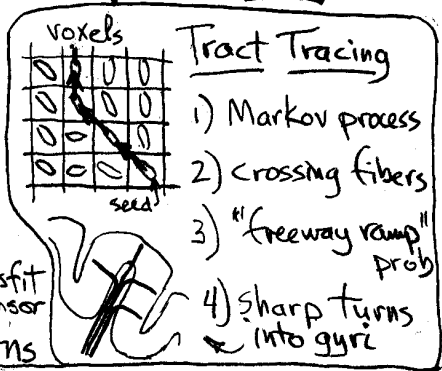
- isotropic: off diag = 0, diag equal
- since D is symmetric, need minimum of 6 diff. measurement directions
- without 3rd number (z) x & y projections same

$D = U^T \cdot D \cdot U$

scalar diffusion diffusion tensor measurement direction

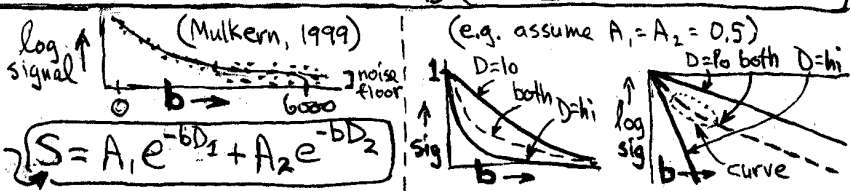
Diffusion Surface (non-Gaussian)

- need to measure diffusion in many directions (>6) to properly characterize even 2 main directions
- fit w/ spherical harmonics
- misfit tensor



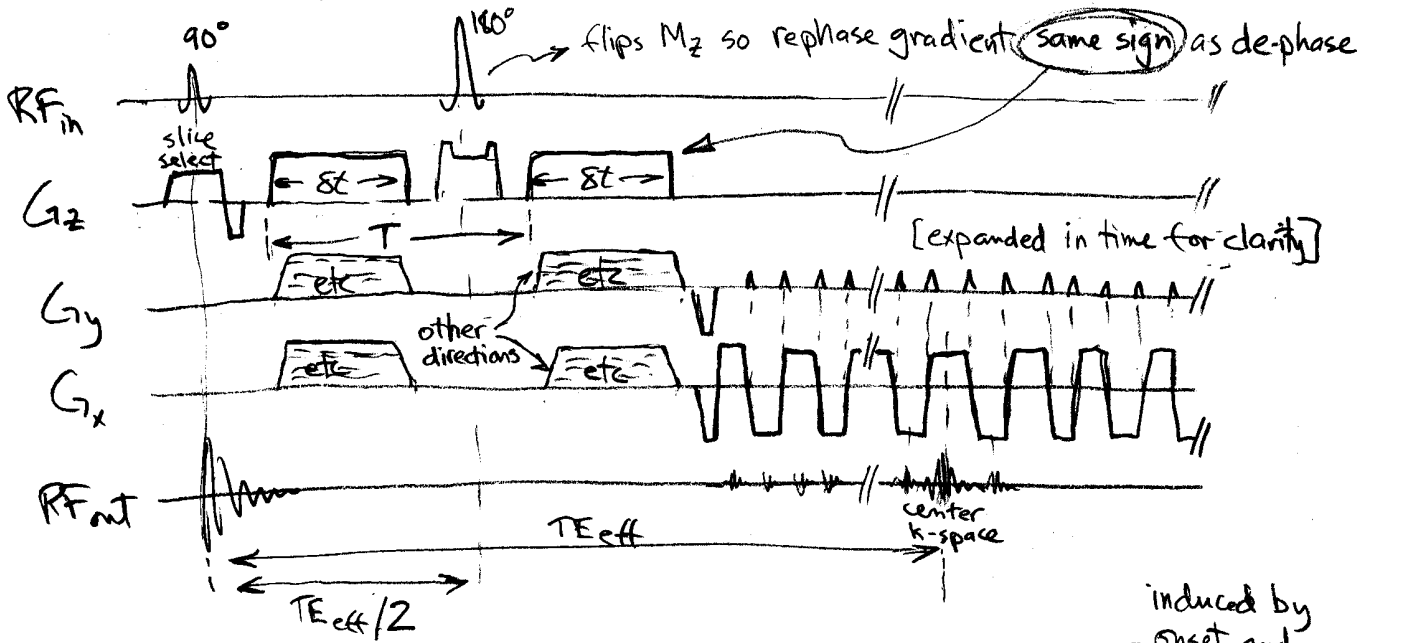
2) Length Scale by multiple b-values

- fit line to semilog signal as funct of b
- if not straight line: multi-exponential, e.g.
- hi ADC / fast/extra. vs. lo ADC / slow / intracellular



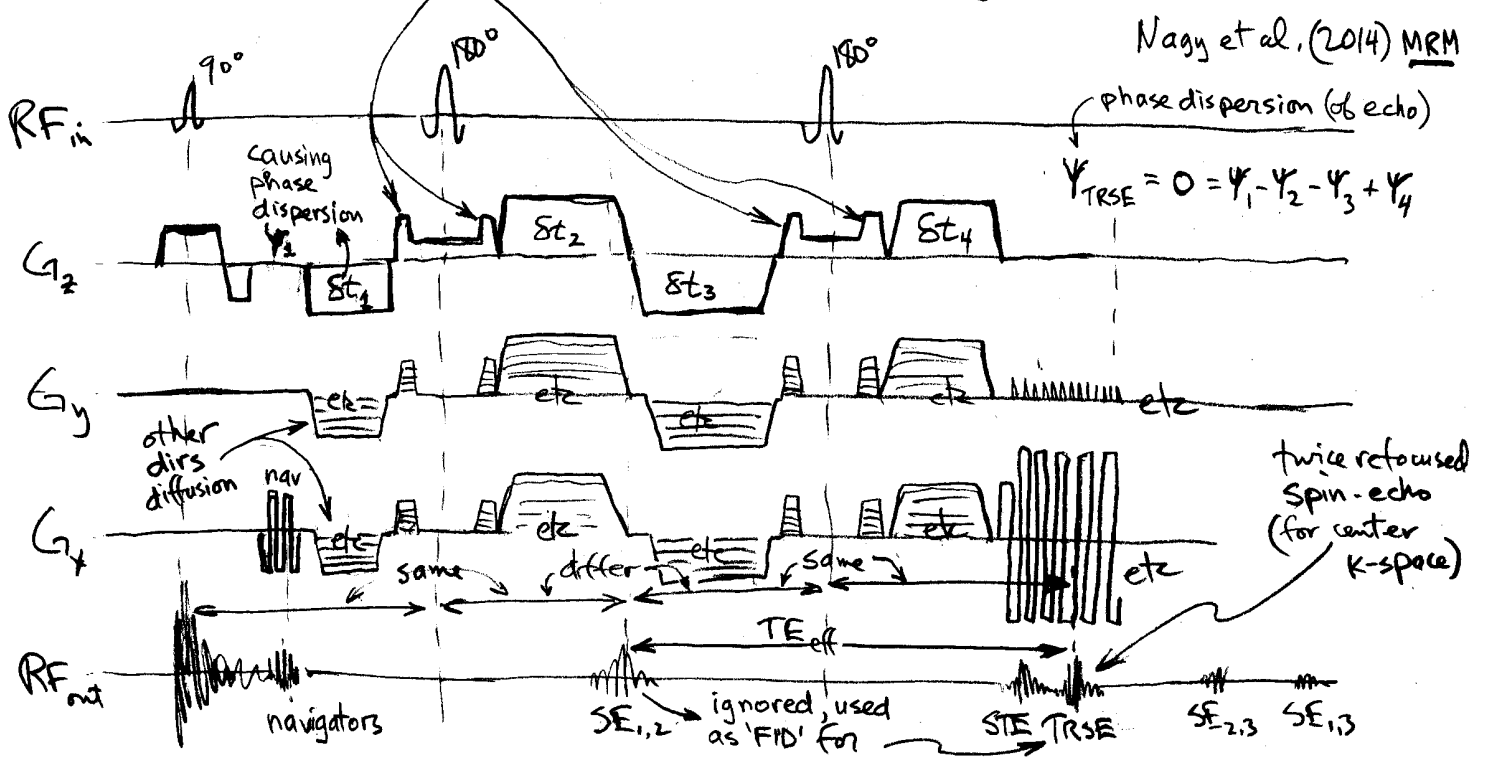
diffusion-2
PRACTICAL DIFFUSION-WEIGHTED PULSE SEQ

- spin-echo 'Stejskal-Tanner' EPI seq. (standard on scanners)
 ↳ allows longer TE



- eddy-currents are long time-constant currents in metal of scanner that distort B field → spatial image distortion

- "doubly-refocused" spin echo sequence (DSE) can cancel the effects of eddy current (w/partic. time constants)
 ↳ (also, keep crushers orthogonal to diffusion-encoding gradients)



PERFUSION - ARTERIAL SPIN LABEL



- basic idea: tag blood below area of interest
 collect control & tagged image
 assume directional input flow!

- tag is 180° pulse
 - sign not problem when delay long enough (see below)

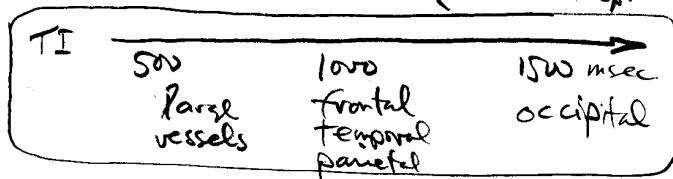
continuous ASL (CASL) - continuously tag a plane →
 pseudo-contin. ASL (PCASL) - ^{see next} gradient on, blood gets adiabatically inverted as it passes through location w/ correct resonant freq.
 pulsed ASL (PASL) - e.g., EPICSTAR, FAIR, PICORE, QUIPSS II
 tag block of tissue below slice(s) →

- small diffs between control and tag (~1%)

↳ requires accurate balancing of control & tag images, control mag. transfer

- contrast problems: transit delays → biggest confounding factor
 relaxation rate diffs
 venous clearance (vs. microspheres, which get stuck!)

↳ transit delays



solutions for quantitative
 - insert delay so all spins arrive into low velocity capillaries
 - kill end of tag to reduce spatial variation of tag

QUIPSS II - quantitative perfusion

TURBO ASL

- use TI longer than TR
- omit QUIPSS tag ending

tag pulse

control img.
control pulse

tag image
tag pulse

control img.

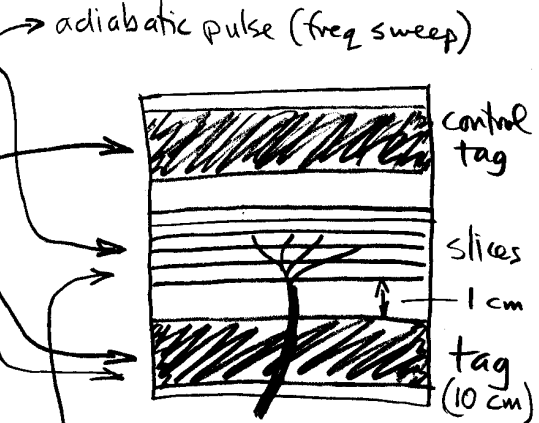
2x faster but limited slice #

1) pre-saturate spins in target slices

2) tag - 180° pulse below slices
 control - 180° pulse above slices (to control off-resonance)

3) saturate tagged block to end tag (TI₁)
 [both tag and control
 can use train of thin slices pulses at top of tag band]

4) EPI or spiral images of target slices (TI₂)
 ↳ image most distal slice last to cancel delays
 ↳ fast between slice so imaging excitations don't get interpreted as flow



$$\Delta M \approx \text{flow} \times [2M_0 T I_1 e^{-T I_2 / T1A}]$$

can extract flow and BOLD adjacent subtractions minimize movement artifact

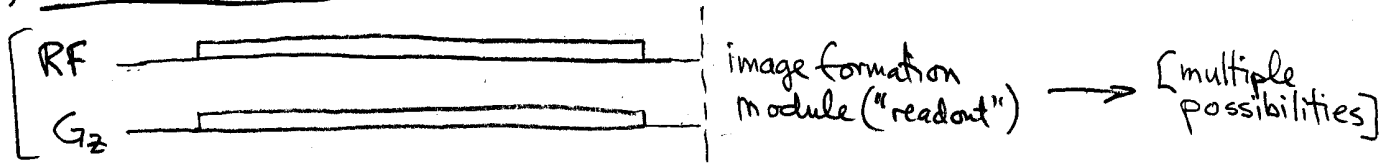
1) alternate tag and control, GRE TE=30ms
 ↳ both BOLD-weighted
 control - tag → flow
 control + tag → BOLD
 tag - control - tag - control ...

2) dual echo spiral
 [k=0 early ⇒ hi S/N flow
 TE=30ms ⇒ BOLD]

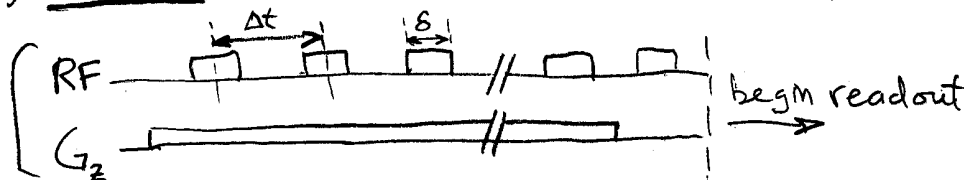
PERFUSION - pCASL

- original CASL (continuous arterial spin labeling) requires RF on continuously to adiabatically invert blood flowing through one plane
 - ↳ can only image one slice (b/c dephasing from gradient)
 - ↳ hard to keep RF on continuously on modern scanner (esp. BC)
 - ↳ can use special purpose RF transmit (separate xmit channel)

A) original CASL



B) pCASL - pseudo (or pulsed!) continuous arterial spin labeling Dai, Alsop (2008)



- problem: multiple pulses create aliased slice planes

$$RF(t) = \frac{1}{\Delta t} \text{comb}\left(\frac{t}{\Delta t}\right) \otimes \text{rect}\left(\frac{t}{\delta}\right)$$

convolution

$$\text{comb}(t) = \sum_n \delta(t-n)$$

↑ spike num

$$\text{rect}(t) = \begin{cases} 1 & \text{if } |t| < \frac{1}{2} \\ 0 & \text{otherwise} \end{cases}$$

[use: convolution of 2 funct equals multiplying their FT's]

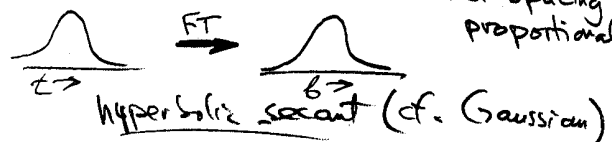
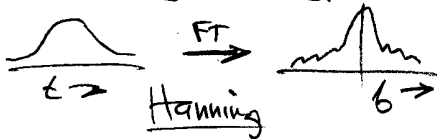
$$F[RF(t)] = \text{comb}(\delta \omega) \cdot \delta \text{sinc}(\pi \delta \omega)$$

multiply

for const G_z: $z = \frac{n}{\gamma G_z \Delta t}$

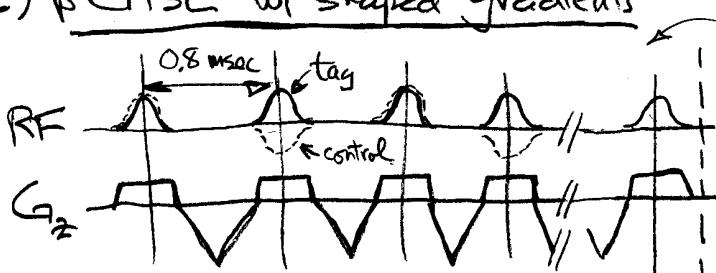
↳ aliased labeling planes at: $\delta = n/\Delta t$ in frequency space, modulated by broad sinc()

- use Hanning or hyperbolic secant to reduce replicas



i.e. spacing inversely proportional to Δt

C) pCASL w/ shaped gradients



(control called a "transparent" pulse)

- readout
- FLASH
 - EPI
 - SMS
 - stack spirals 3D

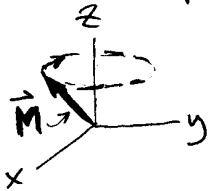
- tag pulses have phase offset respecting gradient
- control identical except every other has $+\pi$ phase
- ↳ no net flip

perfusion-3
OFF RESONANCE EXCITATION

adiabatic RF pulse

- main idea: examine evolution of \vec{M} vector in rotating coord syst set to "off-resonance" \vec{B}_1 field freq (ω_{rf}), not Larmor freq of \vec{M} (ω_0)
- normally, if rotating coord syst freq set to Larmor freq ($\omega_{rf} = \omega_0$), an actually precessing \vec{M} will be stationary (ignoring decay) \rightarrow implies effective $B_z = 0$ in rotating

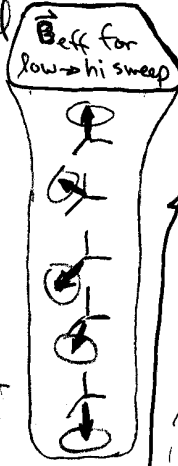
- now, move \vec{M} to rotating coord syst at \vec{B}_1 freq lower than ω_0 (assume $B_1 = 0 = \text{off}$): existing \vec{M} will now appear to precess around z-axis:



N.B.: this is precession in already rotating coordinate system! (slow relative to ω_0)

$$\Delta\omega_0 = \omega_0 - \omega_{rf}$$

freq of precession in rotating coordinate syst Larmor freq of \vec{M} rotation freq \vec{B}_1 (= "incorrectly set rotating coord syst frequency")



- thus, viewing \vec{M} vector in off-resonance rotating coord syst makes it look like additional \vec{B}_z field is causing "extra" precession

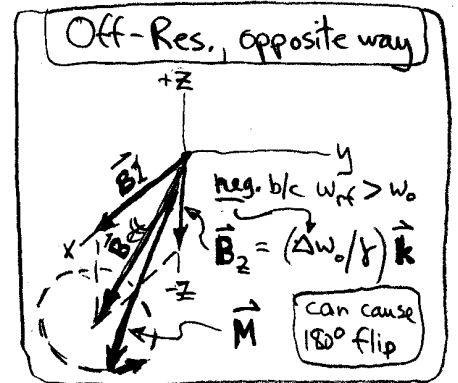
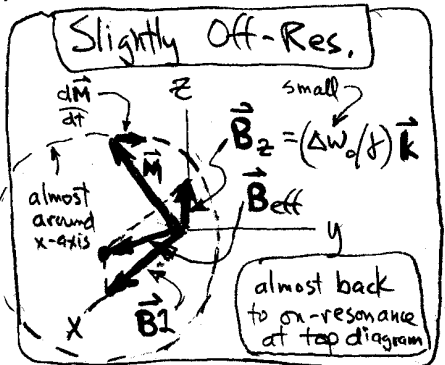
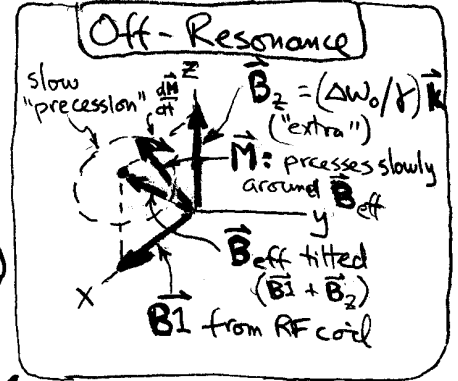
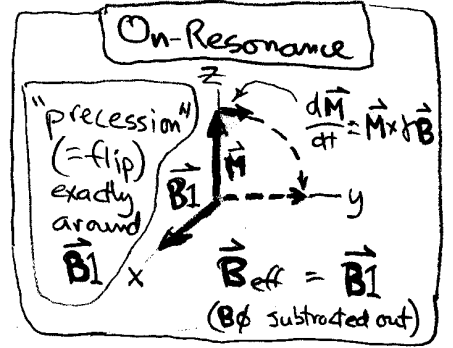
- "extra" \vec{B}_z component is proportional to $\Delta\omega_0$ offset
 \hookrightarrow can be pos or neg: rot coord syst freq: \nearrow too low \rightarrow pos \vec{B}_z \searrow too high \rightarrow neg \vec{B}_z

- extra \vec{B}_z adds to \vec{B}_1 resulting in slow precession around tipped axis: \vec{B}_{eff} (effective)

- extra \vec{B}_z from any gradient \rightarrow same effect on $\Delta\omega_0$ (changes ω_0 instead of changing ω_{rf})

$$\vec{B}_{eff} = \left(\frac{\Delta\omega_0}{\gamma}\right)\vec{k} + B_{G_z}\vec{k} + B_1\vec{i} \leftarrow x\text{-axis}$$

effective \vec{B} in rotating frame set to \vec{B}_1 freq apparent "extra" \vec{B}_z from Larmor- B_1 freq mismatch (pos or neg) (if on-res. $\rightarrow 0$) extra \vec{B}_z from optional gradient (pos or neg) (additional source of \vec{B}_{eff} tilt) transverse RF stim (here, around x-axis)

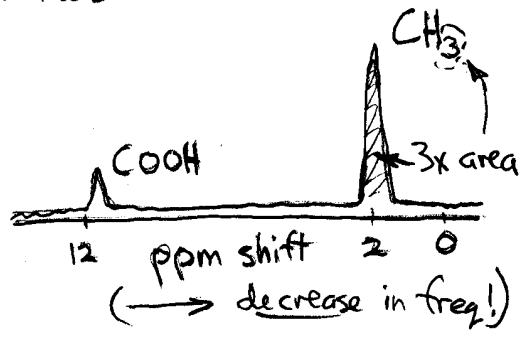
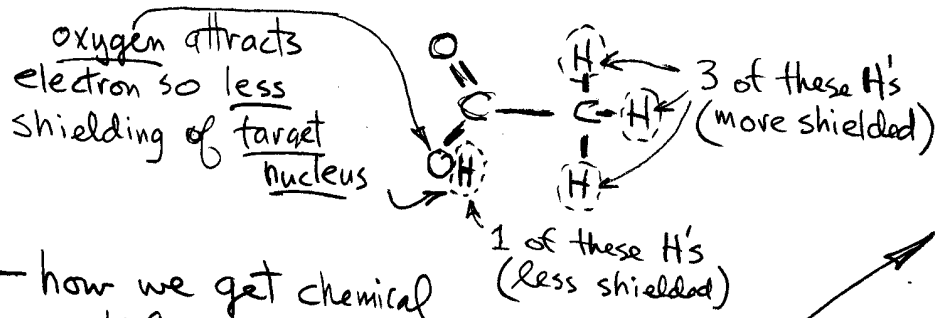


| | | |
|--|-----------|---|
| adiabatic RF pulse | \approx | flow-driven CASL tag |
| RF: sweep freq. | | RF: const freq |
| ω_0 : ~constant (for given slice) | | ω_0 : sweeps because spins flow along gradient direction |

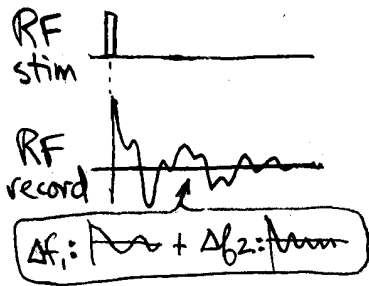
spect-1

SPECTROSCOPY + IMAGE

- chemical shift: small displacement resonant freqs due to variable shielding of target nucleus (e.g. ^1H) by surrounding electron orbitals
- e.g., acetic acid:



- how we get chemical shift spectrum:

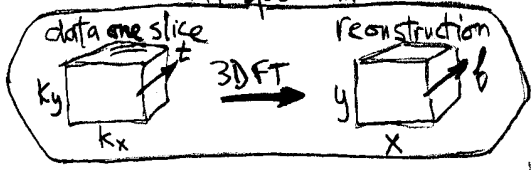


Larmor oscillations are multiplied (PSD) by center freq to obtain Δf (not MHz high freq)

- N.B.: opposite "direction" of FTs!

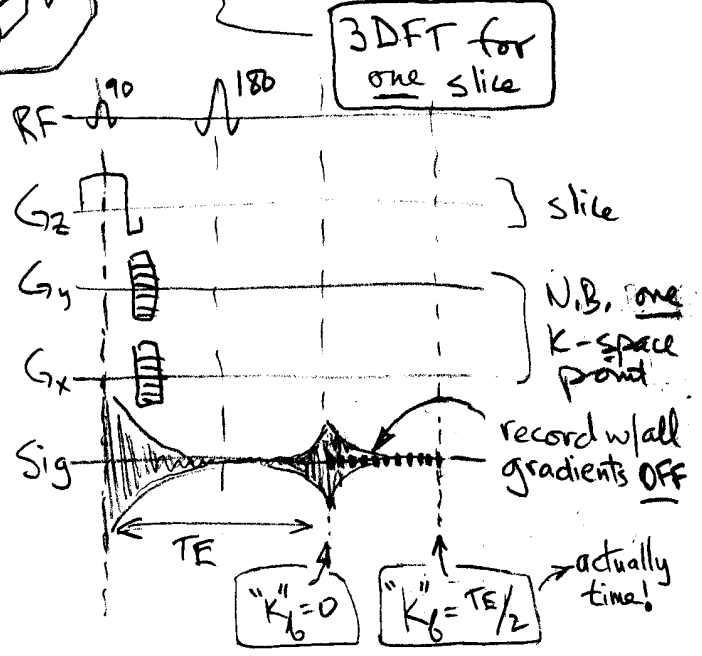
| | signal | result |
|------------|---|---|
| NMR | time domain oscillation samples (shift) | FT → shift freq. spectrum |
| MRI | spatial freq. samples | FT → spatial object (like time domain signal) |

- data before FT is a series of time-domain samples of the mix of shifted-freq offsets
- FT turns data into "shift spectrum"



Pulse Sequence

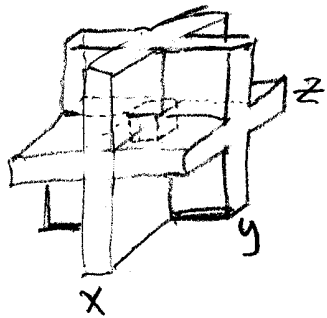
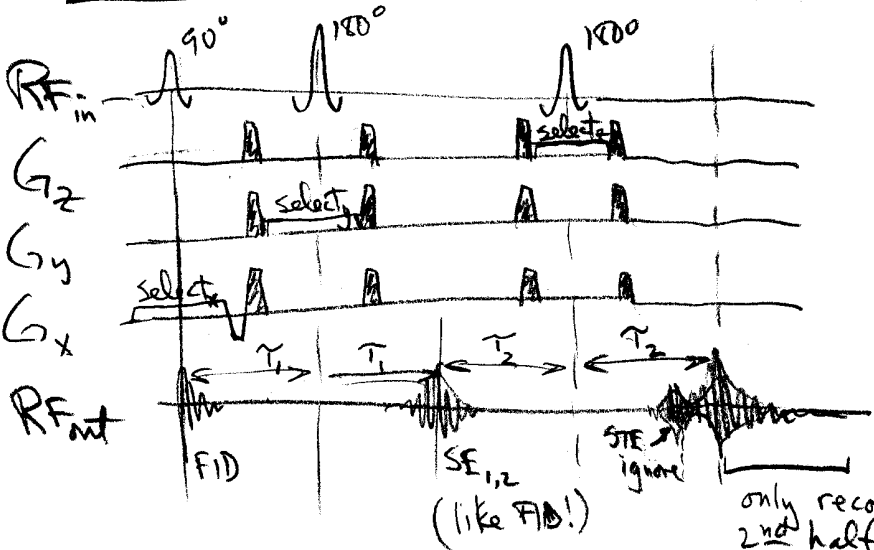
- since we are already using phase (=freq) encoding for space, we need an "extra dimension" w/ all gradients OFF!
 - use spin-echo to undo built-up chemical shifts, then record chemical-NMR-like signal
- ↳ and FT-it like chemists do!



Speet-2
PRESS, MEGA-PRESS

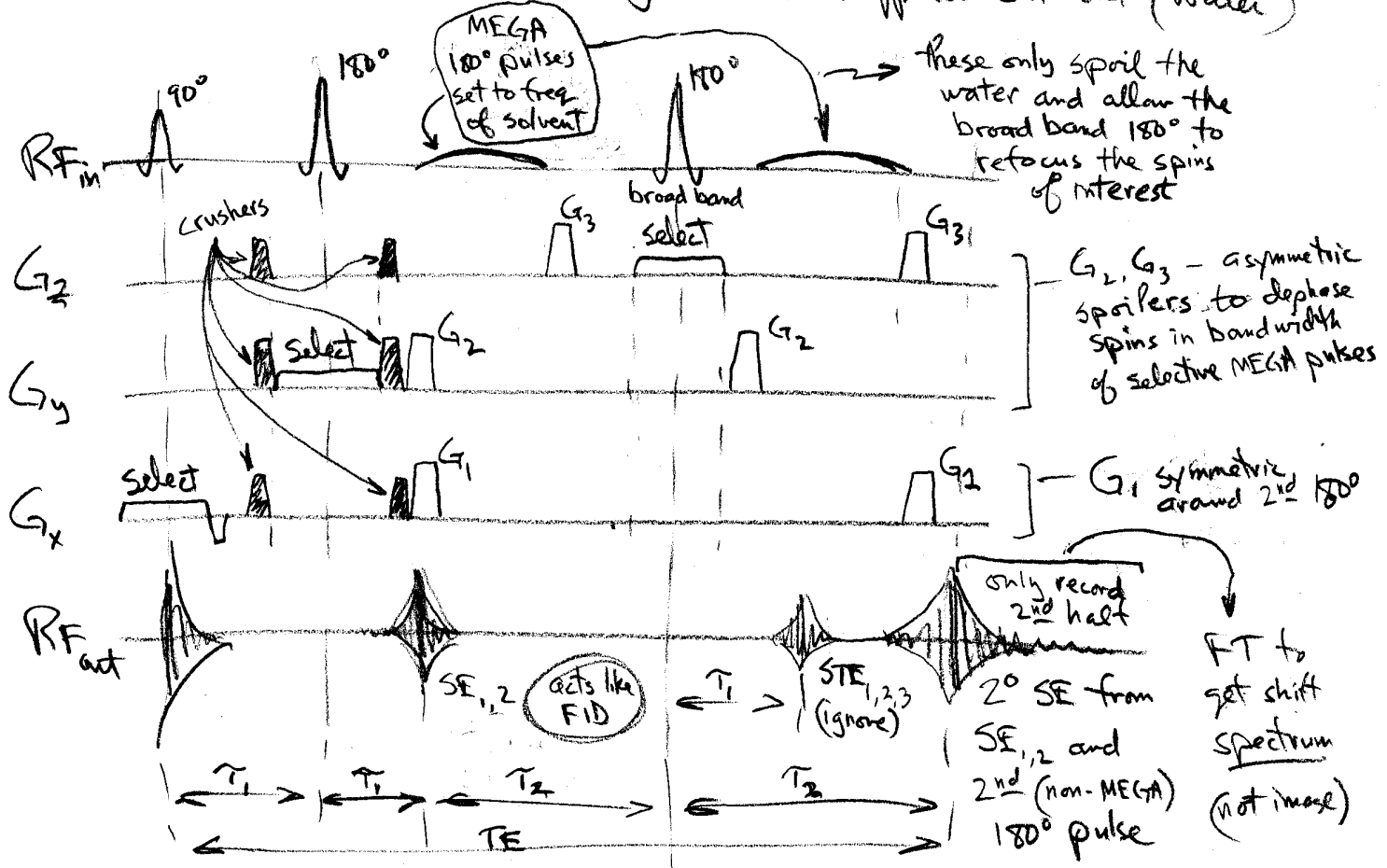
- usu. single voxel by using 3 orthog. slice selects
 (tho can add PE gradients & more excitations to get multiple vox)

PRESS — 3 orthog slice select

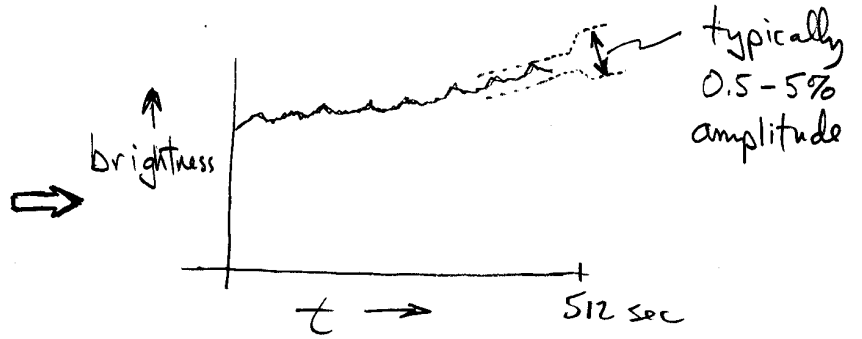
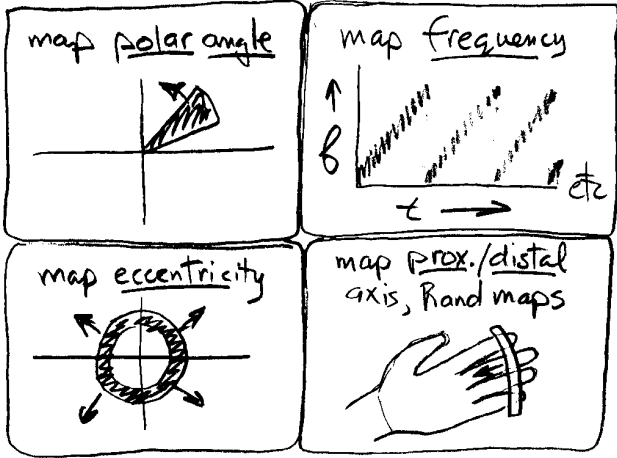


It's OK, now to think of multiple frags here!
 FT to get shift spectrum

MEGA-PRESS — add "editing" RF's to suppress solvent (water)



PHASE-ENCODED STIMULUS & ANALYSIS



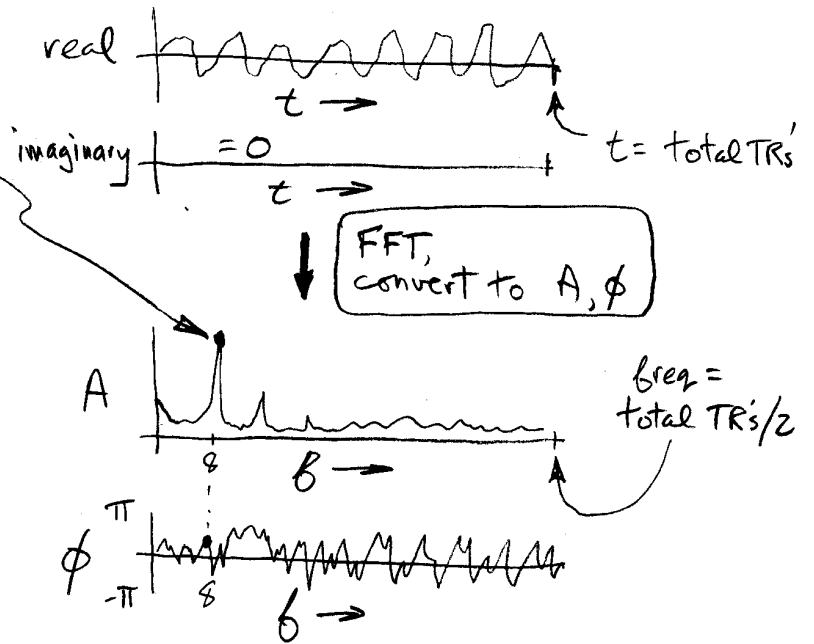
Periodic stimuli (Phase-encoded) - e.g., 8 cycles at 64 sec/cycle

Strongly periodically activated single voxel time course

remove constant (avg) and linear trend

calculate significance

- ratio between amplitude at stimulus frequency (=signal) and average of amplitudes at other frequencies (=noise)
- ignore harmonics, low freq (=movement)



smooth

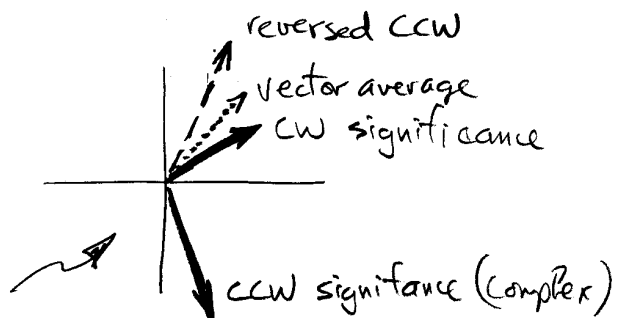
- vector average of complex significance (A, ϕ) with that at nearest neighbor surface points

display

- plot phase using hue and saturation to indicate significance

delay correction

- record responses to opposite directions of stimulus (ccw/cw, in/out, up/down)
- vector average after reversing angle of one
- penalizes inconsistent more than just avg of angles



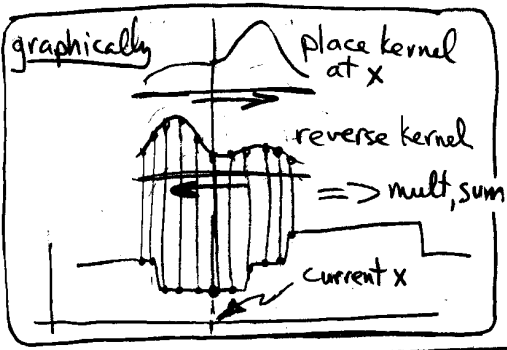
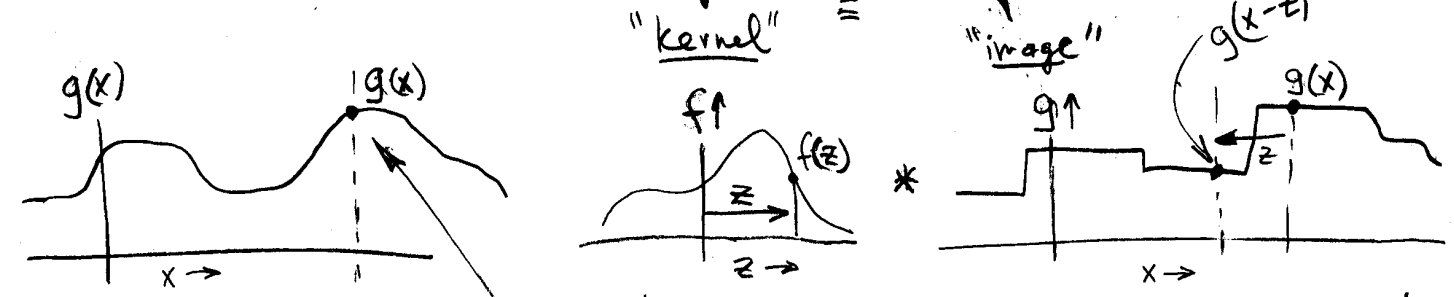
CONVOLUTION

for one x

$$h(x) = f(x) * g(x) = \int_{z=-\infty}^{z=+\infty} f(z) \cdot g(x-z) dz$$

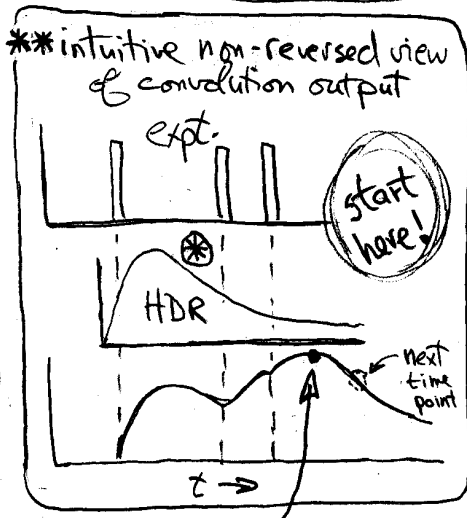
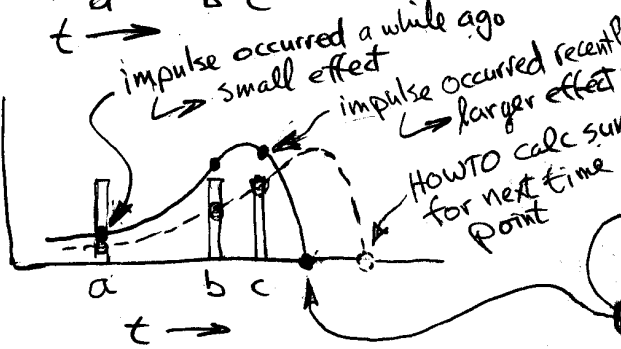
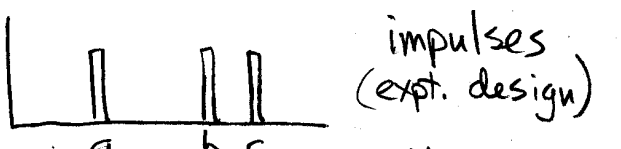
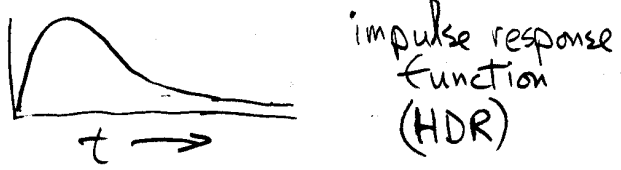
linear time/space invariant system

- definition of convolution $(f * g)(x)$
- commutative



- how to calculate one term
- sum across all z to get the value of the convolution at point x
- move kernel to calculate next x

Why reverse makes sense (b/c commutative, can think like: $h(x) = \int \underbrace{g(z)}_{\text{image}} \cdot \underbrace{f(x-z)}_{\text{kernel}} dz$)



N.B. cross-corr same as convolution except no reversal of $g(x-z)$ instead of $g(x+z)$

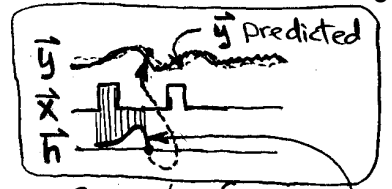
N.B. auto-corr same, except no-reversal and use same funct for both f, g

how to calculate convolution output for this time point (only 3 terms in sum, all other zero)

stats-3

GENERAL LINEAR MODEL

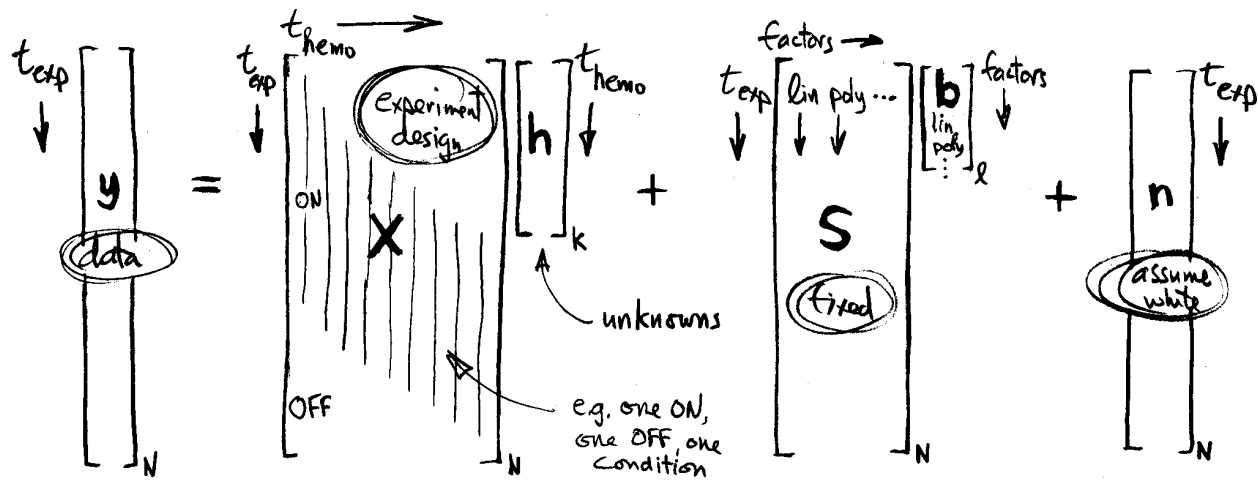
"block design"
 ↳ better to detect resp.
 "event-related design"
 ↳ better to measure HDR shape



- goal: solve for the hemodynamic response functions, \vec{h}

$$\vec{y} = \mathbf{X}\vec{h} + \mathbf{S}\vec{b} + \vec{n}$$

data = design · HDR + drifts · weights + noise



can concat X, S

$$\vec{y} = \begin{bmatrix} \mathbf{X} & \mathbf{S} \end{bmatrix} \begin{bmatrix} \vec{h} \\ \vec{b} \end{bmatrix} + \vec{n}$$

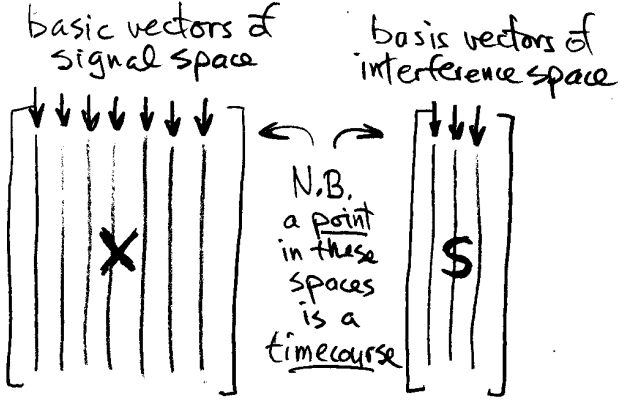
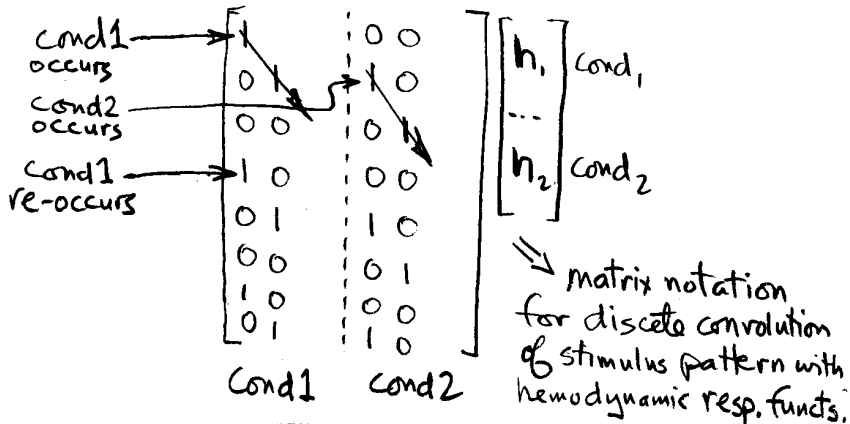
simpler: preconvolve

- conv. \vec{X} w/ fixed \vec{h}
- solve for $\vec{\beta}$

$$\vec{y} = \vec{X}\vec{\beta} + \vec{n}$$

scalar y/x

multiple conditions



maximum likelihood estimate (Liu et al. 2001 Neuroimage)

orthogonal cols most efficient minimize trace $[(\mathbf{X}_\perp^T \mathbf{X}_\perp)^{-1}]$ to get

1) assume white noise, solve for \vec{h}

$$\hat{\vec{h}} = (\mathbf{X}^T \mathbf{P}_S^+ \mathbf{X})^{-1} \mathbf{X}^T \mathbf{P}_S^+ \vec{y} \quad \text{where } \mathbf{P}_S^+ = \mathbf{I} - \mathbf{S}(\mathbf{S}^T \mathbf{S})^{-1} \mathbf{S}^T$$

or

$$= (\mathbf{X}_\perp^T \mathbf{X}_\perp)^{-1} \mathbf{X}_\perp^T \vec{y} \quad \text{where } \mathbf{X}_\perp = \mathbf{P}_S^+ \mathbf{X}$$

↳ projection matrix that removes part of vector that lies in \mathbf{S} space

3) significance (how to construct F-ratio) ↳ design matrix w/ nuisance effects removed from cols

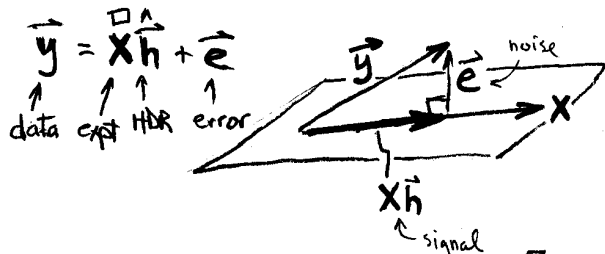
$$F = \frac{N - k - l}{k} \left[\frac{\vec{y}^T (\mathbf{P}_{XS} - \mathbf{P}_S) \vec{y}}{\vec{y}^T (\mathbf{I} - \mathbf{P}_{XS}) \vec{y}} \right]$$

\mathbf{P}_{XS} - projects data on expt + nuisance subspace
 \mathbf{P}_S - projects data onto nuisance subspace
 ↳ see diagram next page for geometric interp

stats-4

GEOMETRIC INTERPRETATION OF GENERAL LINEAR MODEL

- with no nuisance functions (S), we could look at orthogonal projection of data onto experimental design and compare that to error to determine significance



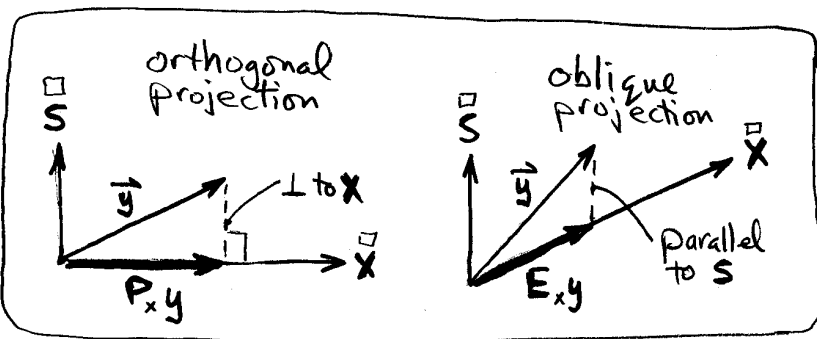
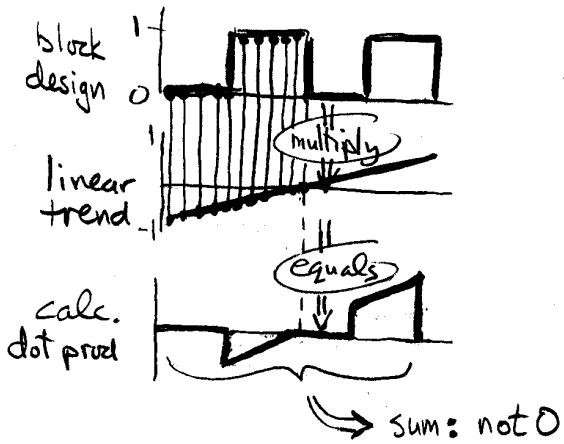
$\vec{X}\vec{h} = \mathbf{P}_x \vec{y}$

Projection matrix, \mathbf{P}_x , operates on \vec{y} to give projection of data into experiment space, X

- when nuisance functions, S , are considered, problem: S may not be orthogonal to X

↳ for example: linear trend not orthogonal to std. block design

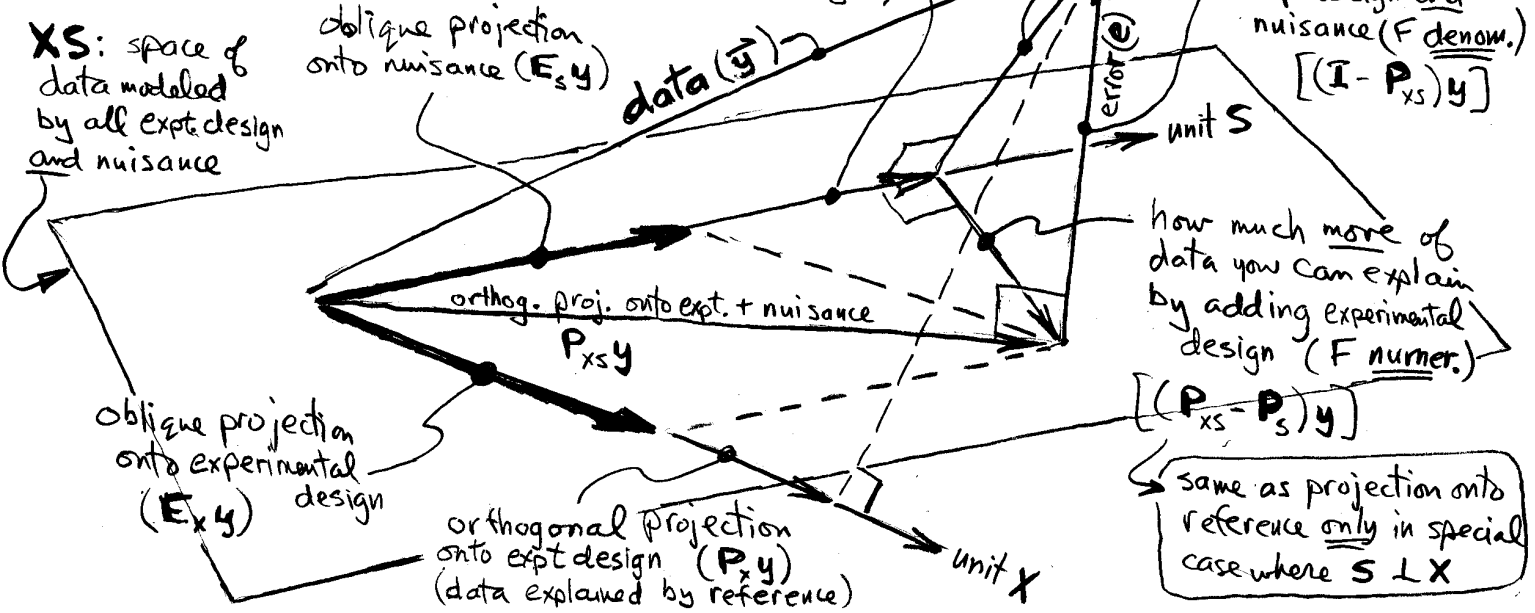
[remember: "orthogonal" means [dot prod. = 0
corr = 0]



Geometric Picture

(Liu et al., 2001, Neuroimage)

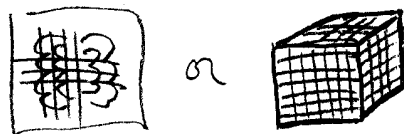
(orig from Scharf & Friedlander, 1994 IEEE)



Surf. 0 WHY USE SURFACES?




- raw MRI data is a 2D flat slice or a 3D volume

↳ $I(x,y)$ or $I(x,y,z)$



but...

1) the neocortex (and cerebellar cortex) are thin, folded 2D sheets

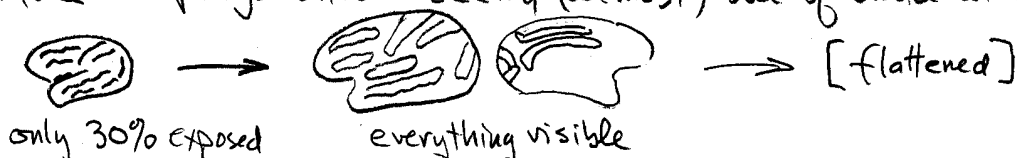
[cortex starts as smooth "balloon" → 
 major sulci, temporal lobe form → 
 great size increase, "crinkles" form → 

2) neocortex contains many topological maps along its surface

[retinotopy
 tonotopy
 somatotopy
 musculotopy

plus higher level maps → $\sim 2/3$ of its area

3) surface displays allow seeing (almost) all of data at once



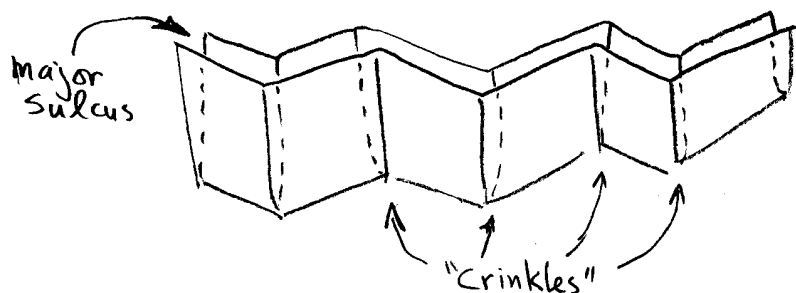
4) differences in major sulci make 3D-based alignment difficult



e.g. STS, monkey-like IPS vs. postcentral plus extra

↳ extremely anisotropic def.

5) idiosyncratic sulcal crinkles



- these introduce additional noise into alignment in 3D
 - exact position of crinkles unlikely to have functional implications (tho 3D align might respect them)

SEGMENTATION & SURFACE RECON Talairach, Normalize, StripSkull

1) MNI auto-Talairach → generates 4x4 matrix

$$\begin{bmatrix} 3 \times 3 \\ \text{(rotate} \\ \text{\&scale)} \\ 0 \ 0 \ 0 \ 1 \end{bmatrix} \begin{matrix} x \\ y \\ z \end{matrix} \rightarrow \text{translate}$$

- make average brain target (blurry)
- blur target (further), blur single brain (a bit), gradient descent on x_{corr}
- repeat w/ less blurring of avg target and current brain
- problems: variable neck cut off
 ↳ but much better than standard! (only 2 points near center of brain!
 ↳ fit to bounding box

2) Intensity Normalization (output: "T1")

- histogram of pixel values in 10 mm thick HOR slices



- smooth histogram

- peak find to get initial estimate of white matter



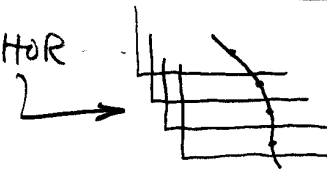
- discard outlier peaks across slices

- fit splines to peaks across slices



↳ interpolates scaling factor \perp to HOR

- scale each pixel so WM peak is 110



- refine estimate to interpolate in 3D

find points in $5 \times 5 \times 5$ within 10% of WM, get new scale for them
 build Voronoi to interpolate scales unset above
 soap-bubble-smooth Voronoi boundaries (3 iterations)
 re-scale each voxel

5-10 times

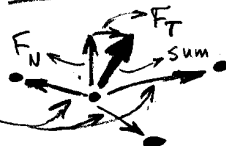
3) Skull Stripping (output: "brain")

- "shrink-wrap" algorithm

- start with ellipsoidal template → subtesselated icosahedron

- minimize brain penetration and curvature

- curvature: spring force
 (from center-to-neighbor vect sum)



- brain penetration

apply force along surface normal that prevents surface from entering gray matter

12 vertices → even distribution of points on a sphere
 20 tri faces



"top"

"side"

- to go finer, subdivide each triangle & promote new vertices to sphere



- decompose into \perp and tangential (local normal from summed, normed cross products)

SEGMENTATION & SURFACE RECON

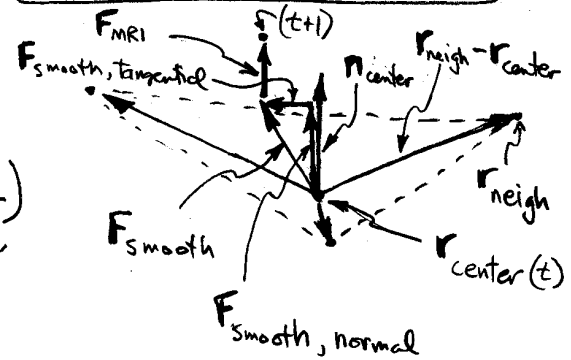
Spring force in detail

- implementing a "force" is like directly constructing the operator that minimizes something (without first defining the "something")
- more formally, we would define cost function, then take its derivative (gradient) to minimize it

Shrinkwrap update eq. (skull strip, original Dale & Sereno surface refinement)

$$\underbrace{\mathbf{r}_{center}(t+1)}_{\text{for one vertex}} = \underbrace{\mathbf{r}_{center}(t)}_{\text{previous}} + \underbrace{\mathbf{F}_{Smooth}(t) + \mathbf{F}_{MRI}(t)}_{\text{local quantities}}$$

rule for each vertex, \vec{r}_{center}



HOWTO

$$\mathbf{n}^T \mathbf{n} = x^2 + y^2 + z^2$$

$$\mathbf{n} \mathbf{n}^T = \begin{bmatrix} x^2 & xy & xz \\ yx & y^2 & yz \\ zx & zy & z^2 \end{bmatrix}$$

$(\mathbf{n} \mathbf{n}^T) \mathbf{v} = \mathbf{n}(\mathbf{n}^T \mathbf{v}) =$ dot prod.

$d\mathbf{n} =$ "project \mathbf{v} onto \mathbf{n} " ($\|\mathbf{n}\|=1$)

λ_{tang} $\sum_{\text{neigh}} (\mathbf{I} - \mathbf{n}_{center} \mathbf{n}_{center}^T) \cdot (\mathbf{r}_{neigh} - \mathbf{r}_{center})$

identity 3x3

stronger than normal (0.5)

expand by distribution to: neighbor vector minus projection of neighbor onto normal \rightarrow tangential!

vector to neighbor vertex

project second onto first

$$+ \lambda_{\text{normal}} \left[\sum_{\text{neigh}} (\mathbf{n}_{center} \mathbf{n}_{center}^T) \cdot (\mathbf{r}_{neigh} - \mathbf{r}_{center}) - \frac{1}{\# \text{vertices}} \sum_{\mathbf{v}} \sum_{\text{neigh}} (\mathbf{n}_{\mathbf{v}} \mathbf{n}_{\mathbf{v}}^T) \cdot (\mathbf{r}_{neigh} - \mathbf{r}_{\mathbf{v}}) \right]$$

weaker than tangential (0.1)

projection of a neighbor vertex vector onto normal in the direction of the normal (\mathbf{n} is squared (as above) so we get a vector out (not a scalar))

average normal component

vector, subtract off

$$\mathbf{F}_{MRI} = \lambda_{MRI} \mathbf{n}_{center} \prod_d \text{Max} \left[0, \tanh \left[I(\mathbf{r}_{center} - d \mathbf{n}_{center}) - I_{\text{thresh}} \right] \right]$$

strong (1.0)

multiply all terms \rightarrow $F_{MRI} = 0$ if any are zero

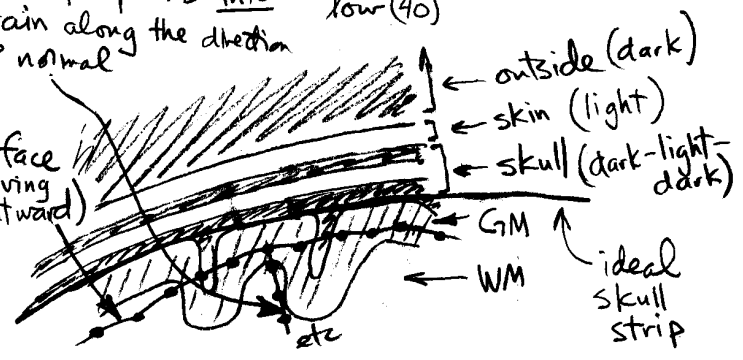
max force saturates at 1.0 (max "prod" product = 1.0)

intensity MRI data

d sample points into brain along the direction of normal

low (40)

Snapshot of surface and "core sample" from one vertex



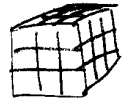
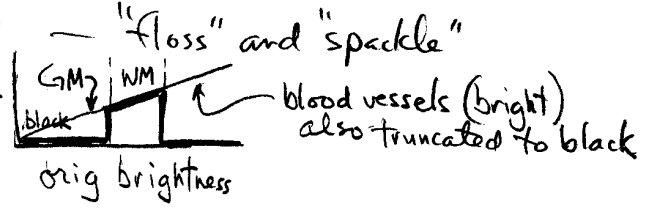
surf-3

SEGMENTATION & SURFACE RECON

filter, cut, tessellate

4) Non-isotropic filtering (output: "wm")

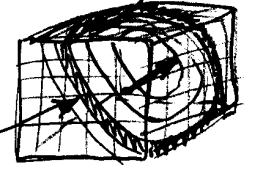
- preliminary hard threshold: output
- find ambiguous/boundary voxels
 ↳ 20% or more of 26 immediate neighbors different
- find plane of least variance



↳ to avoid expensive calc below...

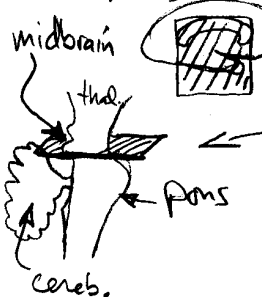
for each ambiguous voxel

for each direction (from icosahedral supertessellation) consider 5x5x5 volume around 1 voxel
 find plane of least variance in this hemisphere (1 voxel thick)
 median filter w/ hysteresis



- ↳ if 60% of within-slab differ, reverse classification
- ↳ "flosses" sulci without blurring

5) Find cutting planes



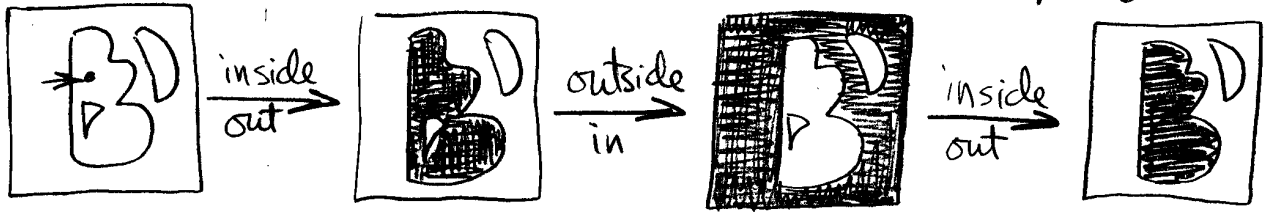
callosum, to separate hemispheres (SAG)
 midbrain, to avoid fill into cerebellum (HOR)

↳ Talairach to start; fill WM in SAG or HOR till min area

6) Region-growing to define connected parts (output: "filled")

- inside-out, outside-in, inside-out — for each hemisphere

- up/down cycles within each plane
- plane-by-plane



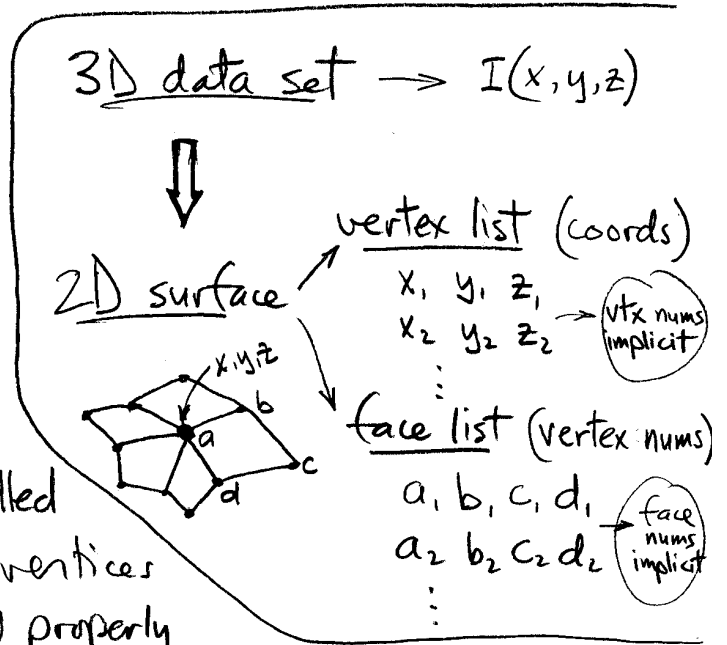
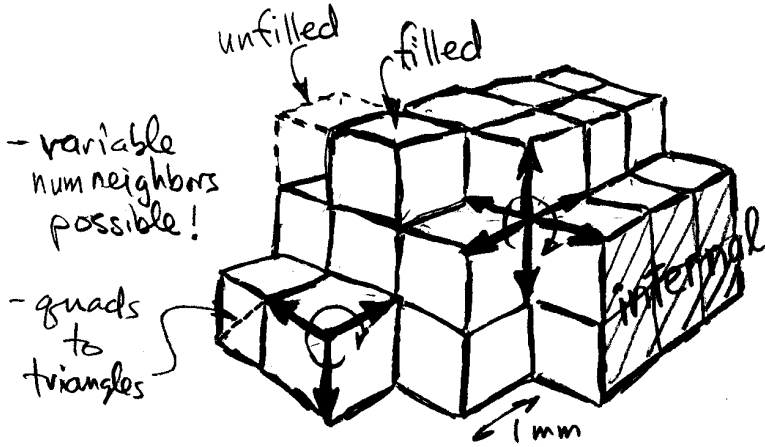
- "wormhole filter." (3x3x3 = center + 26)

↳ fill (unfilled) voxel if 66% neighbors differ → eliminates structures w/ thin, 1-D structure

surf-4

SEGMENTATION & SURFACE RECON 3D → 2D

1) Surface Tessellation (output: rh.orig, lh.orig)



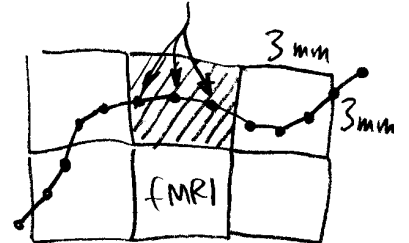
- find filled voxels bordering unfilled
- make ordered list of neighboring vertices
↳ so cross-products oriented properly
- long list of values associated with each numbered vertex

e.g.
 position (orig, morphed)
 area (orig, morphed)
 curvature (intrinsic, Gaussian)
 "sulcus-ness" (summed \perp movement during unfolding)
 cortical thickness
 fMRI data ←
 EEG/MEG dipole strength

- separate fMRI data set must be aligned, sampled

fMRI voxels larger
 sample at each surface vertex
 nearest-neighbor "soap bubble" smoothing
 to interpolate data onto hi-res mesh

fMRI → surface
initial sample
same value here



- some quantities only well-defined on surface

↳ gradient of magnitude of cortical map measure (e.g., eccentricity)

⇓
interpolate on surface

SEGMENTATION & SURFACE RECON smooth, inflate, final surfaces

- smoothing/inflation/wm, pia done as derivative of energy functional

$$J = \underbrace{J_{\text{tangential}}}_{\text{total scalar error to minimize}} + \underbrace{\lambda_{\text{normal}} J_{\text{normal}}}_{\substack{\text{small (0.25)} \\ \text{scalar curvature error (fixed by reducing curvature)}}} + \underbrace{\lambda_{\text{image}} J_{\text{image}}}_{\substack{\text{smaller (0.075)} \\ \text{scalar image error (fixed by moving toward target image value)}}$$

$$J_{\text{normal}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \sum_{\text{neighbors}} \left[\underbrace{\mathbf{n}_{\text{center}}}_{\substack{\text{vertex unit normal} \\ \text{project onto normal}}} \cdot \underbrace{(\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}})}_{\substack{\text{vector from current center to one neighbor (position vector diff.)}}}\right]^2$$

across all vertices, curvature error

1/2 so no coefficient on derivative

across all vertices

neighbors of one vertex

$$J_{\text{tangential}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \sum_{\text{neighbors}} \left[\underbrace{\mathbf{t}_{\text{center}}^x}_{\substack{\text{x-direction in tangent plane} \\ \text{project vector to neighbor onto x \& y}}} \cdot (\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}}) \right]^2 + \left[\underbrace{\mathbf{t}_{\text{center}}^y}_{\substack{\text{y-direction in tangent plane}}} \cdot (\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}}) \right]^2$$

"squishing" of mesh

$\mathbf{t}^x, \mathbf{t}^y$ are first 2 eigenvect. of neighbor vector cloud (\mathbf{n} is third)

$$J_{\text{image}} = \frac{1}{2 \# \text{vert}} \sum_{\text{centers}} \left[\underbrace{I_{\text{center}}^{\text{targ}}}_{\substack{\text{target brightness}}} - \underbrace{I(\mathbf{r}_{\text{center}})}_{\substack{\text{brightness at current location}}} \right]^2$$

image error

I^{targ} for WM: mean of voxels labeled WM in 5mm neighborhood

I^{targ} for pia: global - small num for C.S.F.-like

- take directional derivative of energy functional (to find steepest uphill)
- move each vertex in the opposite (negative) direction w/ self-intersect test

$$-\frac{\partial J}{\partial \mathbf{r}_{\text{center}}} = \underbrace{\lambda_{\text{image}}}_{\substack{\sum_{\text{centers}} \text{ gone b/c const} \\ \text{scalar}}} \left[I_{\text{center}}^{\text{targ}} - I(\mathbf{r}_{\text{center}}) \right] \underbrace{(-\nabla I(\mathbf{r}_{\text{center}}))}_{\substack{\text{vector - calculate gradient on image (first blur w/ Gaussian)}}} + \sum_{\text{neighbors}} \lambda_{\text{normal}} \left[\underbrace{\mathbf{n}_{\text{center}} \cdot (\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}})}_{\substack{\text{x-component of tangential}}} \right] \underbrace{(-\mathbf{n}_{\text{center}})}_{\substack{\text{scaled by} \\ \text{unit normal vector}}} + \sum_{\text{neighbors}} \left[\underbrace{\mathbf{t}_{\text{center}}^x \cdot (\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}})}_{\substack{\text{x-component of tangential}}} \right] \underbrace{(-\mathbf{t}_{\text{center}}^x)}_{\substack{\text{scaled by} \\ \text{unit normal vector}}} + \left[\underbrace{\mathbf{t}_{\text{center}}^y \cdot (\mathbf{r}_{\text{neigh}} - \mathbf{r}_{\text{center}})}_{\substack{\text{y-component of tangential}}} \right] \underbrace{(-\mathbf{t}_{\text{center}}^y)}_{\substack{\text{scaled by} \\ \text{unit normal vector}}}$$

go the opposite direction (vector) of largest scalar error for one vertex movement

N.B.: eq. 9 in Dela, Fischl & Sereno different - and incorrect!

HOWTO derivative: constants var $\frac{\partial J}{\partial r} = \partial(C_1 \cdot (C_2 - V)) = \partial(C_1 C_2 - C_1 V) = -C_1$

surf-6

SULCUS-BASED CROSS-SUB. ALIGN

- use summed perpendic. vertex move during inflation as vtx measure of "sulcus-ness"
- add term to error function, J : "sulcus-ness" error

$$J_{sulk} = \frac{1}{2 \#vert} \sum_{centers} [S_{cent}^{sub1} - S_{cent}^{targ} (r_{center})]^2$$

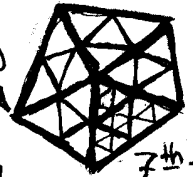
find neg of steepest uphill direction of change in sulcus-ness of target

take deriv. grad descent 2D

$$\frac{\partial J_{sulk}}{\partial r_{center}} = \lambda_{sulk} [S_{cent}^{sub1} - S_{cent}^{targ} (r_{center})] (-\nabla S_{cent}^{targ} (r_{center}))$$

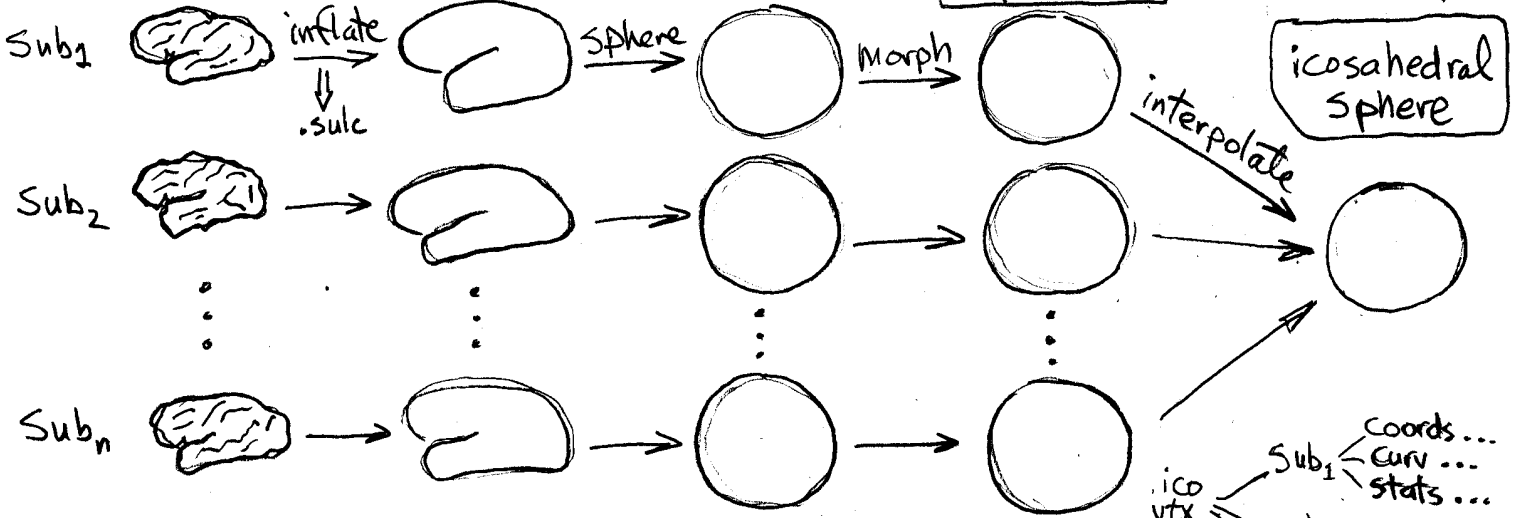
- bootstrap morph to one brain make avg targ re morph to avg targ
- sulcus-ness of moveable subj vtx

icosahedron (5-fold symmetry)



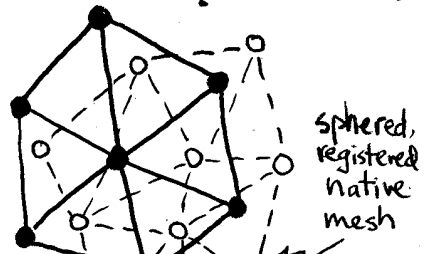
7th triangular sub-tessellation

Smooth wm inflated sphere registered sphere



- each sub's native surf has diff # vertices

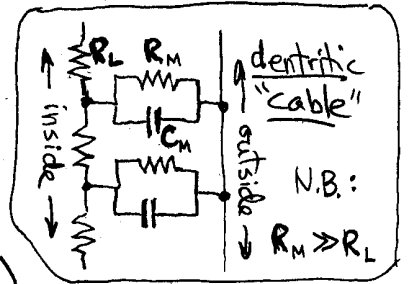
- interpolate values (coords, surface measures, stats) to each icosahedral vertex from neighboring vertices of native mesh (dashed lines)



- average surface made from folded/inflated avg coords
- folded: loses area from sulcal crinkles (fs average "inflated")
- inflated: retains orig area, correct sulc/gyrus ratio ("inflated-avg")

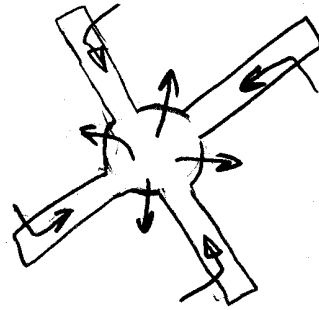
- can use sampled-to-icos individual subj coords to draw icosahedral surface in shape of an indiv. brain
- N.B.: morph will have changed local vertex density compared to more uniform native mesh (use native for sing. sub.)

SOURCE OF EEG/MEG



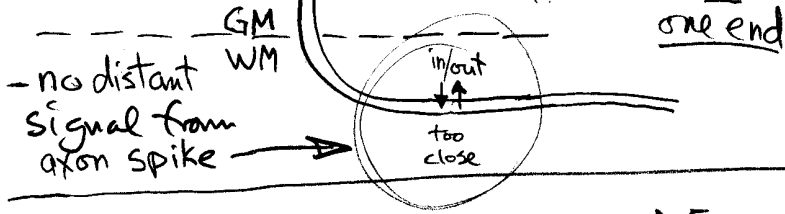
PSPs

anisotropic cables
+
aligned spatially
+
coherent/biased stim
one end



isotropic

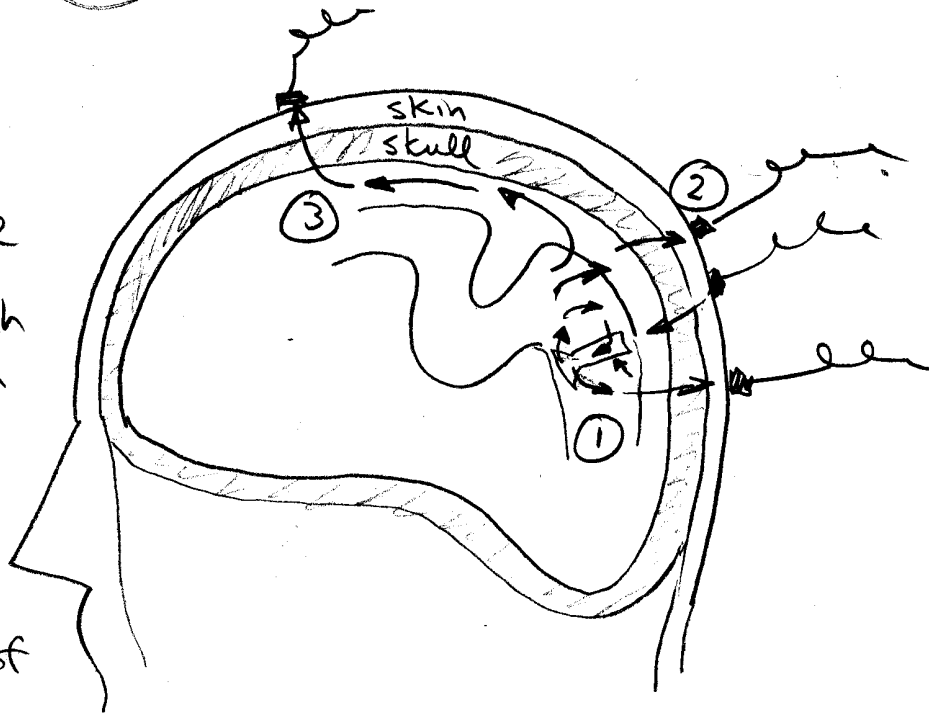
"closed field"
(invisible at distance)



N.B.: spikes only detected by 15µm microelectrode in gray matter!

Head

- 1) - local dipole
- 2) - EEG through skull, skin
- 3) - smearing because skull 1/80 conductivity of brain

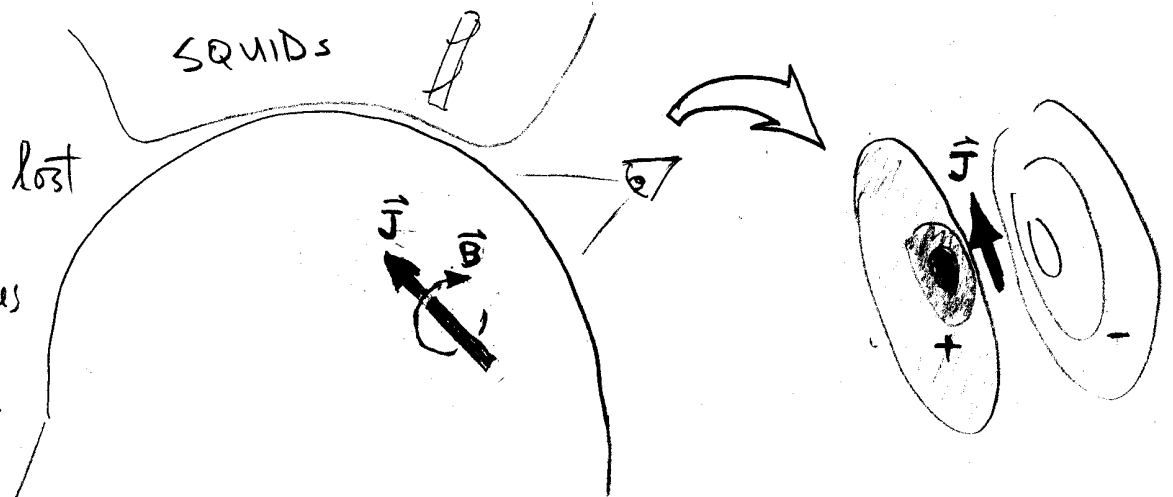


the effect on current flow is like a higher order (larger) "cable"

MEG

SQUIDS

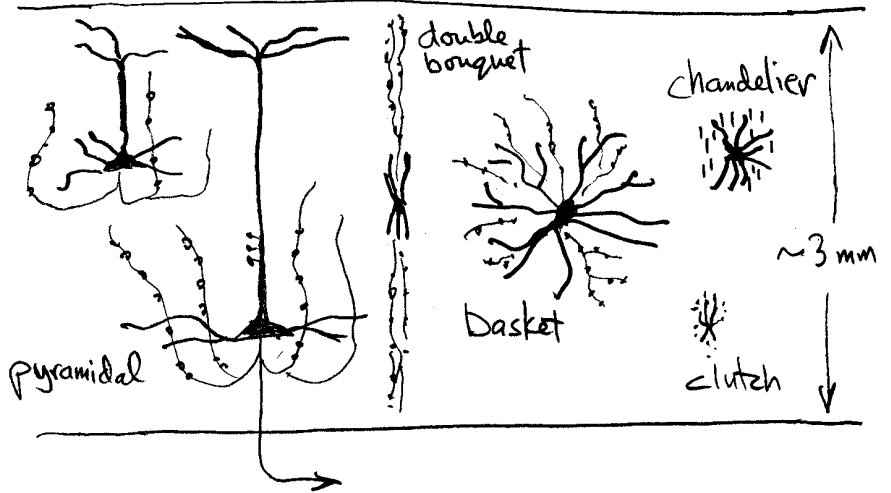
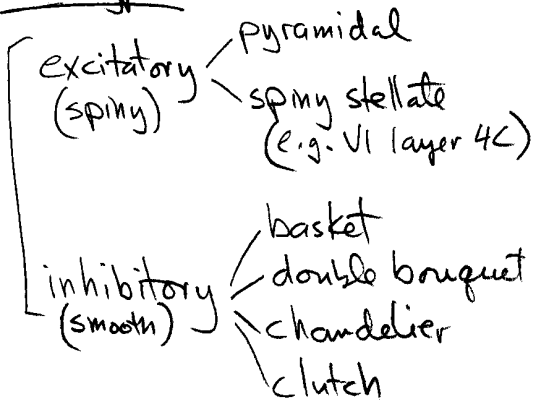
- radial dipoles lost
- tangential dipole generates Gabor-like scalp distrib. of \vec{B} field



Source-2

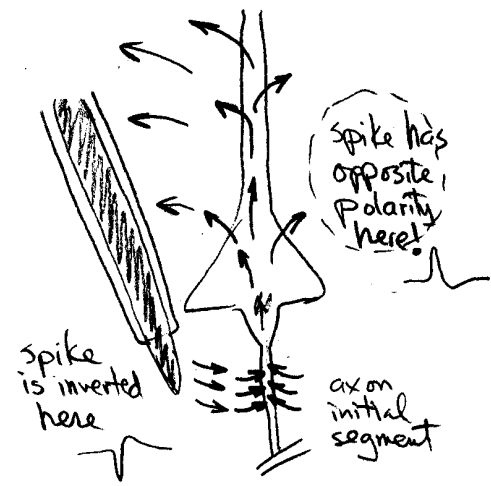
INTRACORTICAL CIRCUITS & ORIGIN OF EEG

Cell types

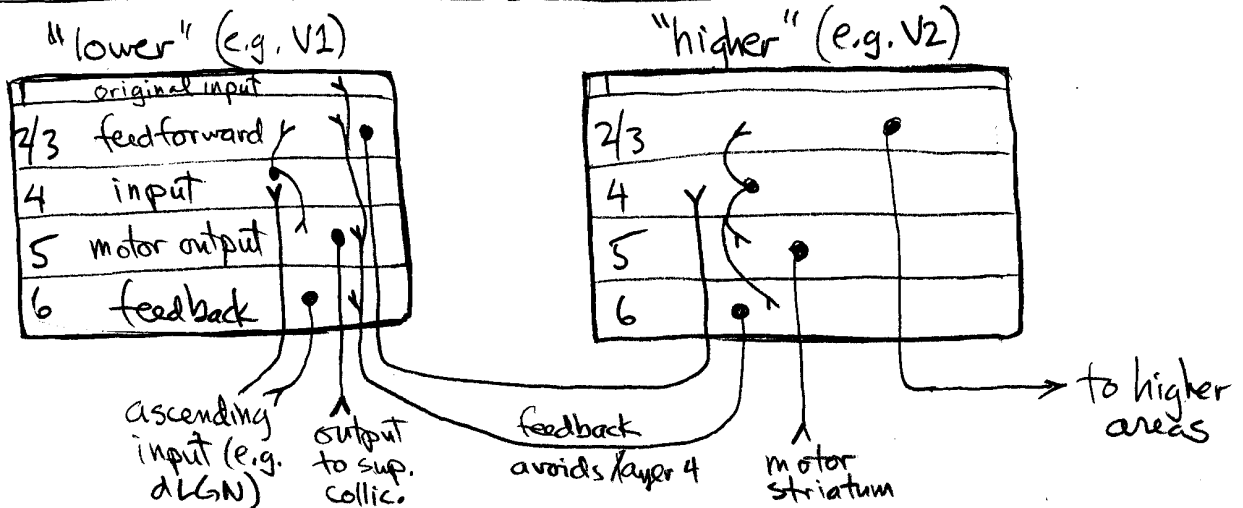


Circuits

- huge complexity
- first principal components: input → layer 4 → layer 2/3 → feedforward
- layer 4 → layer 5/6 → output feedback
- microelectrode recording (e.g. 10 μm tip)
 - high pass → spikes
 - low pass → local field potentials
- spikes only recordable in gray matter
- white matter spikes only recordable with pipette w/ very fine tip b/c inward & outward currents so spatially close in axon/spike (> 1 μm)



intra/inter cortical connections cartoon



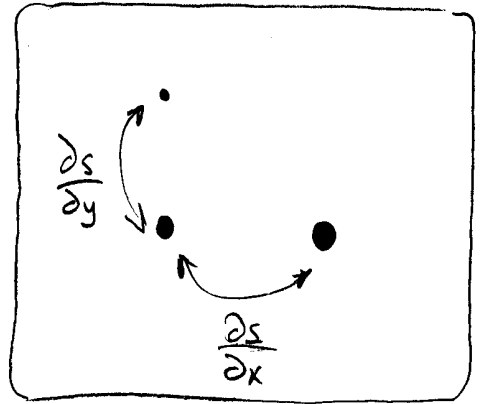
grad div curl

GRADIENT, DIVERGENCE, CURL

gradient (∇) (generalized deriv.)

$$\nabla s(\vec{r}) = \frac{\partial s(\vec{r})}{\partial x} \hat{i} + \frac{\partial s(\vec{r})}{\partial y} \hat{j} + \frac{\partial s(\vec{r})}{\partial z} \hat{k}$$

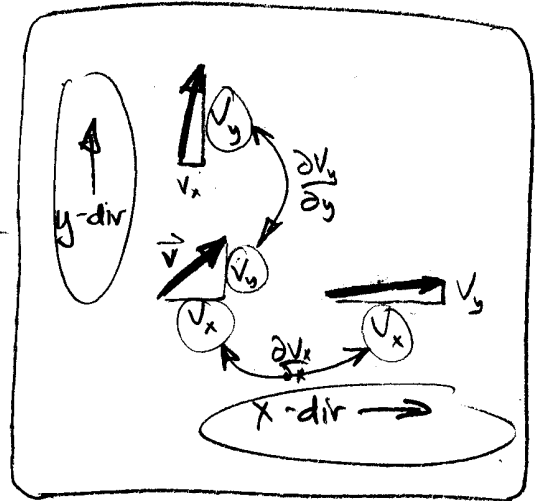
x, y, z
 turns scalar field into vector field
 scalar funct defined at each x, y, z point, \vec{r}
 change of s in x direction at point \vec{r}
 unit vector in x dir



divergence ($\nabla \cdot$) (deriv. "dot prod")

$$\nabla \cdot \vec{v}(\vec{r}) = \frac{\partial v_x(\vec{r})}{\partial x} + \frac{\partial v_y(\vec{r})}{\partial y} + \frac{\partial v_z(\vec{r})}{\partial z}$$

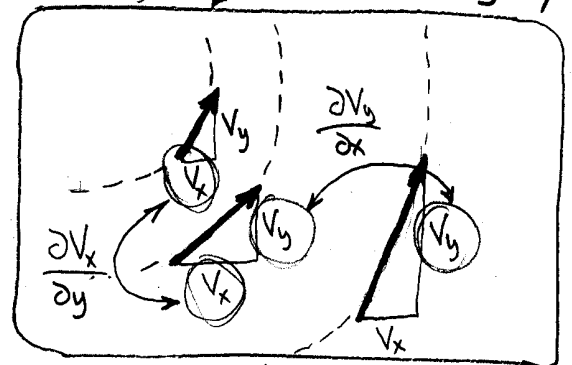
turns vector field into scalar field
 vector funct defined at each x, y, z point, \vec{r}
 change of just x -component of \vec{v} in x -direction at point \vec{r}



curl ($\nabla \times$) (deriv. "cross product")

$$\nabla \times \vec{v}(\vec{r}) = \left(\frac{\partial v_z(\vec{r})}{\partial y} - \frac{\partial v_y(\vec{r})}{\partial z} \right) \hat{i} + \left(\frac{\partial v_x(\vec{r})}{\partial z} - \frac{\partial v_z(\vec{r})}{\partial x} \right) \hat{j} + \left(\frac{\partial v_y(\vec{r})}{\partial x} - \frac{\partial v_x(\vec{r})}{\partial y} \right) \hat{k}$$

turns vector field into another vector field
 vector funct defined at each x, y, z point, \vec{r}
 change of just z component of \vec{v} in y -direction at point \vec{r}



N.B. $\vec{k} \perp$ to this plane

Vector identities

$$\nabla \times \nabla s = 0$$

curl of the gradient of any scalar field is zero

$$\nabla \cdot (\nabla \times \vec{A}) = 0$$

divergence of the curl of any vector field is zero

$$\vec{A} \cdot (\vec{B} \times \vec{C}) = (\vec{A} \times \vec{B}) \cdot \vec{C}$$

CSD-1

POTENTIAL (Φ), ELECTRIC FIELD ($\nabla\Phi$) \neq CSD ($\nabla \cdot (-\nabla\Phi) = \nabla^2\Phi$)

low-frequency field approximation

- electric fields uncoupled from magnetic (vs. electromagnetic radiation)
 - ↳ pre-Maxwellian approx. (EEG freq's \ll 1 MHz)
- calculate electric fields as if magnetic fields don't exist
- calculate magnetic fields strictly from distribution of currents
- ignore capacitative effects, too

scalar potential, Φ (what we measure with electrode)

ignore couplings $\vec{B} = \nabla \times \vec{A}$ vector potential \Rightarrow because EEG \ll 1 MHz scalar potential at one position

$$\vec{E} = -\nabla\Phi - \frac{\partial\vec{A}}{\partial t} \approx -\left[\frac{\partial\Phi}{\partial x}\hat{i} + \frac{\partial\Phi}{\partial y}\hat{j} + \frac{\partial\Phi}{\partial z}\hat{k}\right] + 0$$

electric field vector turns scalar field (Φ) into vector field (\vec{E}) gradient of scalar field

(1) \vec{E} defined as force (vector) acting on unit charge at a given point in space (as result of arbitrary distribution of other charges)

(2) Current density, \vec{J} (not curr. source dens.!) is proportional to \vec{E} \rightarrow still a vector!
 $\vec{J} = \sigma \vec{E}$ (Ohm's law) σ is conductivity

CSD is Laplacian of Φ ($= \text{div } \vec{E}$)

(3) Two def's of \vec{A} :
 $\vec{B} = \nabla \times \vec{A}$
 $\vec{A} = \frac{\mu_0}{4\pi} \int_{\text{vol}} \frac{\vec{J}}{|\vec{r}|} d\text{vol}$ (dist-weighted sum of directional currents)

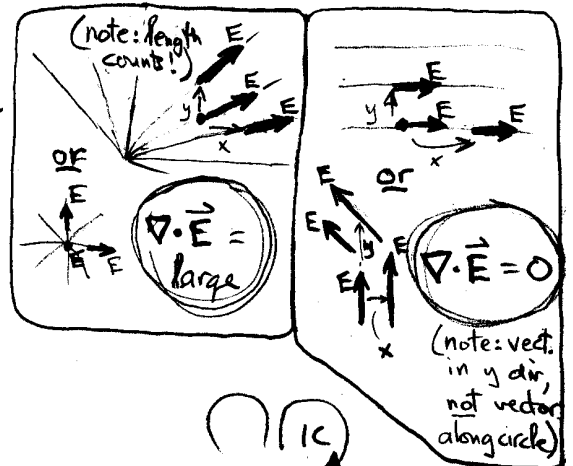
divergence

$$\nabla \cdot (-\nabla\Phi) = \text{scalar field} = -\left[\frac{\partial^2\Phi}{\partial x^2} + \frac{\partial^2\Phi}{\partial y^2} + \frac{\partial^2\Phi}{\partial z^2}\right] \equiv -\nabla^2\Phi$$

measures rate of change of vector field across space makes scalar!
 $\nabla \cdot$ turns vector field into scalar field

meaning of $\nabla \cdot$ \uparrow, \downarrow
 find radiating and contracting regions of \vec{E} vector field

sum of:
 change in x component in x direction + change in y comp. in y dir + ...



3D CSD gold standard (rat BAER paper)

$$\Phi \text{ data (360 points)} \xrightarrow{\nabla} \nabla\Phi \text{ electric vector field} \xrightarrow{\nabla \cdot} \nabla \cdot (-\nabla\Phi) \text{ scalar field source/sink movie as function of } t$$

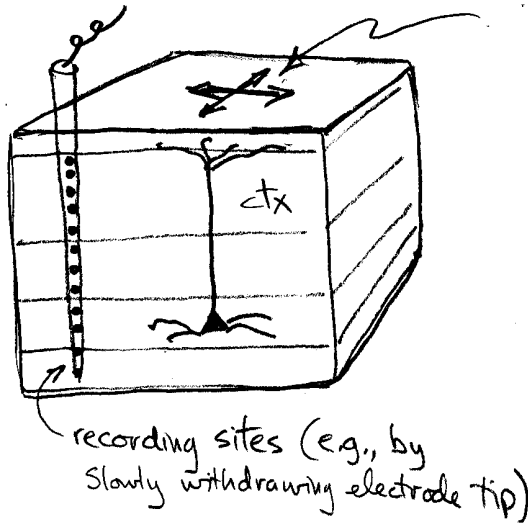
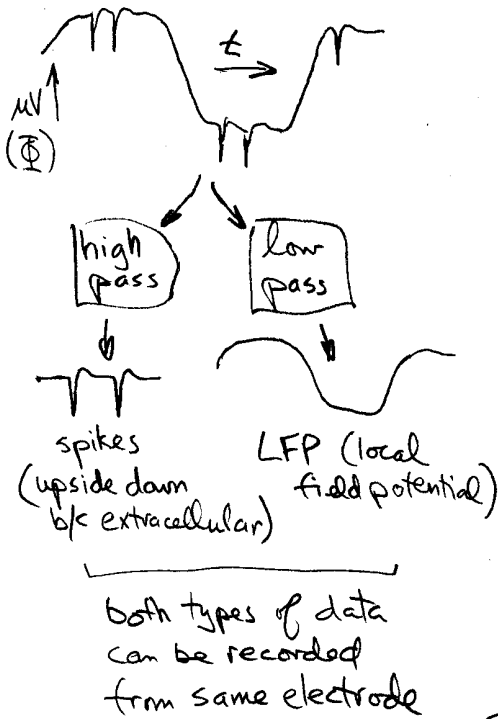


csd-2

1D AND 2D CURRENT SOURCE DENSITY EXPTS.

1D CSD

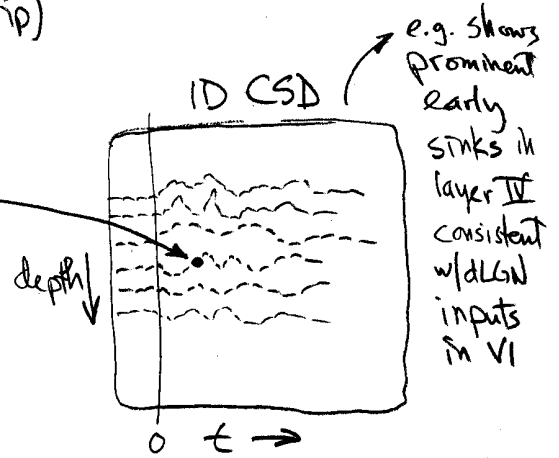
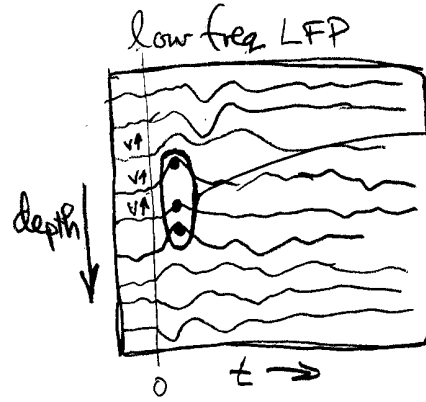
- raw, event-related signal relative to ground, Φ (eg. skull)



ignore these dimension parallel to cortical sheet

rationale: CSD changes much more slowly parallel to cortex than perpendicular to cortical sheet

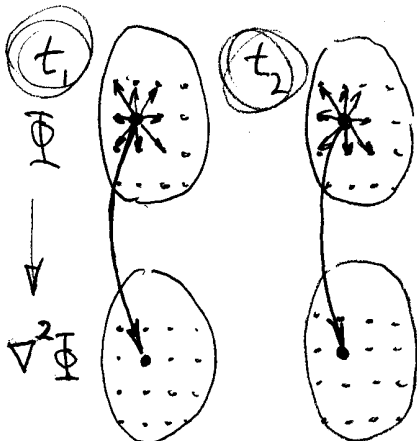
↳ assume approx constant (≈ 0) parallel to ctx



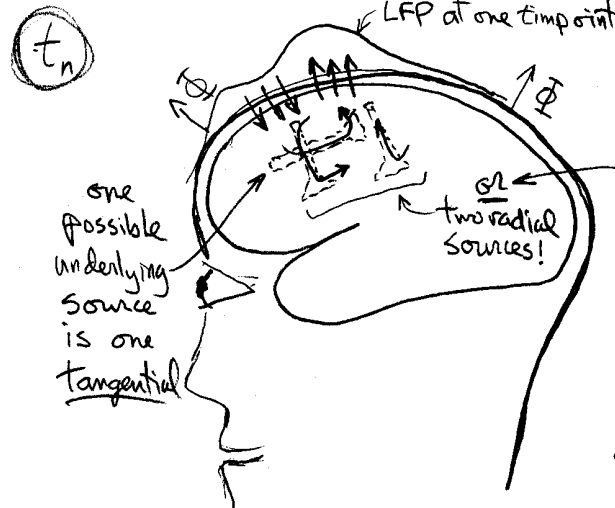
- ∇^2 means find spatial (i.e., 1D depth) curvature of potential
- discrete approx: center - $\frac{\text{above} + \text{below}}{2}$
- N.B. in example above, even though all 3 potentials are positive, smaller value of center point implies sink!

2D CSD

- 2D array of electrodes on pial surface or on scalp



rationale: all electrodes record along same surface so assume depth profiles are constant



- for scalp recordings, sources and sinks are at the scalp (not a depth loc method unless done in 3D)

- can't tell curvature from sign of potential!

concave \rightarrow sink

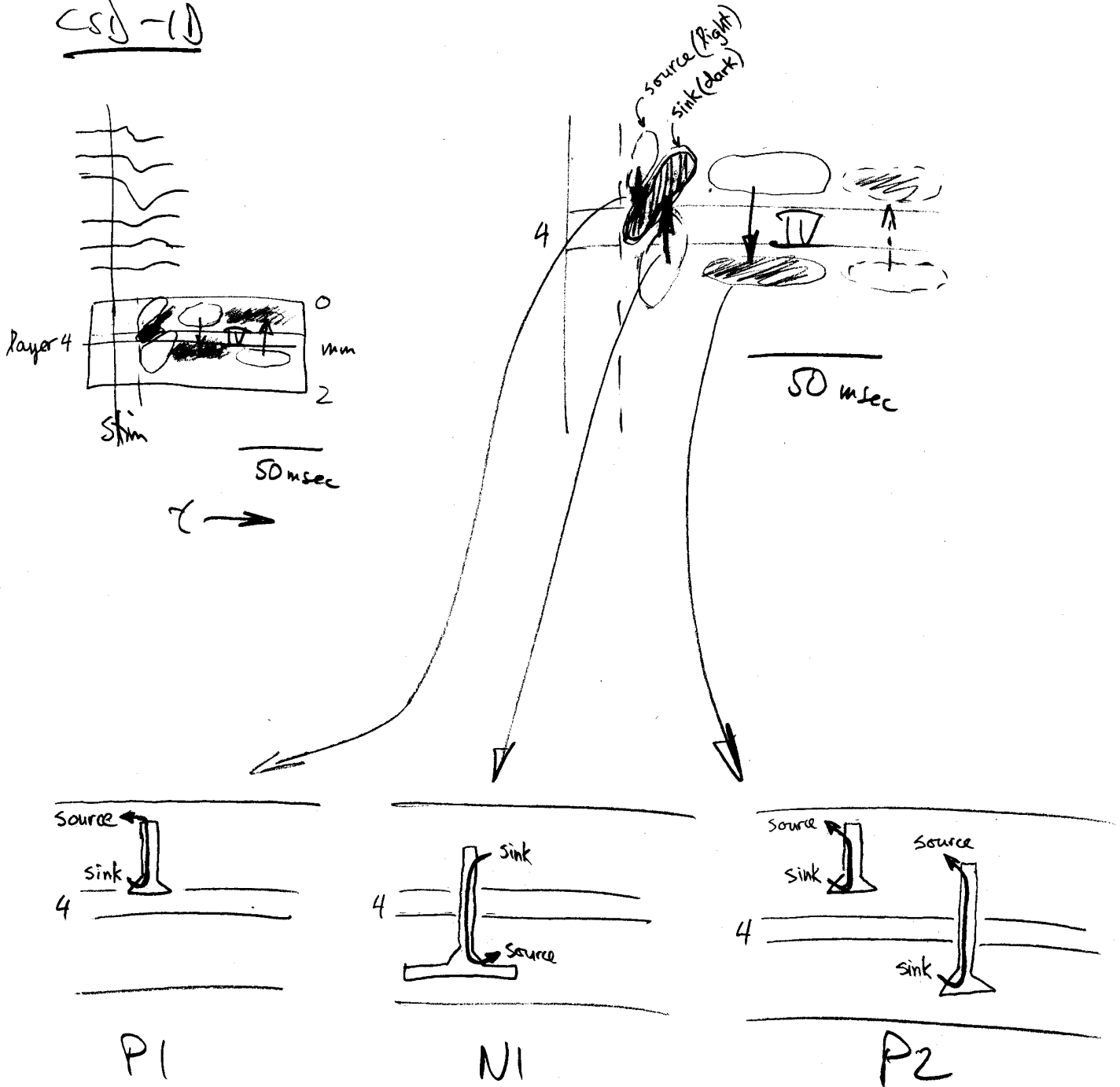
convex \rightarrow source

CSD-3

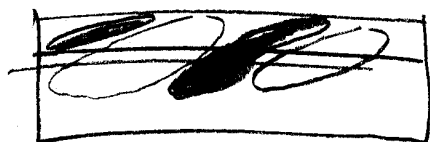
INTRACORTICAL C.S.D.

- e.g. click evoked rat A-I
(Sukov & Barth, 1998)

CSD-1D



- phase-locked CSD p
gamma shifts w/ each cycle



surface electrode is typical ref

forward+
MAXWELL EQUATIONS

Electrostatics, Magnetostatics
 low freq limit'

Ohm's law: $\sigma \vec{E}_i = \vec{J}_i$

like CSD but times σ , conductivity
 (cf. $gV=I, V=IR$)

N.B. these are all defined at a (every) point in space

$\nabla \cdot (\sigma \nabla \Phi) = \nabla \cdot \vec{J}_i$

divergence conductivity constant (or tensor constant if inhomogeneous in different directions) gradient of scalar potential (what we measure invasively) at each point divergence

impressed currents
 currents due to ionic flow that "appear out of nowhere" (Nernst batteries)

$\nabla \cdot \vec{B} = 0$

divergence magnetic field vector at each point

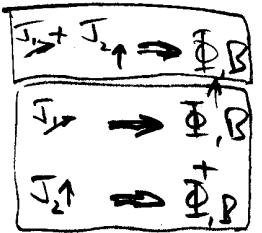
[incidentally, this Maxwell equation violated by a linear gradient in B_z in x, y or z dir]

$\nabla \times \vec{B} = \mu_0 (\vec{J}_i - \sigma \nabla \Phi)$

curl magnetic field permeability impressed currents conductivity gradient of scalar potential ($= \vec{E}$)

- propagation of potentials, magnetic fields instantaneous (no capacitance)
- simultaneous eq's to solve: \vec{J} are sources, Φ, \vec{B} are data
- linear

Potential (Φ) and magnetic fields (\vec{B}) produced by a weighted sum of two current source distributions are equal to weighted sum of fields produced by each current source distribution by itself



forward-2

WHY WE CAN IGNORE MAGNETIC INDUCTION

(from Nunez, 1981)

$$\vec{E} = -\nabla\Phi - \frac{\partial\vec{A}}{\partial t}$$

\vec{E} : electric field
 $-\nabla\Phi$: field component due to charge distribution
 $-\frac{\partial\vec{A}}{\partial t}$: field component due to coupling between electric & magnetic fields

$$\vec{B} \equiv \nabla \times \vec{A}$$

"vector potential"

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

$\nabla \times \vec{H}$: magnetic field (in given medium) induced
 \vec{J} : currents (in given medium)
 $\frac{\partial \vec{D}}{\partial t}$: time varying electric fields (in given medium)

$$\begin{aligned} \vec{H} &= \frac{1}{\mu} \vec{B} && \text{permeability } \mu \\ \vec{J} &= \sigma \vec{E} && \text{conductivity } \sigma \\ \vec{D} &= \epsilon \vec{E} && \text{permittivity } \epsilon \end{aligned}$$

characterize substance linear in all three

this induced magnetic field induces an electric field in turn

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

take $\nabla \times$ of both sides
 use $\vec{B} = \mu \vec{H}$
 substitute this into this

$$\nabla \times \nabla \times \vec{E} = -\mu \frac{\partial}{\partial t} \left(\vec{J} + \frac{\partial \vec{D}}{\partial t} \right)$$

if linear in conductivity and dielectric, too, and fields periodic w/f

$$\nabla \times \nabla \times \vec{E} = -2\pi f i \mu (\sigma + 2\pi f i \epsilon) \vec{E}$$

to neglect: $\frac{2\pi f \mu (\sigma + 2\pi f i \epsilon) |\vec{E}|}{|\nabla \times \nabla \times \vec{E}|} \ll 1$

- 1) $|\nabla \times \nabla \times \vec{E}| \approx |\vec{E}|/L^2$ where L is dist over which \vec{E} varies significantly
- 2) μ of tissue similar to empty space
- 3) assume conservative (large) σ , dielectric const., and EEG freq

↳ number is about $10^{-6} \rightarrow$ small

forward-3
MONOPOLE, DIPOLE FORWARD SOL'N

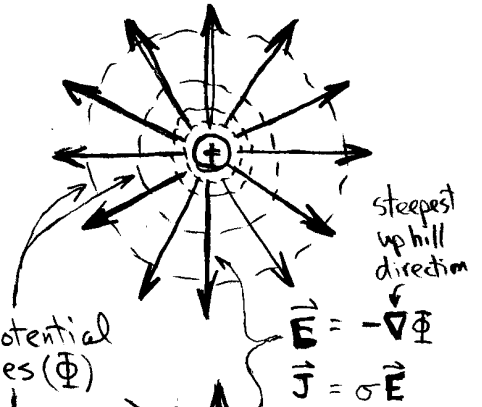
$$\Phi_1 = \frac{S}{4\pi\sigma r}$$

potential recorded for source monopole

strength of source

distance, source to measuring point ($= \|\vec{r}\|$)

Current sources in homogeneous medium (e.g., saltwater tank)

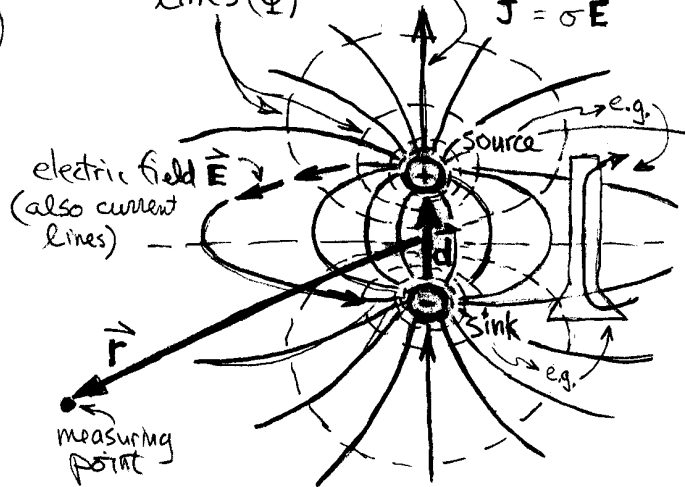


$$\Phi_2 = \frac{S}{4\pi\sigma} \left(\frac{1}{r_1} - \frac{1}{r_2} \right)$$

potential recorded for source-sink pair ("near field")

dipole source to measuring distance

dipole sink to measuring distance



scalar $\Phi_2 \approx \left(\frac{1}{4\pi\sigma} \right) \frac{S \vec{d} \cdot \vec{r}}{r^3}$

measuring point vector (center of dipole to point)

$r \gg d$

now: also explicitly include dipole orientation and measuring point in equations

approximations for "far enough away" measurements (subtracting two 1/r's gives inverse square)

scalar strength

dipole vector, sink to source

distance center of dipole to measuring point

** Since \vec{r} also in numerator, this now inverse square

vector $\vec{B}_2 \approx \left(\frac{\mu_0}{4\pi} \right) \frac{S \vec{d} \times \vec{r}}{r^3}$

$r \gg d$

N.B.: reverse of current flow \leftrightarrow

N.B.: both assume inside infinite isotropic conductor

$$\Phi_i(t) = e_{ij} s_j(t)$$

electrode

gain

one source strength

$$\vec{b}_i(t) = \vec{m}_i s(t)$$

$$b_i(t) = m_i s(t) \rightarrow \text{Squids measure component of } \vec{B}$$

$$\Phi_i(t) = \sum_j e_{ij} s_j(t)$$

all sources

$$b_i(t) = \sum_j m_{ij} s_j(t)$$

$\hookrightarrow 3$ for \vec{B}

Linear superposition with fixed electrodes and sensors

$$\vec{x}(t) = \sum_j \vec{g}_j s_j(t) \rightarrow \vec{x}(t) = \vec{G} \vec{s}(t)$$

elec & mag. measures

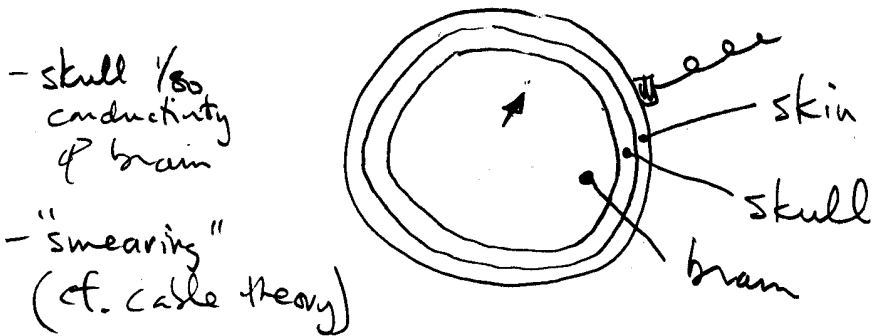
gain vect

strength

forward-4
Forward Solution (1)

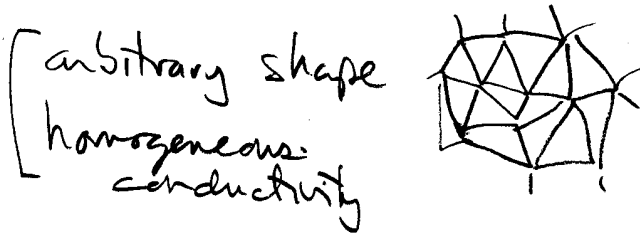
- well-posed (one answer)
- linear: $f(A) + f(B) = f(A+B)$
- approximations due to unknown electrical properties of head

3-shell spherical analytic



- remember, we only need to be able to calc. weight for each dipole/electrode pair independently

3-shell boundary element

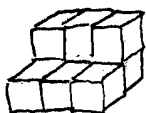


- for magnetic, only need one shell b/c currents thru skin/skull too small to make sig. \vec{B}

calc for one head

solution = infinite homogeneous + $\begin{matrix} x \\ y \\ z \end{matrix}$ matrix of correction factors

finite element



[most general, computational intensive w/ small grid, many unknown parameters to estimate]

forward-S
FORWARD SOLN (2)

recording → V_i ← sensor

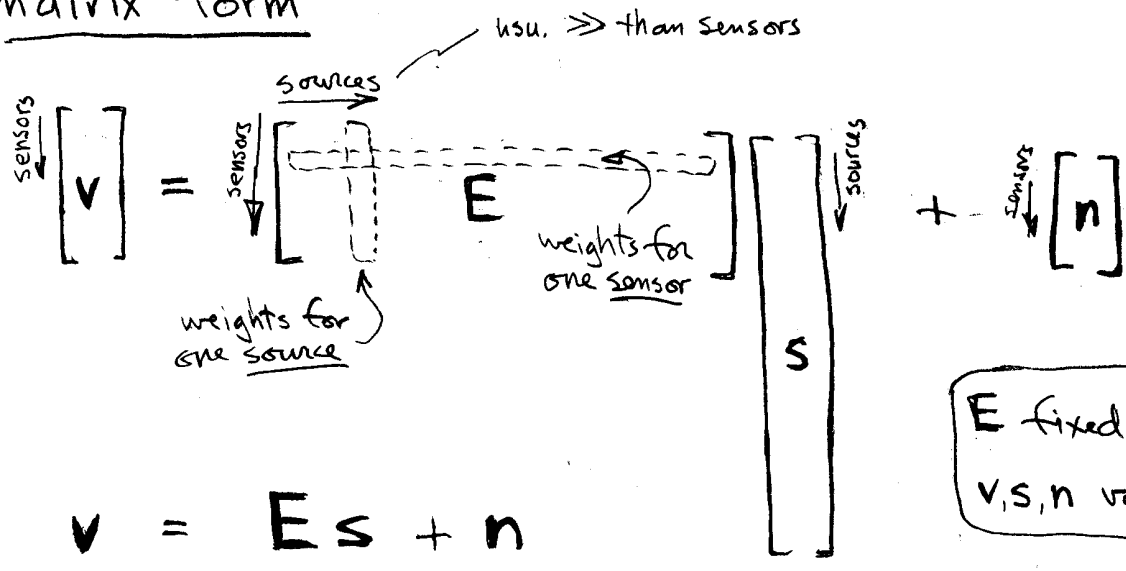
sources → $\sum e_{ij} s_j$ ← forward

source strength at: n_i ← noise

$$V_i = \sum e_{ij} s_j + n_i$$

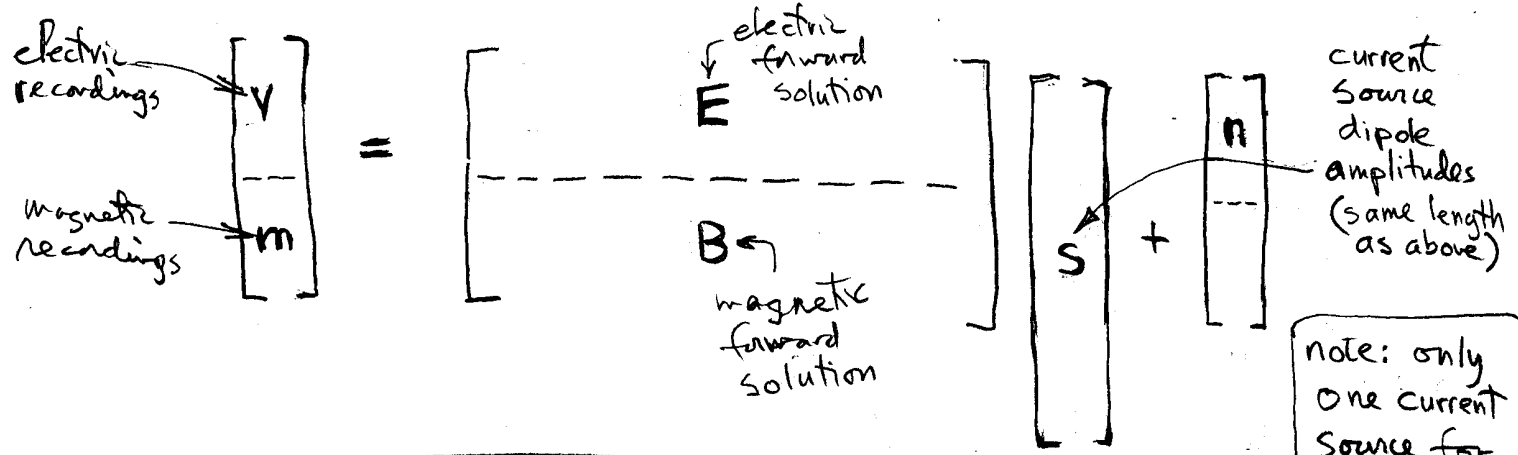
position (x, y, z)
 angle (θ, φ)
 in brain

matrix form



E fixed across time
 V, S, n vary

lower case bold → vector
 upper case bold → matrix



$\vec{x} = \mathbf{A} \vec{s} + \vec{n}$

note: only one current source for each column in the E+B matrix!

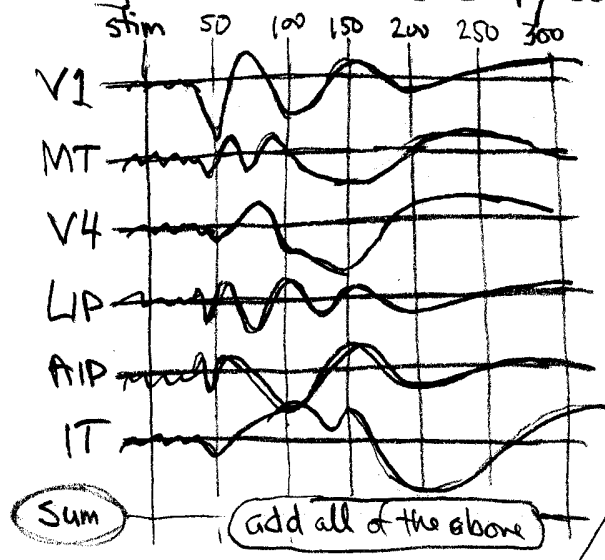
inverse- ϕ
WHY LOCALIZE?

- most of ERP literature based (instead) on temporal "components"

- but:
- 1) underlying local cortical generators (from microelectrode LFP, CSD)
 - extended in time (400 msec), visible from every scalp electrode
 - multiphasic in every cortical area
 - temporally non-static depending on stimulus
 - ↳ e.g. simple contrast, brightness diffs can modulate retinal delay by 50 msec!
 - 2) thus, any "component" consists of sum of activity from multiple cortical areas at different hierarchical levels
 - 3) stimulus manipulations will change temporal overlap
 - ↳ may cause "component" peak to disappear without changing cortical areas being activated
 - 4) verified by intra cortical LFP/CSD (Schroeder et al, 1998)

macaque monkey
 Intracortical data

→ these areas span the visual system from bottom to top, accounting for roughly 50% of the entire macaque monkey cortex



LFP's from approx. layer 4 in cortex ("input layer")

psychologists now identify a few temporal "component" peaks...

↳ but each peak comes from every one of these cortical areas!!

- by contrast, the spatial signature of the signal from one cortical area is static - a better area-based "component"

- temporal "components" should be retired!!
- their original reason for being no longer relevant!!
- easier to record more temporal points (EEG started w/ few electrodes, many time points)
- easier to "paste" high level psychological functions onto a few waveform deflections

inverse-1 Derivation of Ill-posed Inverse

(from Dale & Sereno, 1993)

$$x = As + n$$

x = sensor data vector

A = forward soln matrix ($E+B$)

s = source vector

n = sensor noise vector

solve for
inverse operator

$$Err_w = \langle \|Wx - s\|^2 \rangle$$

probability that rand. var. value is k

$$\text{expectation: } \left[= \sum_k P_k k \right]$$

assume n, s normal, zero-mean w/ corresponding covar. matrices C, R

$$Err_w = \langle \|W(As+n) - s\|^2 \rangle$$

$$= \langle \|(WA - I)s + Wn\|^2 \rangle$$

$$= \langle \|Ms + Wn\|^2 \rangle \quad \text{where } M = WA - I$$

$$= \langle \|Ms\|^2 \rangle + \langle \|Wn\|^2 \rangle$$

$$= \text{tr}(MRM^T) + \text{tr}(WCW^T)$$

diag is noise variance (already squared)

trace is sum of diag elements

(re-expand) $= \text{tr}(WARAT^T W^T - RAT^T W^T - WAR + R) + \text{tr}(WCW^T)$

Explicitly minimize by taking derivative w.r.t. W , set to zero, solve for W

$$0 = 2WARAT^T - 2RAT^T + 2WC$$

$$WARAT^T + WC = RAT^T$$

$$W(ARAT^T + C) = RAT^T$$

$$W = RAT^T (ARAT^T + C)^{-1}$$

equivalent to minimum norm and Tikhonov regularized inverse if C, R are proportional to identity matrix (i.e., sensor noise & sources independent and equal variance)

W is inverse solution operator:

Sources

W

Sensors

inverse-2

INVERSE SOLN (2)

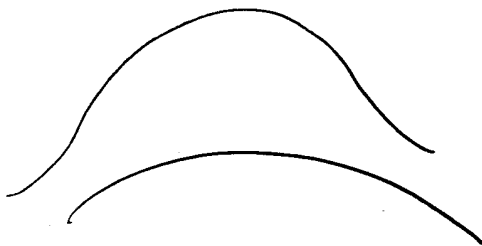
w/ liberal priors [sources uncorrelated (R)
noise uncorrelated (C)

$$W = RA^T (ARA^T + C)^{-1}$$

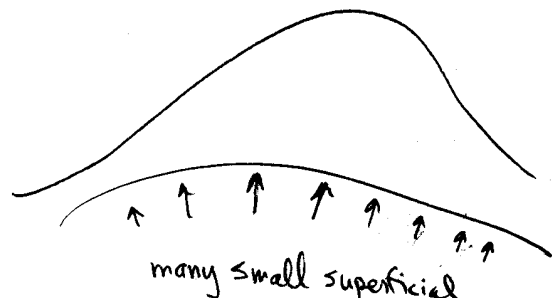
↳ "minimum norm" solution
(find \vec{s} w/ smallest norm = $\|\vec{s}\|$)

- the minimum norm solution appropriately downplays deeper (= weaker scalp signal) sources since these are more likely to fall into the noise floor

- "problems" of minimum norm:
deeper sources get displaced to the surface



↑
one large deep source



many small superficial

achieves smaller norm w/ equivalent fit/error

↑ ↑ ↑

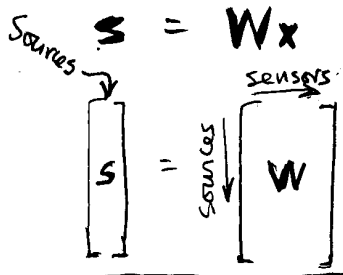
also tiny dipoles in correct place
(see noise normalization)

- small superficial sources "win" because of approx inverse square form of fwd solution,
↳ smaller norm of distributed superficial soln

- can't fix by increasing priors of deep sources!!
↳ that will give deep sources given noise as input!!

inverse-3 INVERSE SOLUTIONS TO ILL-POSED COMPARED

over-determined
↳ least squares
under-determined
↳ minimum norm



- how to use the inverse solution, W
- same W for all time points

"minimum norm" solution
i.e., norm $\|s\|$ of solution is smallest of infinitely many alternate solutions

linear inverse operator \downarrow

spatial covariance sources \swarrow forward soln \searrow

$$W = RA^T (ARA^T + C)^{-1}$$

spatial covariance sensor noise \swarrow

from error minimization derivation

Sensors \downarrow

Sources \downarrow

$$W = \begin{bmatrix} R \end{bmatrix} \begin{bmatrix} A^T \end{bmatrix} \left(\begin{bmatrix} A \end{bmatrix} \begin{bmatrix} R \end{bmatrix} \begin{bmatrix} A^T \end{bmatrix} + \begin{bmatrix} C \end{bmatrix} \right)^{-1}$$

⇓

$[ARA^T] \Rightarrow$ square in # of sensors (small)

easier inverse

linear inverse operator \downarrow

$$W = (A^T C^{-1} A + R^{-1})^{-1} A^T C$$

alternate, algebraically equivalent Bayesian derivation (w/ bigger inverses!)

$$W = \left(\begin{bmatrix} A^T \end{bmatrix} \begin{bmatrix} C \end{bmatrix} \begin{bmatrix} A \end{bmatrix} \right) + \begin{bmatrix} R \end{bmatrix} \begin{bmatrix} A^T \end{bmatrix} \begin{bmatrix} C \end{bmatrix}$$

⇓

$[A^T C^{-1} A] \Rightarrow$ both square in # of sources (large) hard inverses

use inverse-1

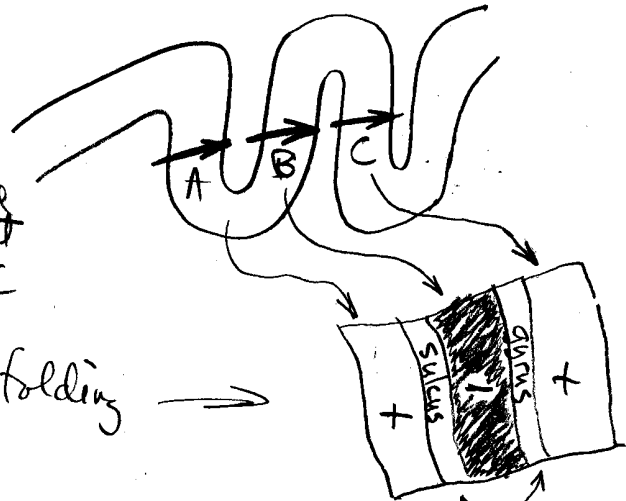
PROBLEMS W/ SURFACE NORMAL

- since nearby points on surface often have different orientation, surface normal constraint can help (since fwd soln A, B very different)



- but, since point spread function: point $\xrightarrow{\text{fwd}}$ data spread $\xleftarrow{\text{invers}}$ typically extends across sulci, artifactual sign reversals occur

positive current at A indistinguishable from negative current at B, or pos at C



↳ after unfolding →

- solutions

- 1) ignore sign → saves useful orientation info!
- 2) solve onto 3 orthogonal dipoles at each cortical point instead of a single oriented dipole
 - ↳ more appropriate when averaging across subjects, since detailed orientations vary a lot
 - also, fills in bottom of sulcus (else unsigned stripes)

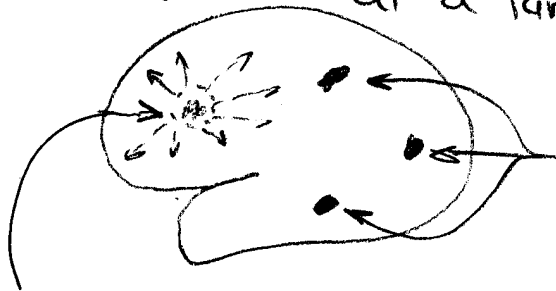


use inverse-2

fMRI Constrained Inverse

[could be
combined
w/ MUSIC!]

- insert fMRI values for R_{ii} 's
- but still allow other sites to have non-zero R_{ii} 's
- pathologies occur if solution restricted completely to fMRI points by setting non fMRI R_{ii} 's to zero ↗ set to small number instead!
- this allows extracting time course from sources visible in EEG/MEG and fMRI
- N.B.: sources that are only visible in EEG/MEG will be dispersed to small distributed values at a large number of vertices



visible in both EEG/MEG
and fMRI

visible only
in EEG/MEG

and not fMRI

→ distributed at small amplitude
across many vertices

NOISE SENSITIVITY NORMALIZATION

(1)

forward: $x = As$ well-posed (Liu, Dale, and Belliveau, 2002)

inverse: $s = Wx$ ill posed

Solve: $x = As + n$ for s

$$W = RA^T(AA^T + C)^{-1}$$

variance of dipole strength estimate due to additive sensor noise *(already squared)*
 $Var(s_i) = \langle (W_i n(t))^2 \rangle = W_i C W_i^T$
 that is, sensor noise run through inverse

multiply inverse operator by noise sensitivity matrix, D (diagonal)

$$D_{ii} = \frac{1}{diag_i \sqrt{W C W^T}}$$

$$W^{ns_norm} = DW$$

normalize each row of inverse operator by noise sensitivity at that location

$$s_i^{ns_norm} = (W^{ns_norm} x)_i = (DWx)_i = \frac{W_i x}{\sqrt{W C W^T}_i} = \sqrt{\frac{(W x x^T W^T)_i}{(W C W^T)_i}}$$

if assume Gaussian white noise, noise covariance, C , is multiple of I , so

$$\|w_i\| = \sqrt{W C W^T}_i$$

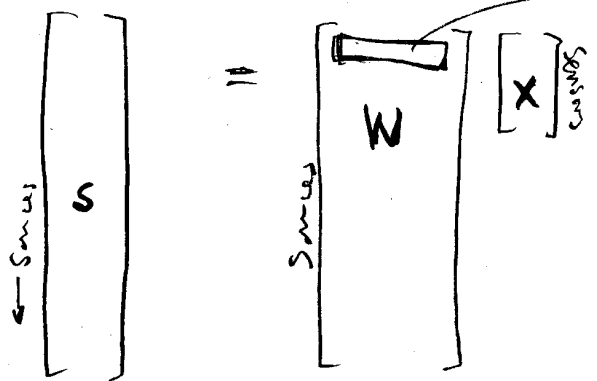
$[W][x][W^T]$
 $\rightarrow W W^T \Rightarrow$ each entry is sum of squares

$$W_i^{ns_norm} = \frac{W_i^{orig}}{\|W_i^{orig}\|}$$

i.e., scale each row of W by single value — the norm of that row

$$s_i = \frac{W_i^{orig} \cdot x}{\|W_i^{orig}\|}$$

row of W is:



inverse solution coefficients for one source \Rightarrow scale (divide) by norm of this row

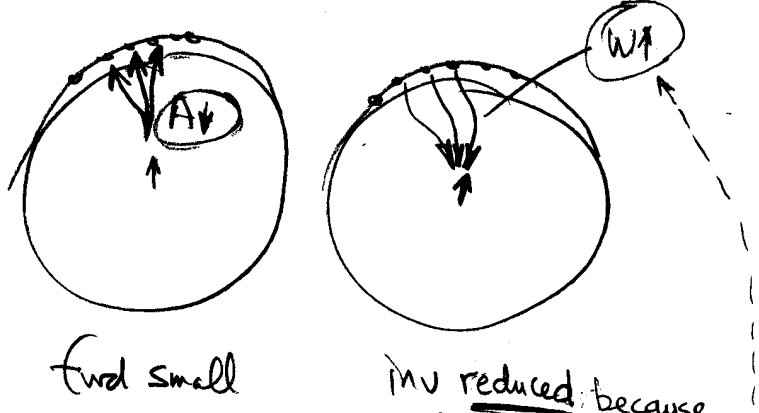
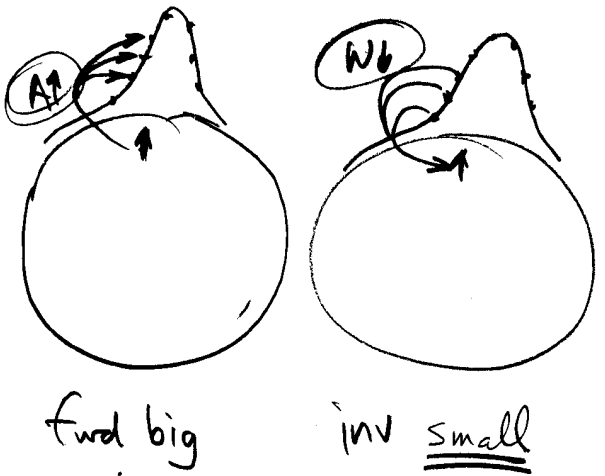
that is, if inverse sol'n for deep source is reduced by interaction of inverse square nature of fwd and min norm, dividing by norm of row of inverse (1 source) will increase / rescue deep source

use inverse-4

NOISE SENSITIVITY NORMALIZATION (2)

shallow source (unit strength)

deep source (unit strength)



inv reduced because of minimum norm
 (N.B. W should be bigger than for superficial source but, min norm reduces b/c of inverse square)

$$S_i = \frac{\vec{W}_i^{orig} \cdot \vec{x}}{\|\vec{W}_i^{orig}\|}$$

shallow: small
 deep: even smaller!

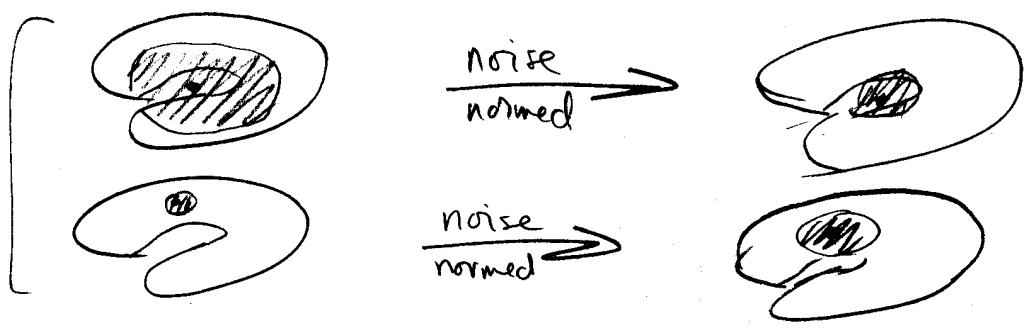
therefore, fixed estimate increased relative to shallow

- effect on inverse solution → more like significance vs actual power

- effect on point-spread function is to equalize shallow & deep

[shallow spread out more than min norm
 deep shrunk to same as shallow

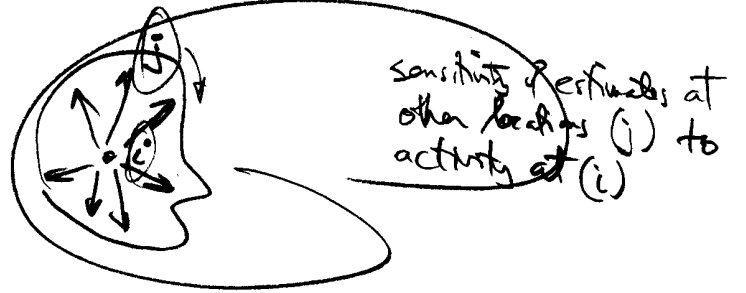
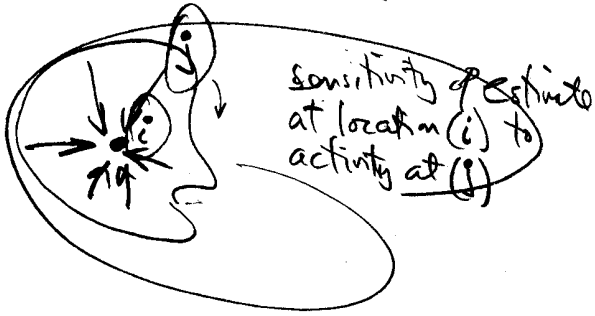
point spread functions



point-spread point fwd data spread in

use inverse -5
POINT-SPREAD / CROSS TALK

point $\xrightarrow{\text{fwd}} \mathbf{W} \xrightarrow{\text{inv}} \text{blur}$
 thus, **WA** measures blur!
 just "take inverse of fwd"



Crosstalk (rows of resolution matrix, WA)
 true fwd

$$\xi_{ij}^2 = \frac{|(W\tilde{A})_{ij}|^2}{|(W\tilde{A})_{ii}|^2} = \frac{|w_i \tilde{a}_j|^2}{|w_i \tilde{a}_i|^2}$$

Point spread (columns of resolution matrix, WA)

$$P_{ij}^2 = \frac{|(W\tilde{A})_{ji}|^2}{|(W\tilde{A})_{ii}|^2} = \frac{|w_j \tilde{a}_i|^2}{|w_i \tilde{a}_i|^2}$$

avg crosstalk

$$ACM_i = \frac{\sum_j \xi_{ij}^2}{j}$$

avg point spread

$$APSF_i = \frac{\sum_j P_{ij}^2}{j}$$

- PSF & crosstalk maps identical for standard inverse (WA, the "resolution matrix" is symmetric)
- PSF affected by noise-normalized; crosstalk same (DWA not symmetric)

Conclusions

- more EEG or more MEG, better
- EEG better than MEG (cf. radial) (EEG fwd real currently less accurate)
- biggest gain from adding small # EEG (or MEG) (e.g. 30) to many MEG (or EEG) (e.g. 150)
- easier to add many MEG, so: optimal $\begin{cases} 30 \text{ EEG} \\ 300 \text{ MEG} \end{cases}$
- EEG/MEG forward-solution-scaling-factor error causes \rightarrow more cross talk

music-1
MUSIC (1)

(from Dale & Sereno, 1993) (cf. Mosher & Leahy)

- using sensor covariance

$$D = \langle \mathbf{x}\mathbf{x}^T \rangle = \underbrace{\sigma^2 \mathbf{I}}_{\text{average value of covariance}} + \sum_i \sum_j \underbrace{\sigma_i \sigma_j}_{\text{sensor noise}} \underbrace{Cor(i,j)}_{\text{source correlation}} \underbrace{\mathbf{A}_i \mathbf{A}_i^T}_{\text{times fwd sol'n}}$$

recording vectors at one time point

$$\approx \frac{[\mathbf{x}_1 \dots \mathbf{x}_n] [\mathbf{x}_1 \dots \mathbf{x}_n]^T}{n}$$

Sensors
 Sensors

n recording time points

can take this estimate over short time epochs
 t →

$$D = \mathbf{U} \mathbf{\Lambda} \mathbf{U}^T = \begin{bmatrix} \mathbf{u}_1 & \mathbf{u}_2 & \dots & \mathbf{u}_n & \dots & \dots \\ \lambda_1 & & & & & 0 \\ & & & & & \lambda_n \end{bmatrix}^T$$

** Columns of \mathbf{U} matrix are orthogonal basis vectors of "spatial pattern" space (one pat is spatial patt across sensors)

eigenvector corresponding eigenvalue

= find, order most significant spatial patterns in sensors, over time

Project forward sol'n onto these spatial patterns
 ("project" = dot prod = similarity) for each point in brain
 (fwd defines spatial sensor pattern for unit source)

$$\xi_i = \mathbf{A}_i^T \mathbf{U} \mathbf{\Lambda} \mathbf{U}^T \mathbf{A}_i \Rightarrow \text{big single number if fwd sol'n looks like } \mathbf{u}_i$$

one num for each source all eigenvectors of sensor spatial patterns fwd for → 1 column one source ("gain vector") of \mathbf{A} matrix

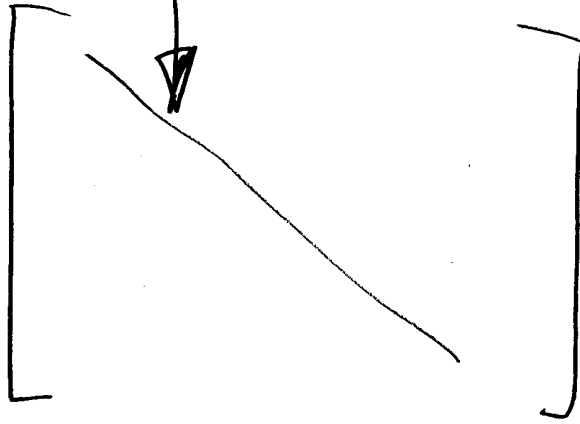
music-2
MUSIC

(2)

how to weight the
minimum norm inverse

$$R_{ii} \approx \frac{A_i^T A_i}{A_i^T U \Lambda^{-1} U^T A_i}$$

total R:



$$W = R A^T (A R A^T + C)^{-1}$$

cf.

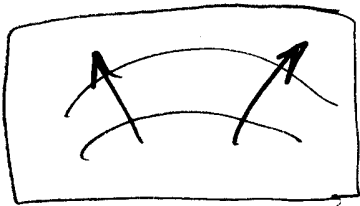
- like parallel resistance

$$R_{\text{parallel}} = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \dots}$$

- ↳ any low resistance (ξ_i) decreases overall resistance (small R_{ii})
- ↳ i.e., if forward soln has appearance like any low eigenvalue spatial pattern, it gets devalued

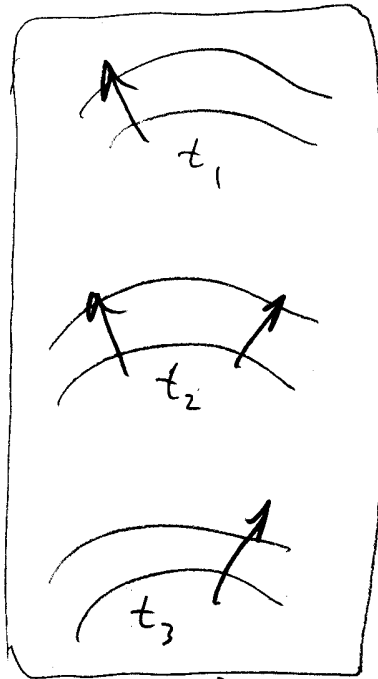
music3
MUSIC (3)

- how it works: take advantage of spatial information that changes over time



one time point

vs.

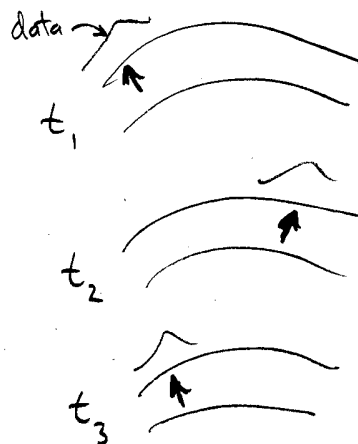
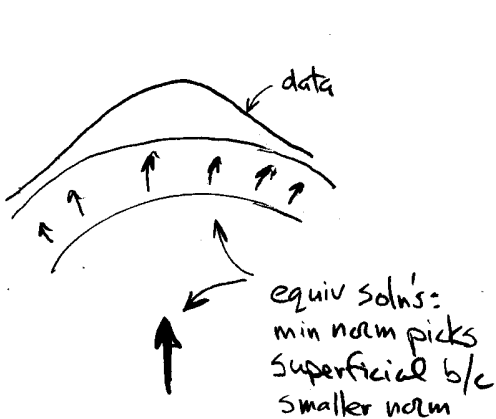


multiple time points

N.B.:
 Problem if assumption about lack of perfect correlation is violated

e.g., if two widely separated sources (i.e. diff fwd solns) are highly correlated, MUSIC will eliminate both since no single fwd soln will look like that "2-separated dipole" pattern (e.g., L/R A-1)
 ↳ "dual MUSIC" hack to fix...

- how it fixes min norm problem



if sources really were superficial, these spatial patterns would appear in \ominus
 if not, superficial sources would be eliminated, leaving deep